

MSc Thesis Project

---

**BCP Lithography Defined Arrays of InAs NWs  
Grown Using MOVPE with Au Seeds**

---

## APPENDIX

2015-11-30

Björn Landeke-Wilsmark



**LUND  
UNIVERSITY**

**Supervisor:** Ivan Maximov ([ivan.maximov@ftf.lth.se](mailto:ivan.maximov@ftf.lth.se))

**Co-supervisor:** Nicklas Nilsson ([nicklas.nilsson@ftf.lth.se](mailto:nicklas.nilsson@ftf.lth.se))

**Examiner:** Carina Fasth ([carina.fasth@ftf.lth.se](mailto:carina.fasth@ftf.lth.se))

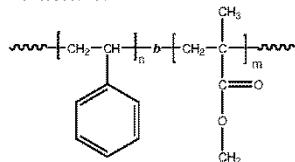
APPENDIX A0  
**Polymer Characterization Data**  
**Supplied By *Polymer Source Inc.***

B82 Data Sheet – Directly From Polymer Source Inc.

**Sample Name:** Poly(styrene-b-methyl methacrylate)  
*(polymethylmethacrylate rich in syndiotactic contents > 78%)*

**Sample #:** P8269-SMMA

**Structure:**



**Composition:**

Mn x 10 <sup>3</sup>	PDI
S-b-MMA	
57.0-b-25.0	1.07
T <sub>g</sub> for PS block: 106°C	T <sub>g</sub> for PMMA block: 127°C

**Synthesis Procedure:**

Poly(styrene-b-methyl methacrylate) is prepared by living anionic polymerization in THF at -78 °C using cumyl potassium initiator in the presence of LiCl. Polystyrene macroanions were end capped with a unit of diphenyl ethylene (DPE) before adding methylmethacrylate (MMA) monomer. For further details please see our published articles.<sup>1-5</sup>

**Characterization:**

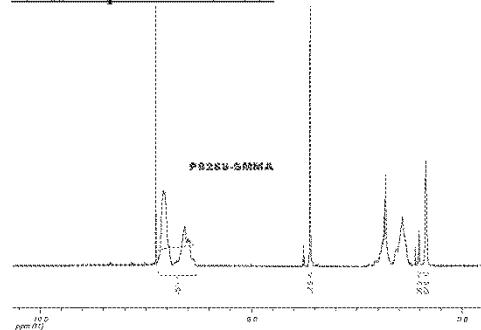
An aliquot of the anionic polystyrene block was terminated before addition of MMA and analyzed by size exclusion chromatography (SEC) to obtain the molecular weight and polydispersity index (PDI). The final block copolymer composition was calculated from <sup>1</sup>H-NMR spectroscopy by comparing the peak area of the poly(methyl methacrylate) protons (eg. -OCH<sub>3</sub> at 3.6ppm) with the of aromatic protons of polystyrene at 6.3-7.2 ppm. Copolymer PDI is determined by SEC.

Thermal analysis of the samples was carried out using a differential scanning calorimeter (TA Q100) at a heating rate of 15°C/min. The inflection glass transition temperature (T<sub>g</sub>) of the sample has been considered.

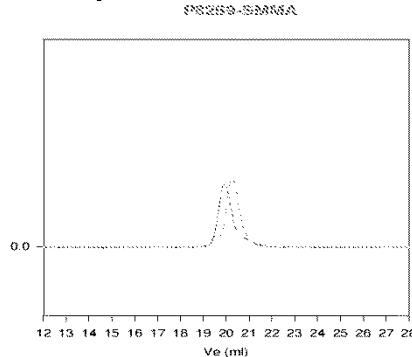
**Solubility:**

Poly(styrene-b-methyl methacrylate) is soluble in THF, toluene, dioxane and CHCl<sub>3</sub>. This polymer readily precipitates from methanol, ethanol, hexanes and water.

**<sup>1</sup>H-NMR Spectrum of SMMA:**

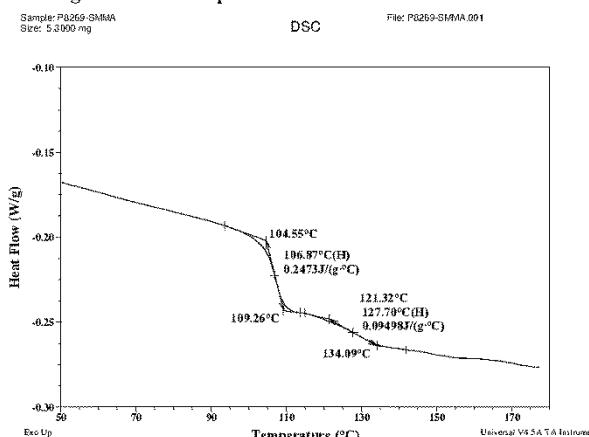


**SEC of Sample -SMMA:**



..... Polystyrene, M<sub>n</sub>=57,000, M<sub>w</sub>=60,000 PI=1.05  
 .... Block Copolymer:  
 From composition from <sup>1</sup>H NMR PS(57,000)-b-PMMA(25,000) Mw/Mn : 1.07

**Thermogram for the sample**



**References for further information:**

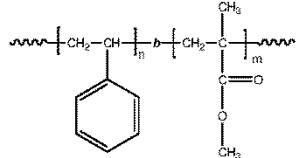
1. S. K. Varshney, R. Fayt, Ph. Teyssie, and J.P. Hautekeer US Patent 5,264,527 (1993)
2. Ph. Teyssie, Ph. Bayard, R. Jerome, S. K. Varshney, and J. S. Wang, *35th IUPAC International Union of Pure & Applied Chemistry International Symposium on Macromolecules* 1994, 67.
3. Ph. Teyssie, R. Fayt, J. P. Hautekeer, C. Jacobs, R. Jerome, L. Leemans and S. K. Varshney *Makromolekulare Chemie, Macromol Symp.*, 1990, 32, 61-73.
4. S. K. Varshney, J. P. Hautekeer, R. Fayt, R. Jerome, and Ph.Teyssie *Macromolecules*, 1990, 23, 2618-2622
5. R. Jerome, R. Forte, S. K. Varshney, R. Fayt, and Ph. Teyssie "The Anionic Polymerization of Alkylacrylates: A Challenge" in the Recent Advances in Mechanistic and Synthetic Aspects of Polymerization. M. Fontanaille and A. Guyot Ed., NATO ASI Series C 215, 101 (1987), C4 Vol. 108, 12, 094992.

**B67 Data Sheet – Directly From Polymer Source Inc.**

Sample Name: Poly(styrene-b-methyl methacrylate) (*polymethylmethacrylate rich in syndiotactic contents > 80%*)

Sample #: P2400-SMMA

Structure:



Composition:

Mn x 10 <sup>3</sup> S-b-MMA	PDI
46.1-b-21.0	1.09
T <sub>g</sub> for PS block: 105°C	T <sub>g</sub> for PMMA block: 128°C

Synthesis Procedure:

Poly(styrene-b-methyl methacrylate) is prepared by living anionic polymerization in THF at -78 °C using sec.BuLi initiator in the presence of LiCl. Polystyrene macroanions were end capped with a unit of diphenyl ethylene (DPE) before adding methylmethacrylate (MMA) monomer.

Characterization:

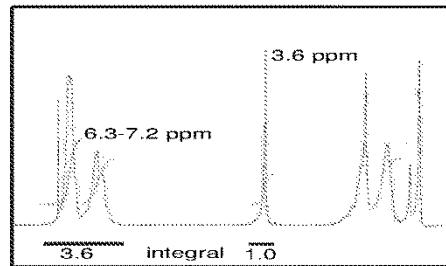
An aliquot of the anionic polystyrene block was terminated before addition of MMA and analyzed by size exclusion chromatography (SEC) to obtain the molecular weight and polydispersity index (PDI). The final block copolymer composition was calculated from <sup>1</sup>H-NMR spectroscopy by comparing the peak area of the poly(methyl methacrylate) protons (eg. -OCH<sub>3</sub> at 3.6ppm) with the of aromatic protons of polystyrene at 6.3-7.2 ppm. Copolymer PDI is determined by SEC.

Thermal analysis of the samples was carried out using a differential scanning calorimeter (TA Q100) at a heating rate of 15°C/min. The inflection glass transition temperature (T<sub>g</sub>) of the sample has been considered.

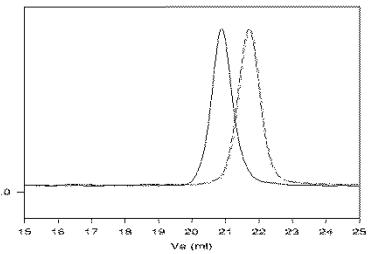
Solubility:

Poly(methyl methacrylate) is soluble in THF, CHCl<sub>3</sub>, toluene and dioxane. The polymer precipitates from hexanes, methanol and ethanol.

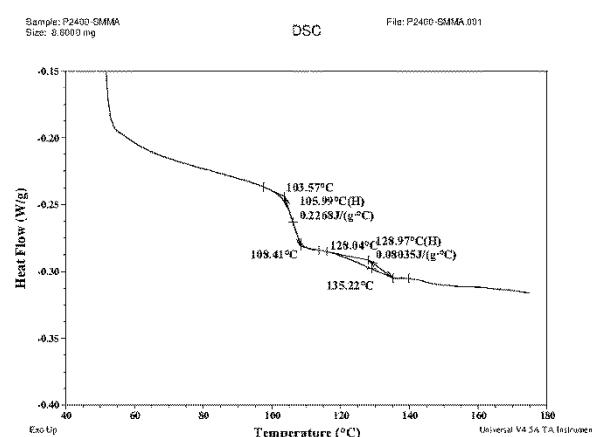
**<sup>1</sup>H-NMR Spectrum of P2400-SMMA:**



**SEC of Sample P2400-SMMA:**



**Thermograms of sample**



**References for further information:**

1. S. K. Varshney, R. Fayt, Ph. Teyssié, and J.P. Hautekeer US Patent 5,264,527 (1993)
2. Ph. Teyssié, Ph. Bayard, R. Jerome, S. K. Varshney, and J. S. Wang, *35th IUPAC International Union of Pure & Applied Chemistry International Symposium on Macromolecules* 1994, 67.
3. Ph. Teyssié, R. Fayt, J. P. Hautekeer, C. Jacobs, R. Jerome, L. Leemans and S. K. Varshney *Makromolekulare Chemie, Macromol. Symp.*, 1990, 32, 61-73.
4. S. K. Varshney, J. P. Hautekeer, R. Fayt, R. Jerome, and Ph.Teyssié *Macromolecules*, 1990, 23, 2618-2622.
5. R. Jerome, R. Forte, S. K. Varshney, R. Fayt, and Ph. Teyssié "The Anionic Polymerization of Alkylacrylates: A Challenge" in the Recent Advances in Mechanistic and Synthetic Aspects of Polymerization: M. Fontanaille and A. Guyot Ed., NATO ASI Series C215,101 (1987), C4 Vol. 108, 12, 094992.

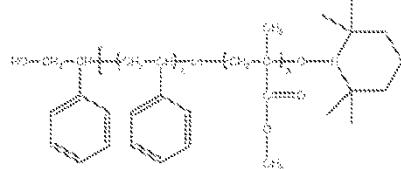
R10.5 Data Sheet – Directly From Polymer Source Inc.

Sample Name:

Random Copolymer Poly(styrene-co-methyl methacrylate),  
 $\alpha$ -Hydroxyl- $\omega$ -Tempo moiety Terminated

Sample #: P18984B-SMMAranOHT

Structure:

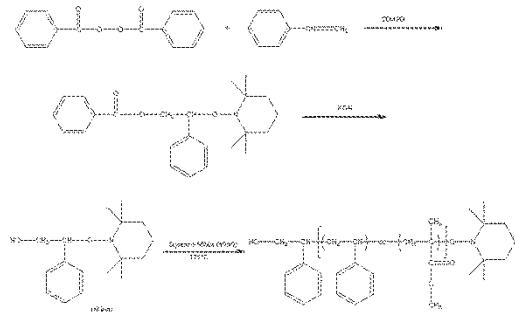


Composition:

Mn x 10 <sup>3</sup> (Styrene content mol%)	Mw/Mn (PDI)
10.5 (66 %)	1.15

Synthesis Procedure:

Hydroxy terminated poly(styrene-co-methyl methacrylate) is prepared by stable free radical polymerization at 135°C. The reaction scheme is shown below:



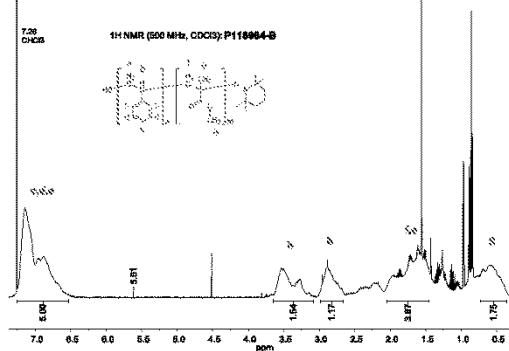
Characterization:

An aliquot of the copolymer was analyzed by size exclusion chromatography (SEC) to obtain the molecular weight and polydispersity index (PDI), the instrument calibrated by Polystyrene standards. The chemical composition was calculated from <sup>1</sup>H-NMR spectroscopy by comparing the peak area of the phenyl protons at 6.8-7.4 ppm with the peak area of methyl methacrylate at 2.6-3.6 ppm.

Solubility:

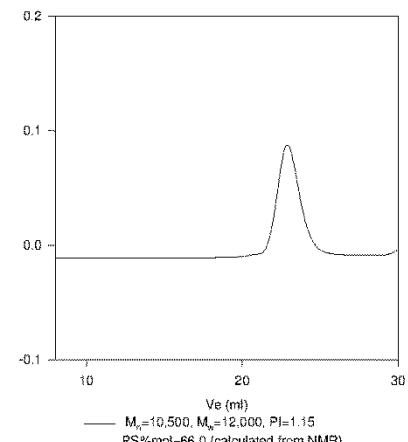
Poly(styrene-co-methyl methacrylate) is soluble in THF, DMF, Toluene and chloroform. Precipitate from methanol and Hexanes.

<sup>1</sup>H NMR spectrum



SEC profile of the random copolymer

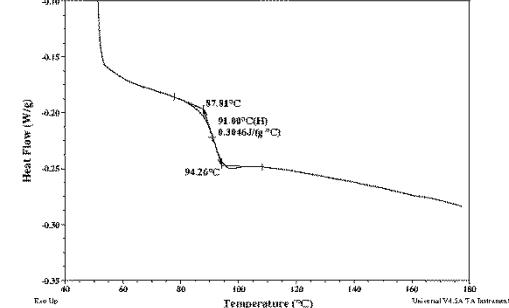
P18984B-SMMAranOHT



— M<sub>w</sub>=10,500, M<sub>n</sub>=12,000, PI=1.15

PS%mol=66.0 (calculated from NMR)

Sample: P18984B-SMMAranOHT  
 Size: 5.6000 mg  
 File: P18984B-SMMAranOHT

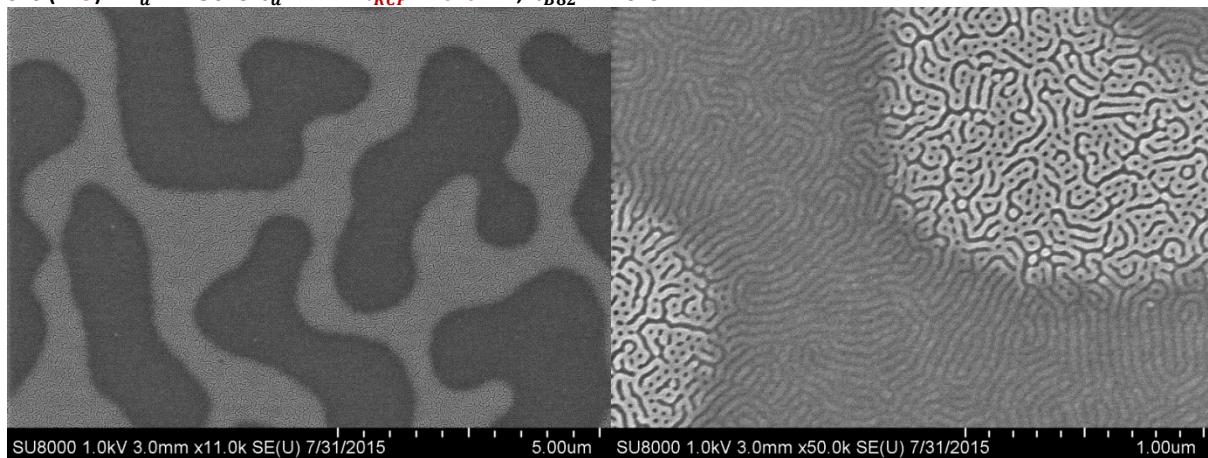


v.A-2

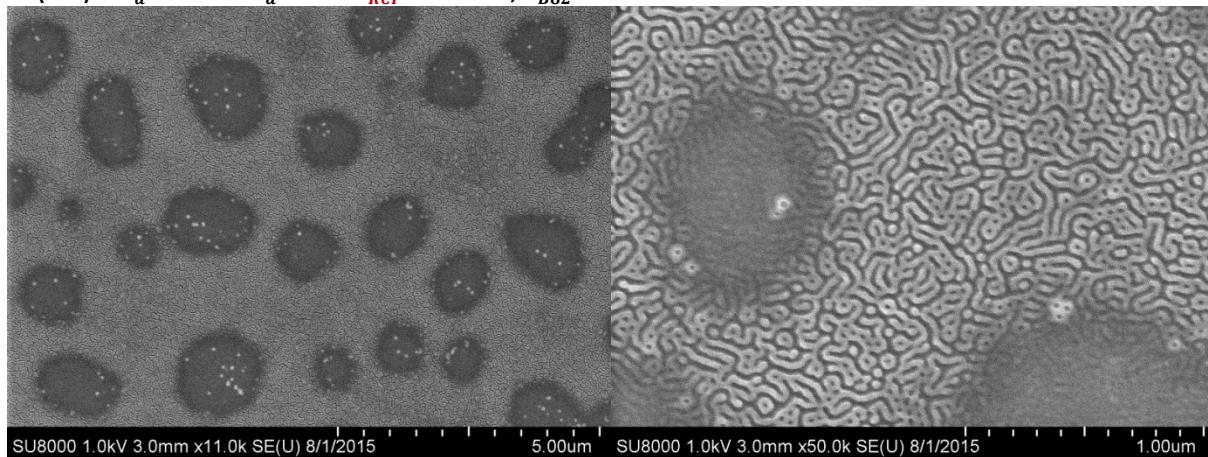
**APPENDIX A1**  
**R10.5 Grafting**

**A1.1** The influence of  $h_{R10.5}$  on orientation and ordering of the subsequent B82 layer

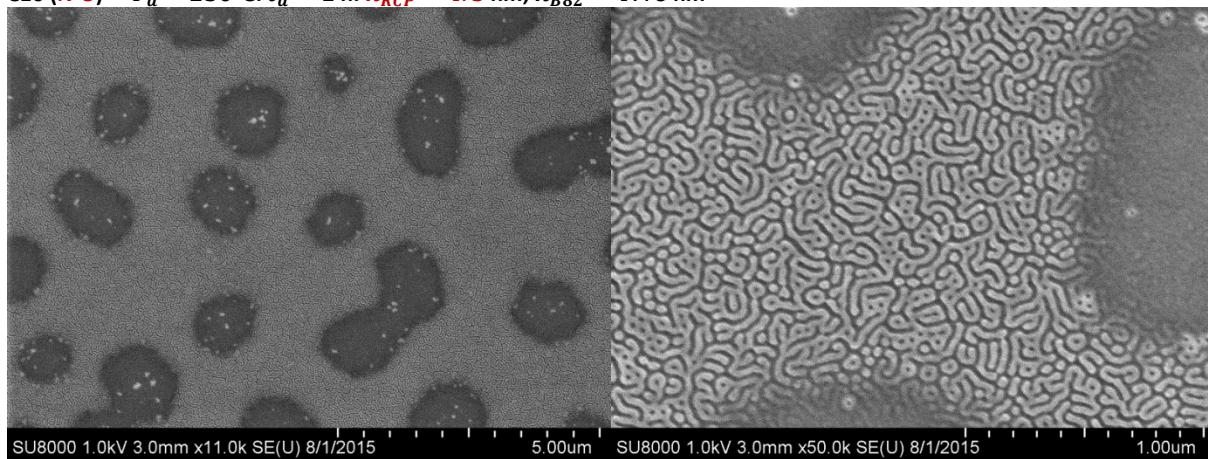
S20 (N-U) –  $T_a = 250^\circ\text{C}$ .  $t_a = 1 \text{ h}$ .  $h_{RCP} = 0.0 \text{ nm}$ ;  $h_{B82} = 46.6 \text{ nm}$



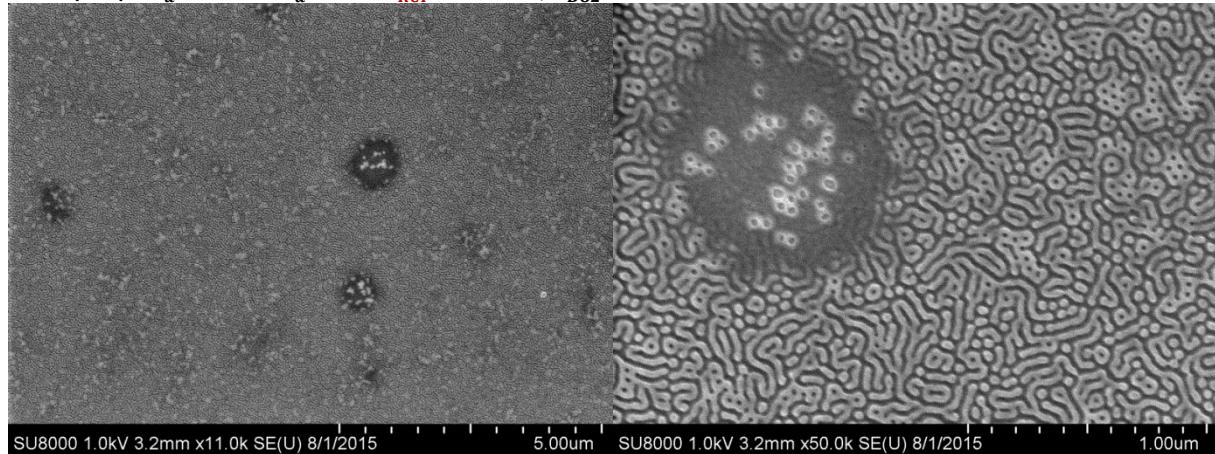
C2 (N-U) –  $T_a = 250^\circ\text{C}$ .  $t_a = 1 \text{ h}$ .  $h_{RCP} = 3.4 \text{ nm}$ ;  $h_{B82} = 46.5 \text{ nm}$



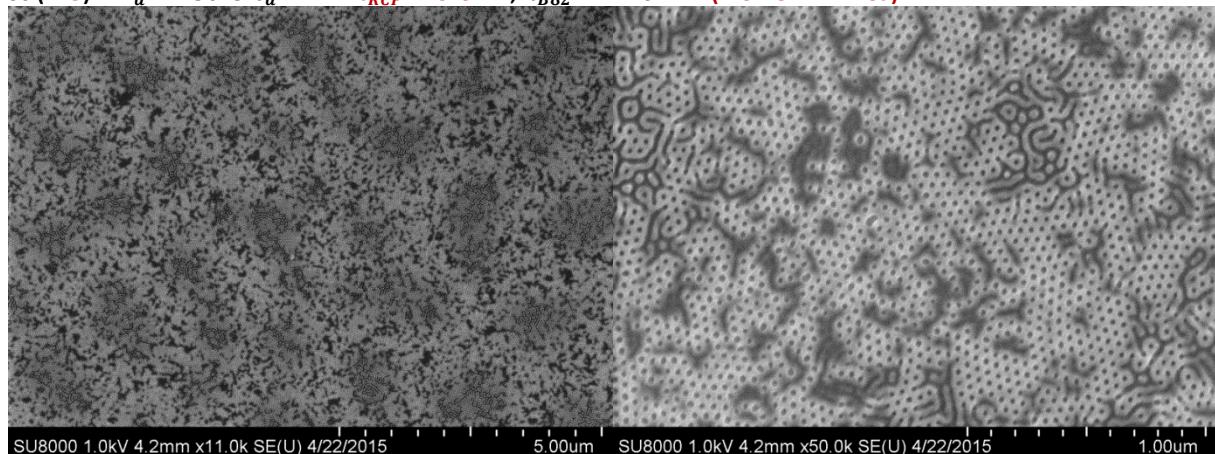
C16 (N-U) –  $T_a = 250^\circ\text{C}$ .  $t_a = 1 \text{ h}$ .  $h_{RCP} = 4.5 \text{ nm}$ ;  $h_{B82} = 47.6 \text{ nm}$



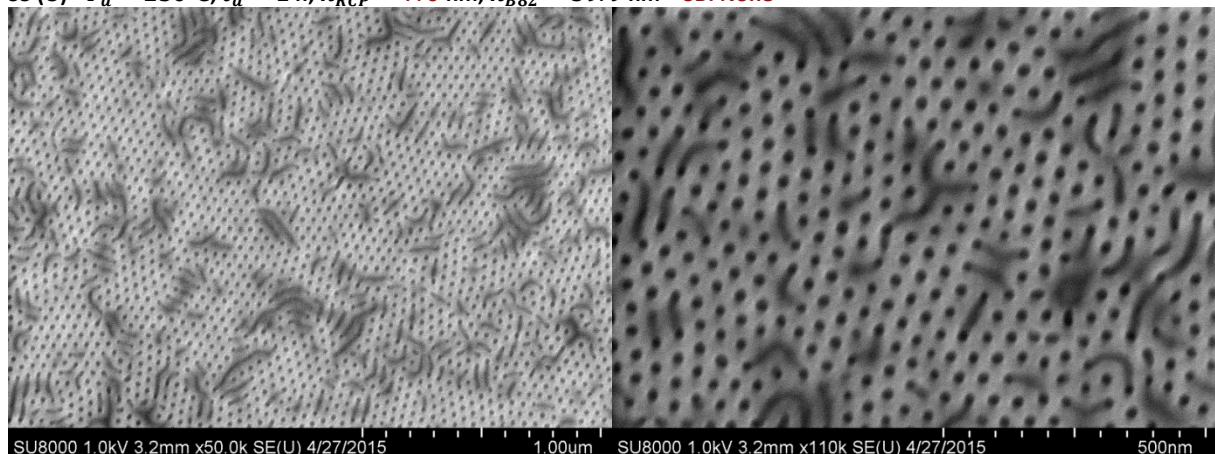
**W48C (N-U) –  $T_a = 250^\circ\text{C}$ .  $t_a = 1 \text{ h}$ .  $h_{RCP} = 5.9 \text{ nm}$ ;  $h_{B82} = 47.9 \text{ nm}$**



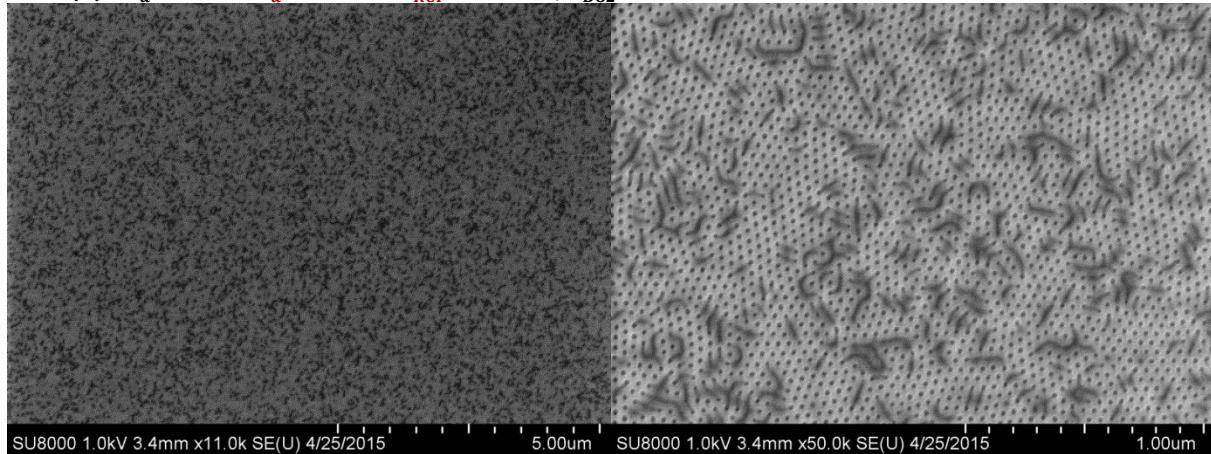
**S6 (N-U) –  $T_a = 250^\circ\text{C}$ .  $t_a = 1 \text{ h}$ .  $h_{RCP} = 6.6 \text{ nm}$ ;  $h_{B82} = 41.0 \text{ nm}$  - (Pre-Dev. Thinned)**



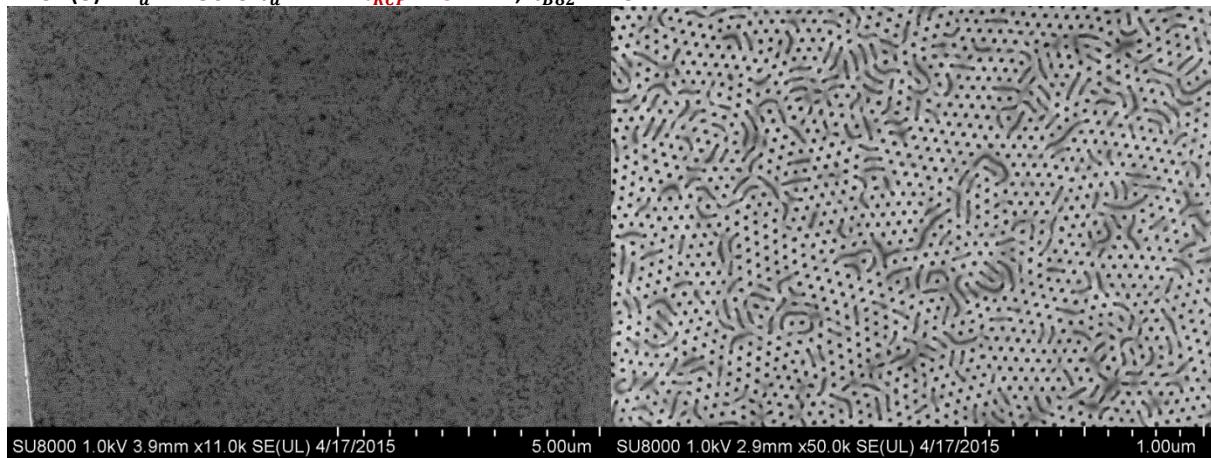
**S3 (U) -  $T_a = 250^\circ\text{C}$ ;  $t_a = 1 \text{ h}$ ;  $h_{RCP} = 7.0 \text{ nm}$ ;  $h_{B82} = 39.9 \text{ nm}$  – SB: None**



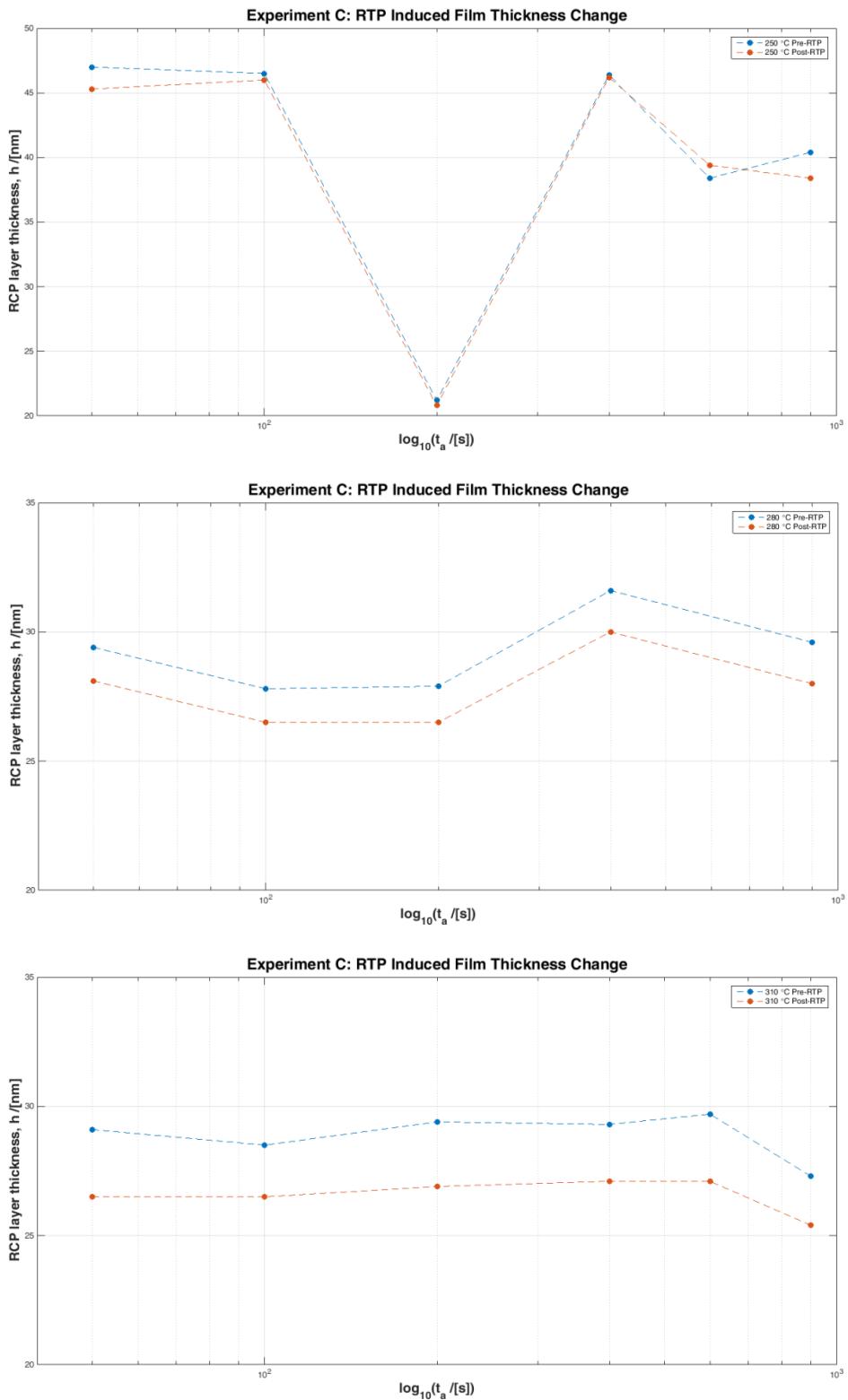
W21C (U) –  $T_a = 250^\circ\text{C}$ .  $t_a = 30 \text{ min}$ .  $h_{RCP} = 7.7 \text{ nm}$ ;  $h_{B82} = 39.4 \text{ nm}$



W15E (U) –  $T_a = 250^\circ\text{C}$ .  $t_a = 1 \text{ h}$ .  $h_{RCP} = 8.1 \text{ nm}$ ;  $h_{B82} = 43.2 \text{ nm}$



### A1.2 RTP Induced R10.5 layer thickness reduction



### A1.3 Identification of RTP $t_{Graft}$ and $T_{Graft}$ combinations conducive to the grafting of R10.5

Sample #	Piranha Treatment		RTP Graft		R10.5 Ellips.					Comments
	$t_{\text{Piranha}}$ /[min]	$T_{\text{Piranha}}$ /°C]	$T_{\text{Graft}}$ /°C]	$t_{\text{Graft}}$ [s]	MSE	$h_{\text{SiO}_x}$ /Å]	$h_{\text{R10.5}}$ /[nm]	$\text{Age}_1$ /[days]	$\text{Age}_2$ /[days]	
C13	40	80	250	50	4.259	15	6.2	0	1	
C14	40	80	250	100	3.948	15	6.5	0	1	
C12	40	80	250	200	4.113	15	6.3	1	0	
C15	40	80	250	400	4.532	15	6.6	1	0	
C17	40	80	250	600	3.992	15	6.4	1	0	
C16	40	80	250	900	3.808	15	6.5	1	0	
C11 (I)	40	80	280	50	3.365	15	6.1	3	3	
C10	40	80	280	100	3.428	15	7.0	2	3	
C9	40	80	280	200	3.37	15	7.2	2	3	
C8	40	80	280	400	3.309	15	7.4	1	4	
A1	30	80	280	600	4.364	15	6.4	1	0	Unfiltered R10.5; <b>Patch (center)</b>
A2	30	80	280	600	4.31	15	8.0	1	0	Unfiltered R10.5
A3	30	80	280	600	4.273	15	7.9	1	0	Unfiltered R10.5
A4	30	80	280	600	4.441	15	7.7	1	0	Unfiltered R10.5
B1	30	80	280	600	4.416	15	8.3	1	0	Unfiltered R10.5
B2	30	80	280	600	4.74	15	8.3	1	0	Unfiltered R10.5
B3	30	80	280	600	4.347	15	7.9	1	0	Unfiltered R10.5
B4	30	80	280	600	4.292	15	7.6	1	0	Unfiltered R10.5
C7	40	80	280	900	3.66	15	7.4	1	4	
C6	40	80	310	50	3.878	15	5.1	1	4	
C5	40	80	310	100	3.779	15	5.5	1	4	
C3	40	80	310	200	3.761	15	5.5	1	4	
C2	40	80	310	400	3.834	15	5.6	0	5	
C4	40	80	310	600	3.805	15	5.7	1	4	
C1	40	80	310	900	3.986	15	5.2	0	5	
D15	40	80	265	600	4.278	15	5.9	16	1	
D16	40	80	295	600	4.216	15	7.1	16	1	
D3	40	80	280	600	4.176	15	5.0	13	1	$dT/dt = 10^\circ \text{ C/s}$
D4	40	80	280	600	3.934	15	6.2	13	1	$dT/dt = 5^\circ \text{ C/s}$
D5	40	80	280	600	3.973	15	6.1	13	1	$dT/dt = 5^\circ \text{ C/s}$

#### A1.4 The efficacy of different surface activation treatments on Si(100) substrates

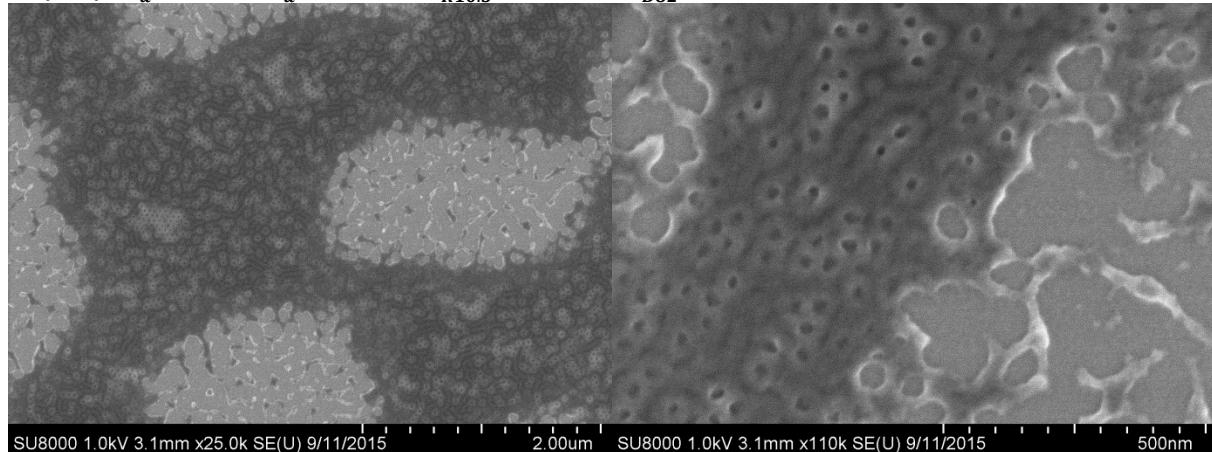
Sample #	Treatment	Before	After	Diff.	R10.5 Ellips.			$h_{SiO_x}$ used /[Å]	$h_{R10.5}$ / [nm]	$Age_1$ / [days]	$Age_2$ / [days]
		$h_{SiO_x, 1}$ / [Å]	$h_{SiO_x, 2}$ / [Å]	$\Delta h_{SiO_x}$ / [Å]	T <sub>Graft</sub> / [°C]	t <sub>Graft</sub> / [min]					
D1	None	NA	NA	NA	280	10	15	6.6	3	1	
D2	None	NA	NA	NA	280	10	15	6.0	3	1	
D10	Ozone	NA	NA	NA	280	10	14.56	7.4	0	0	
D11	Ozone	NA	NA	NA	280	10	14.56	7.3	0	0	
D14	Ozone	15.57	14.56	-1.01	280	10	14.56	6.7	0	0	
D17	PP (FC)	14.92	13.88	-1.04	280	10	13.88	7.8	0	0	
D18	PP (FC)	14.56	13.93	-0.63	280	10	13.93	8.0	0	0	
D6	PP (No FC)	NA	NA	NA	280	10	15	7.8	2	1	
D7	PP (No FC)	NA	NA	NA	280	10	15	7.6	2	1	
D13	PP (No FC)	14.94	15.3	0.36	280	10	15.30	7.6	0	0	
D8	RIE	NA	NA	NA	280	10	31.02	5.3	0	0	
D9	RIE	NA	NA	NA	280	10	31.02	6.4	0	0	
D12	RIE	14.71	31.02	16.31	280	10	31.02	5.8	0	0	

**APPENDIX A2**  
**BCP Annealing**

## A2.1 DUV exposure dose test

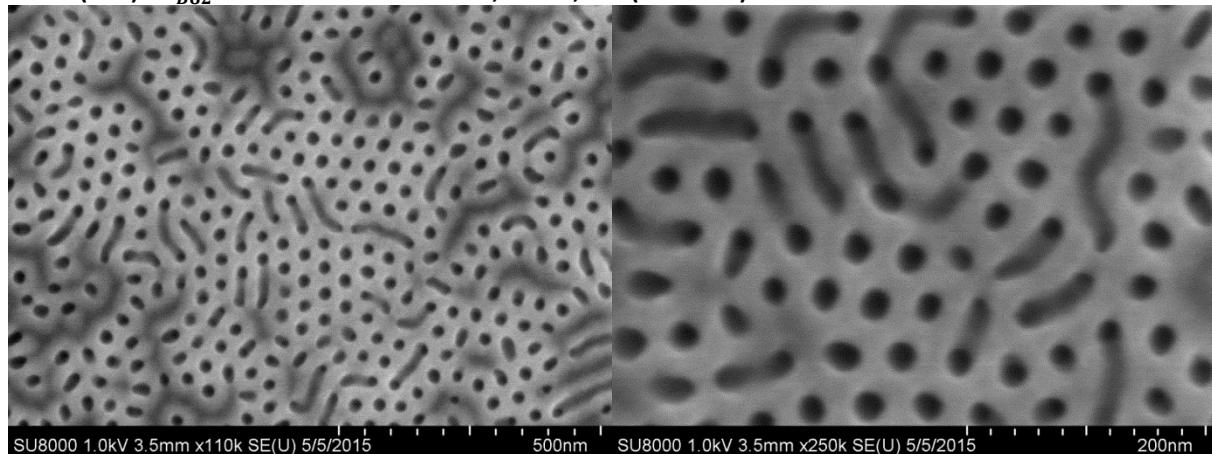
E = cycle exposure time, W = cycle waiting (non-exposure) time, c = number of cycles

B3 (N-U) -  $T_a = 250^\circ\text{C}$ ;  $t_a = 10 \text{ min}$ ;  $h_{R10.5} \leq 7.9 \text{ nm}$ ;  $h_{B82} = 44.6$  – DUV: E 30s, W 60s, 20c

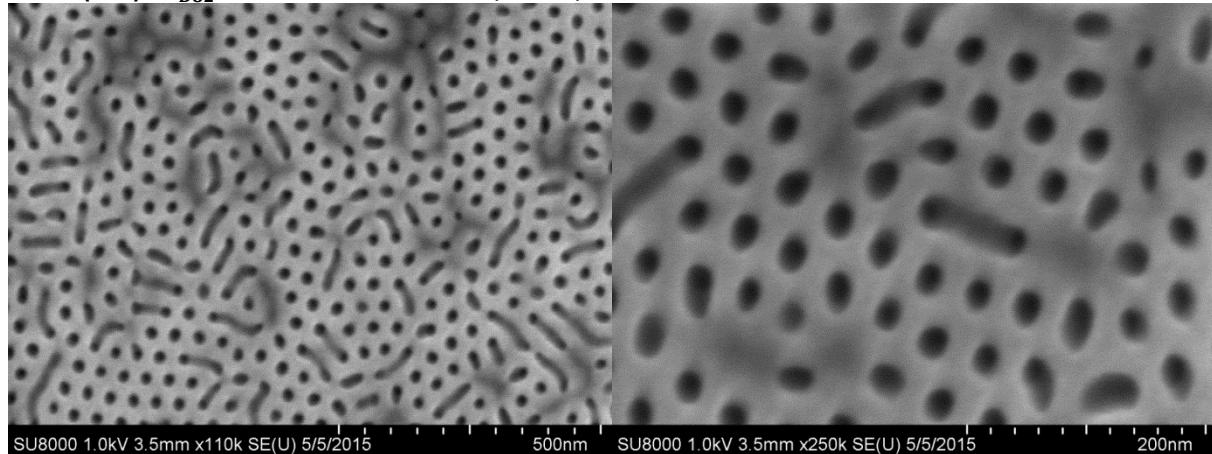


W26C-F: RTP:  $T_a = 250^\circ\text{C}$ ;  $t_a = 30 \text{ min}$ ;  $h_{RCP} = \text{NA}$  (Guess: 8 nm) (AW)

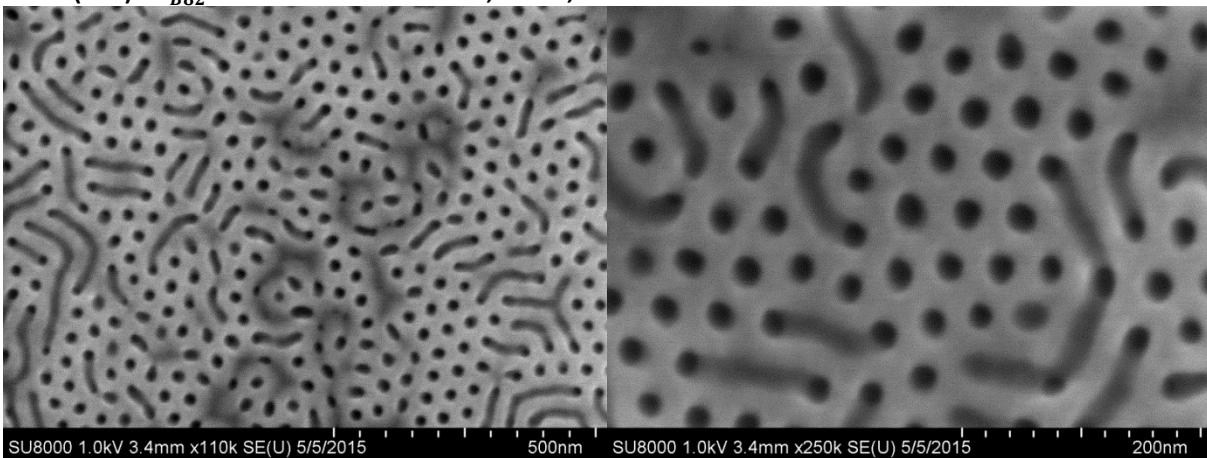
W26C (N-U) -  $h_{B82} \approx 44.4 \text{ nm}$  – DUV: E 10s, W 20s, 24c (Standard)



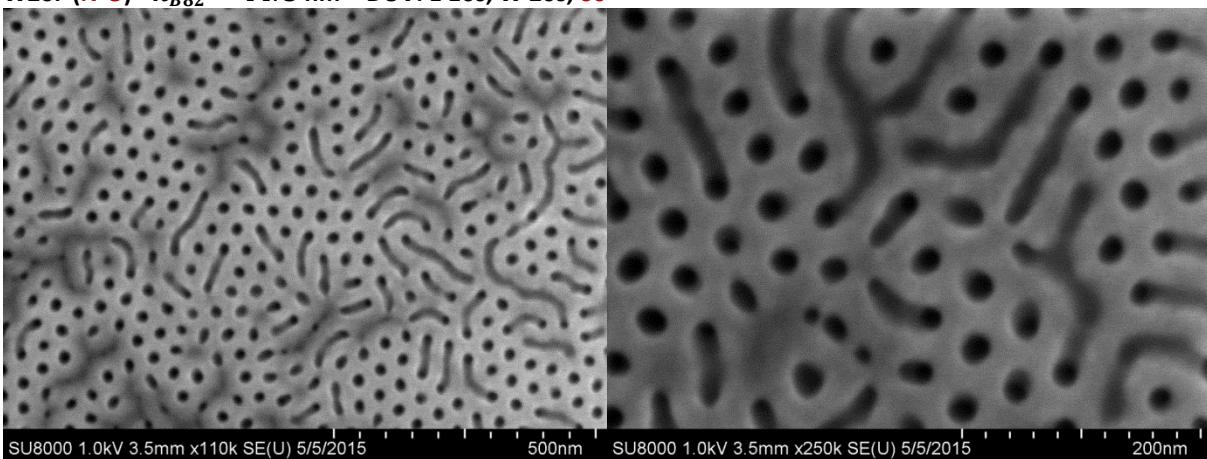
W26D (N-U) -  $h_{B82} \approx 44.3 \text{ nm}$  – DUV: E 10s, W 20s, 18c



W26E (N-U) -  $h_{B82} \approx 44.4 \text{ nm}$  – DUV: E 10s, W 20s, **12c**

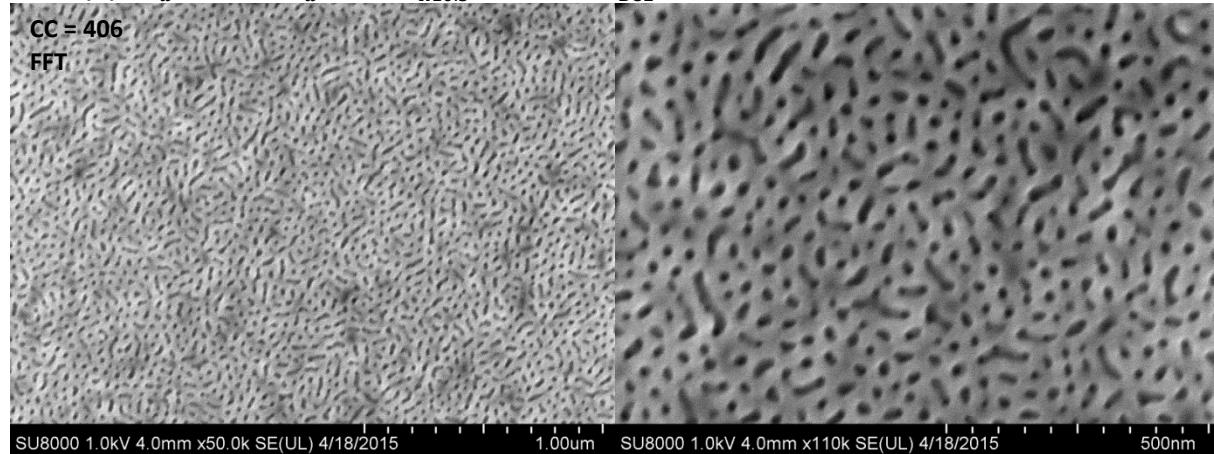


W26F (N-U) -  $h_{B82} \approx 44.5 \text{ nm}$  – DUV: E 10s, W 20s, **6c**

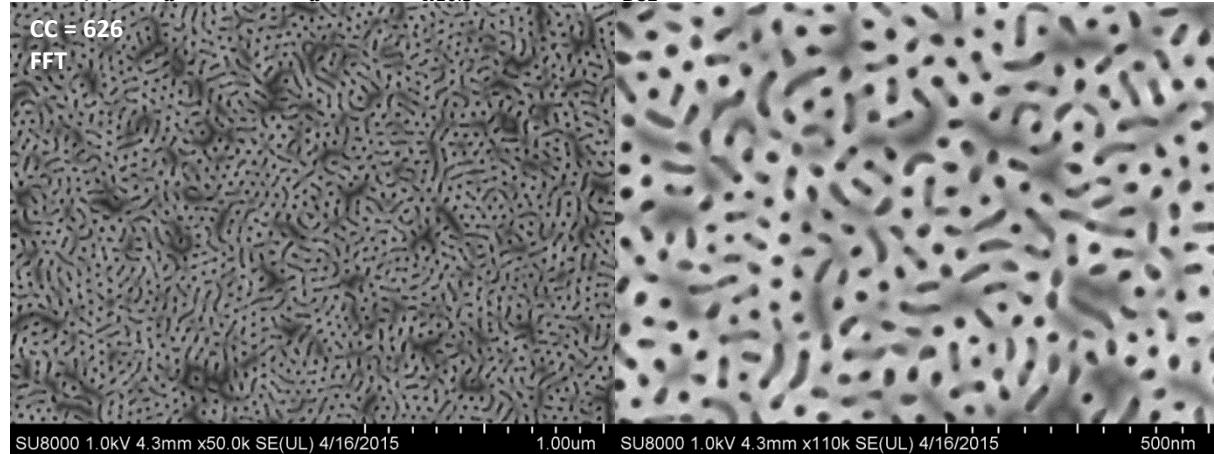


**A2.2 Effects of RTP  $T_a$  at  $t_a = 1$  h for B82 ( $h_{B82} \approx L_{0,B82}$ ) samples**

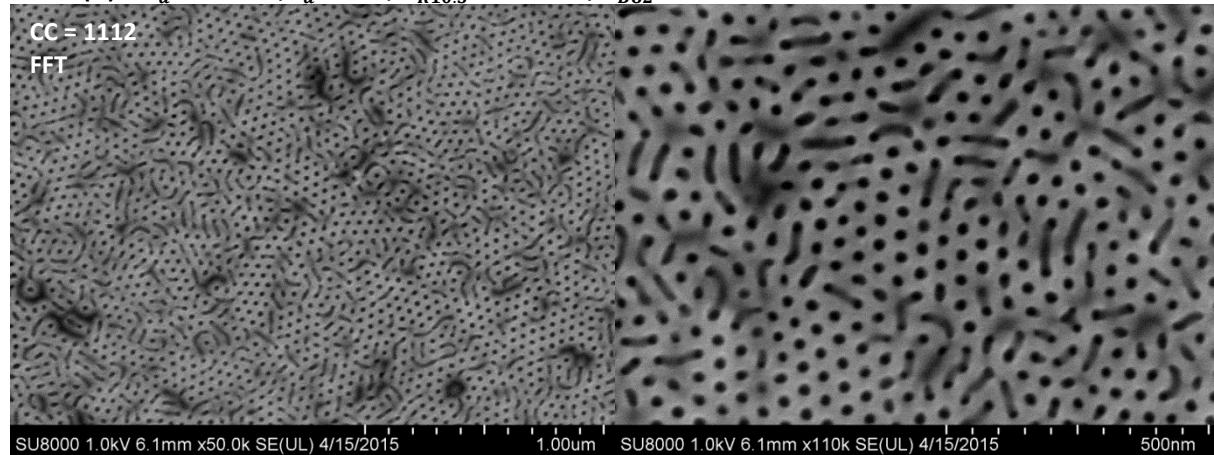
W15A (U) –  $T_a = 170^\circ\text{C}$ ,  $t_a = 1$  h;  $h_{R10.5} = 8.1$  nm;  $h_{B82} = 43.0$  nm



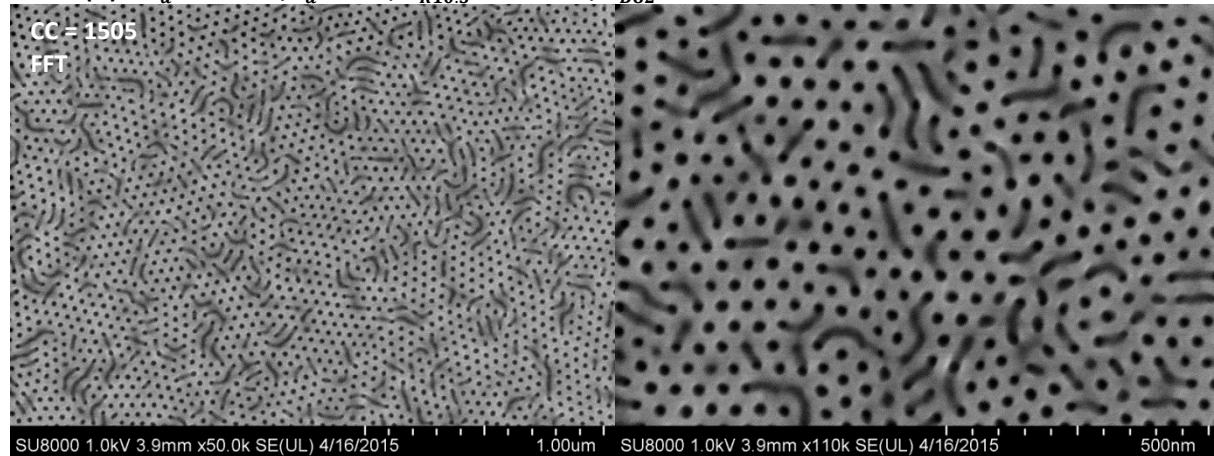
W15C (U) –  $T_a = 190^\circ\text{C}$ ,  $t_a = 1$  h;  $h_{R10.5} = 8.1$  nm;  $h_{B82} = 43.7$  nm



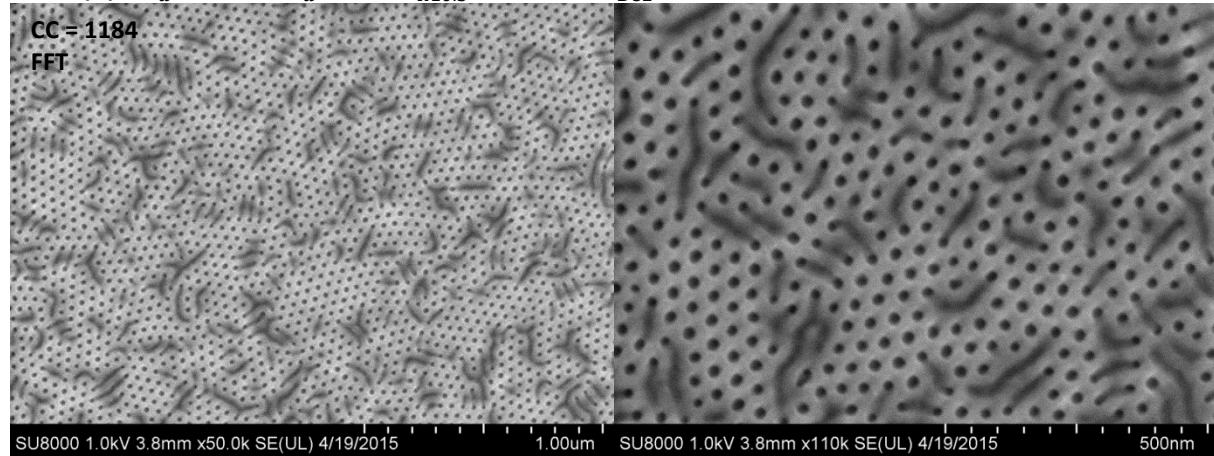
W15B (U) –  $T_a = 210^\circ\text{C}$ ,  $t_a = 1$  h;  $h_{R10.5} = 8.1$  nm;  $h_{B82} = 43.4$  nm



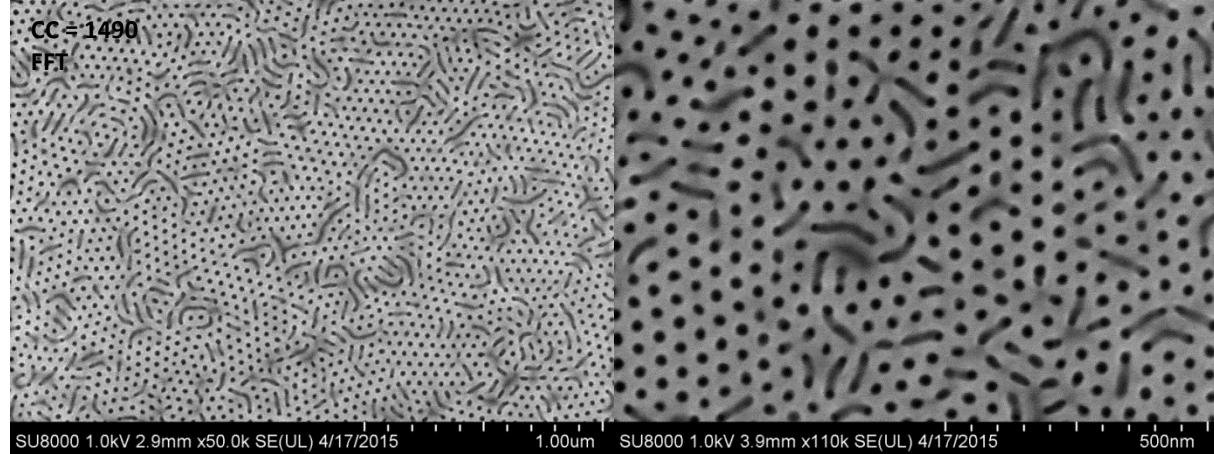
**W15D (U) –  $T_a = 230^\circ\text{C}$ ,  $t_a = 1 \text{ h}$ ;  $h_{R10.5} = 8.1 \text{ nm}$ ;  $h_{B82} = 43.1 \text{ nm}$**



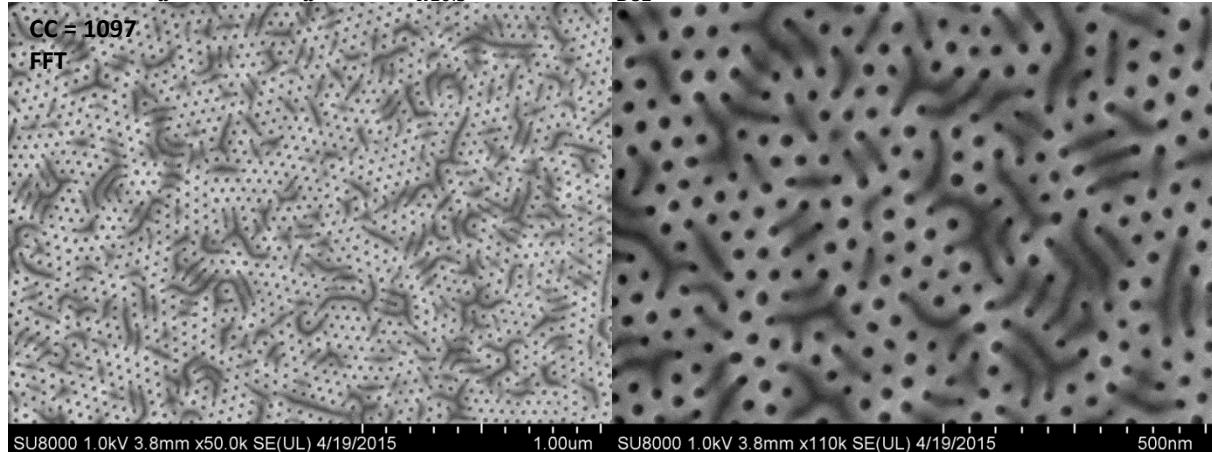
**W17B (U) –  $T_a = 240^\circ\text{C}$ ,  $t_a = 1 \text{ h}$ ;  $h_{R10.5} = 7.9 \text{ nm}$ ;  $h_{B82} = 37.8 \text{ nm}$**



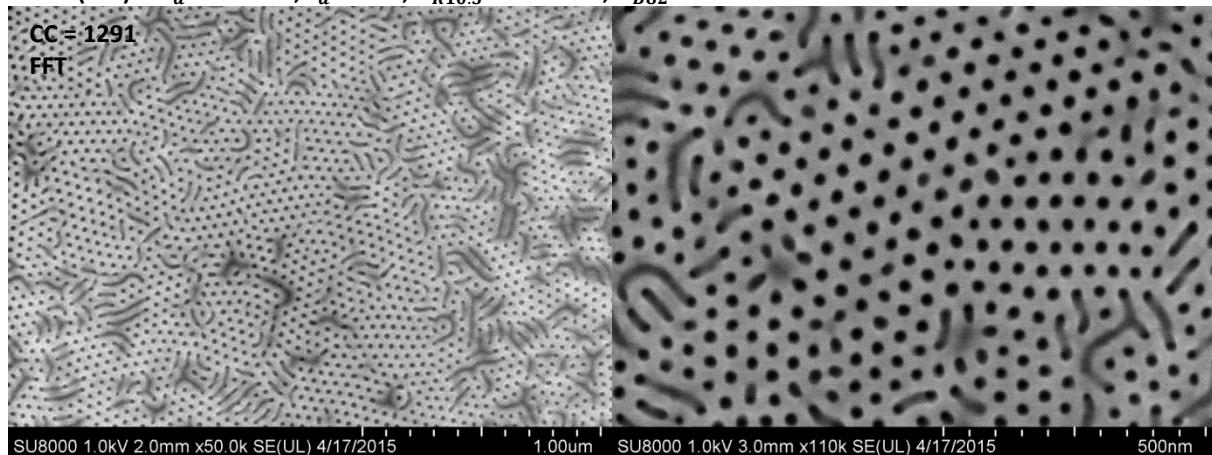
**W15E (U) –  $T_a = 250^\circ\text{C}$ ,  $t_a = 1 \text{ h}$ ;  $h_{R10.5} = 8.1 \text{ nm}$ ;  $h_{B82} = 43.2 \text{ nm}$**



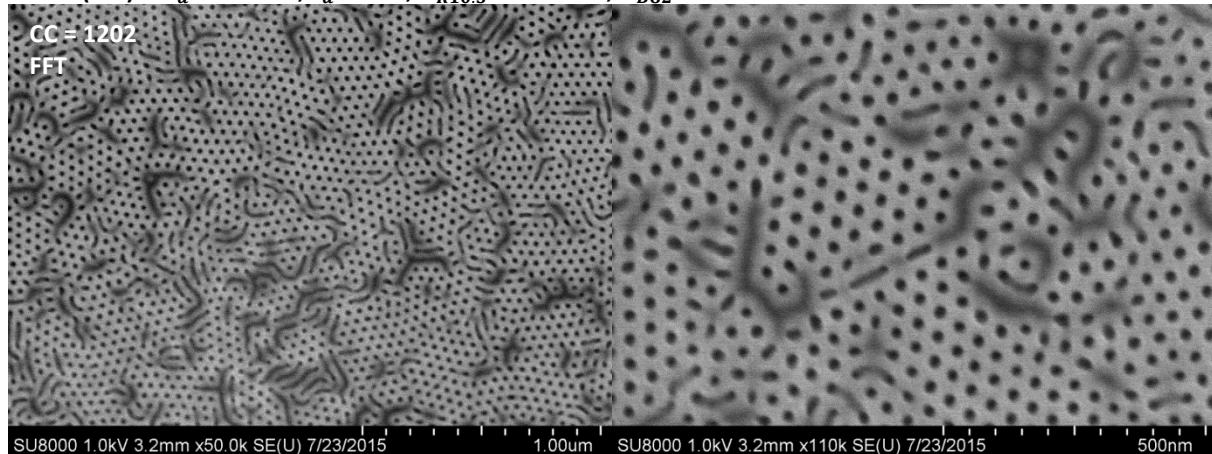
**W17A (U) –  $T_a = 260^\circ\text{C}$ ,  $t_a = 1 \text{ h}$ ;  $h_{R10.5} = 7.9 \text{ nm}$ ;  $h_{B82} = 37.6 \text{ nm}$**



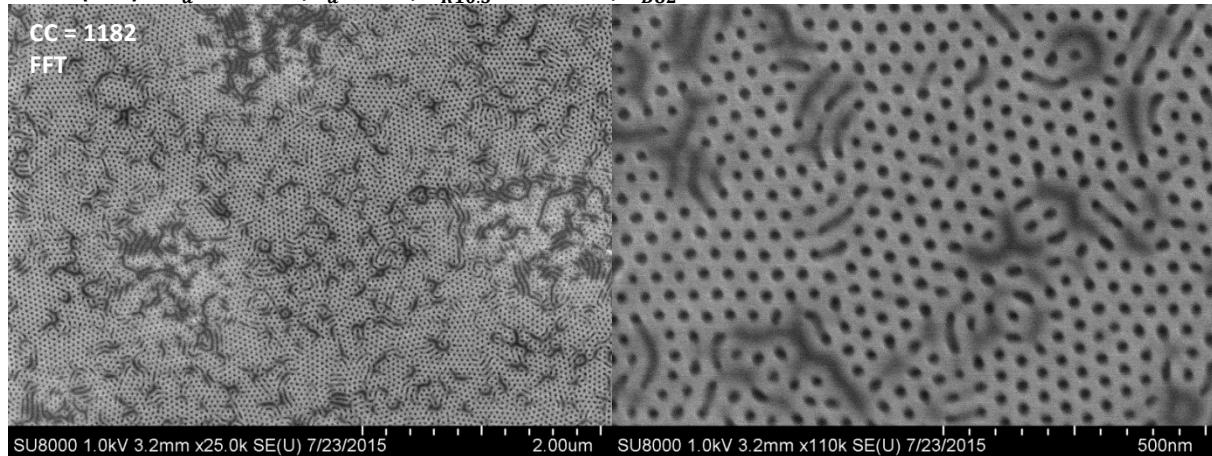
**W15F ( $\approx$ U) –  $T_a = 270^\circ\text{C}$ ,  $t_a = 1 \text{ h}$ ;  $h_{R10.5} = 8.1 \text{ nm}$ ;  $h_{B82} = 43.1 \text{ nm}$**



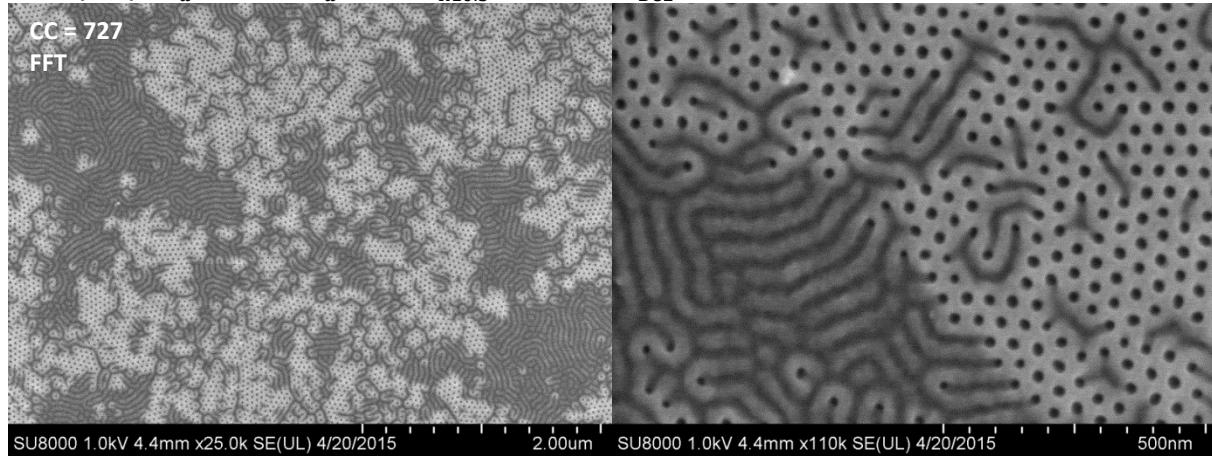
**W40A ( $\approx$ U) –  $T_a = 270^\circ\text{C}$ ,  $t_a = 1 \text{ h}$ ;  $h_{R10.5} = 7.7 \text{ nm}$ ;  $h_{B82} = 45.5 \text{ nm}$**



**W40B (N-U) –  $T_a = 280^\circ\text{C}$ ,  $t_a = 1 \text{ h}$ ;  $h_{R10.5} = 7.7 \text{ nm}$ ;  $h_{B82} = 45.5 \text{ nm}$**

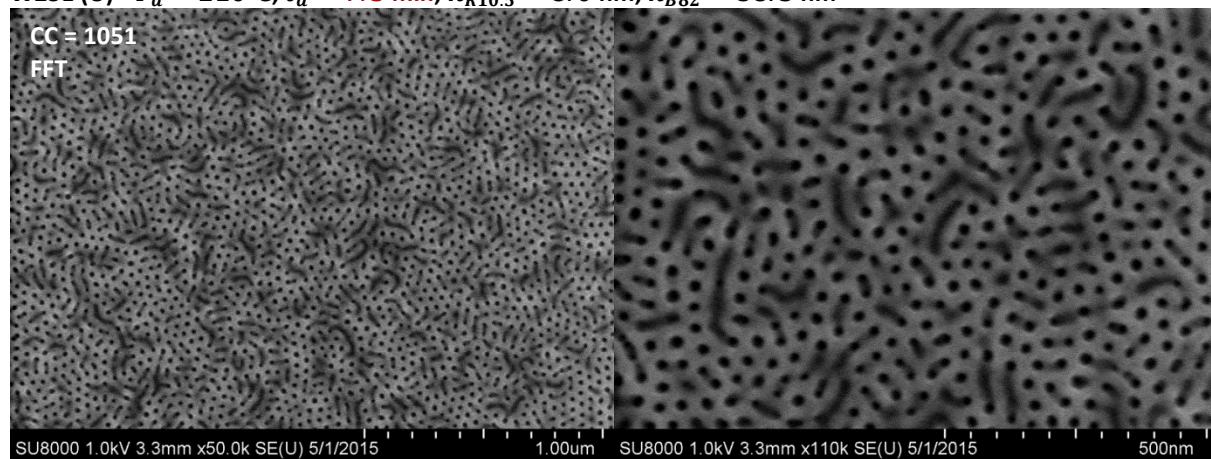


**W17F (N-U) –  $T_a = 290^\circ\text{C}$ ,  $t_a = 1 \text{ h}$ ;  $h_{R10.5} = 7.9 \text{ nm}$ ;  $h_{B82} = 37.1 \text{ nm}$**

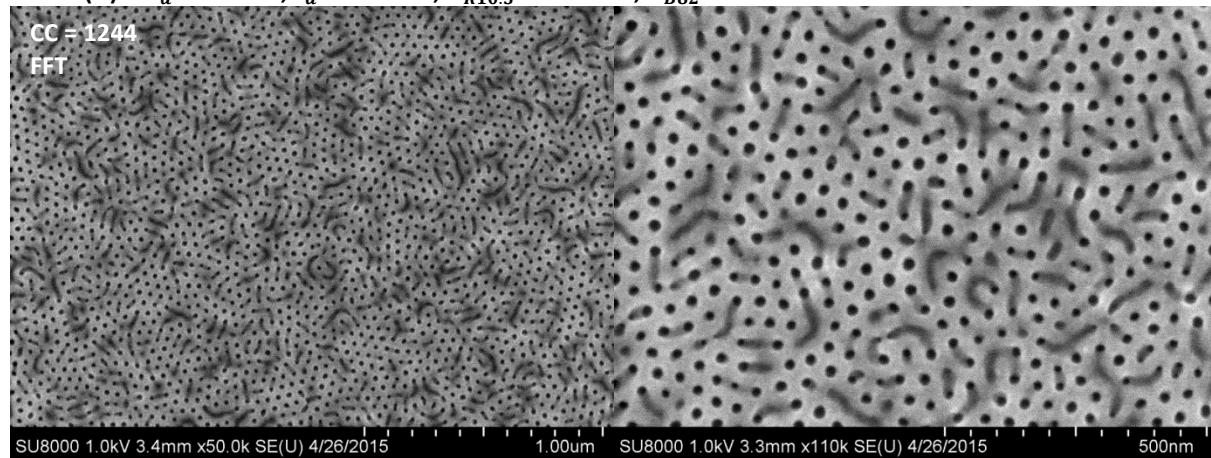


**A2.3 Effects of RTP  $t_a$  at  $T_a = 210^\circ\text{C}$  for B82 ( $h_{B82} \approx L_{0,B82}$ ) samples**

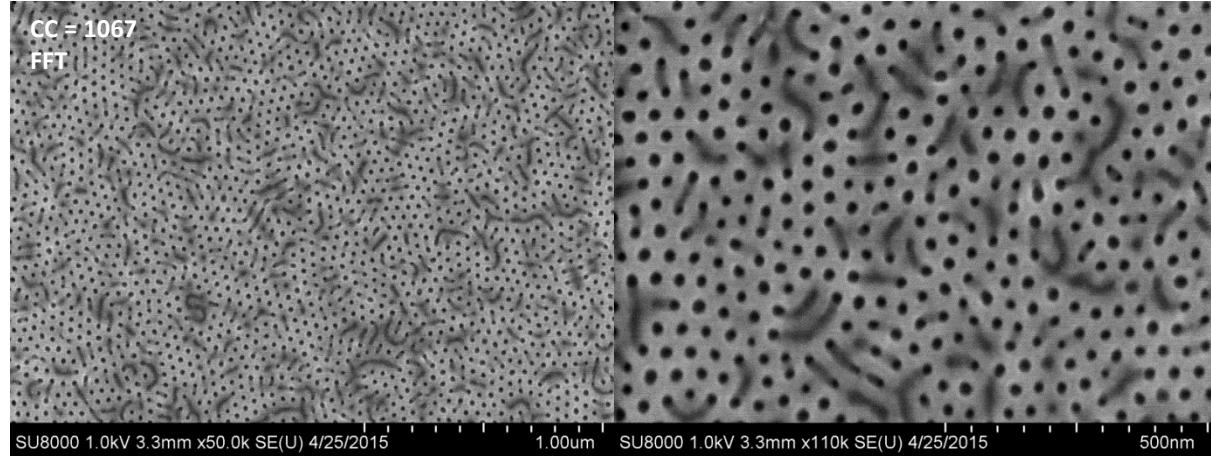
W23E (U) -  $T_a = 210^\circ\text{C}$ ,  $t_a = 7.5$  min;  $h_{R10.5} = 8.0$  nm;  $h_{B82} = 38.5$  nm



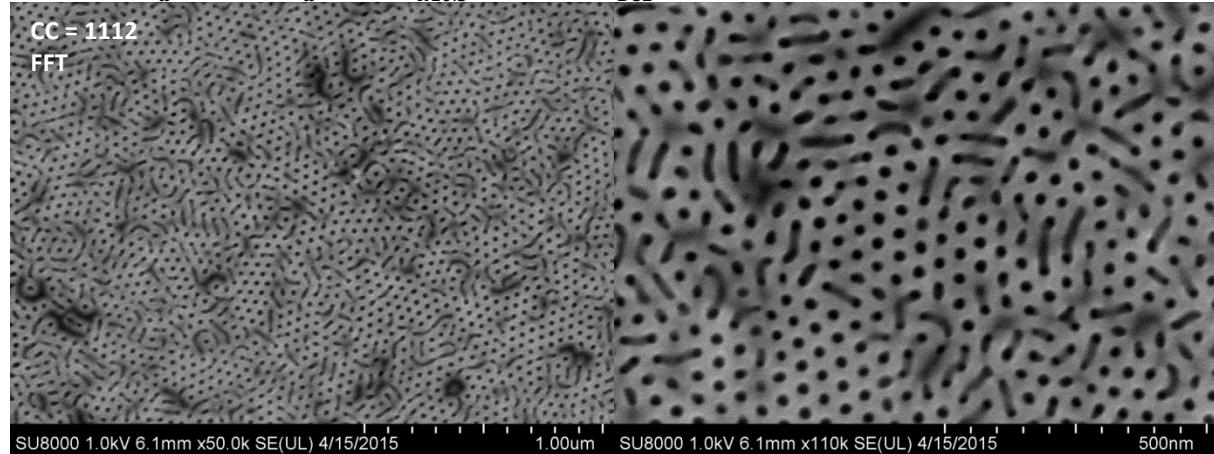
W21D (U) -  $T_a = 210^\circ\text{C}$ ,  $t_a = 15$  min;  $h_{R10.5} = 7.7$  nm;  $h_{B82} = 39.0$  nm



W21A (U) -  $T_a = 210^\circ\text{C}$ ,  $t_a = 30$  min;  $h_{R10.5} = 7.7$  nm;  $h_{B82} = 39.3$  nm

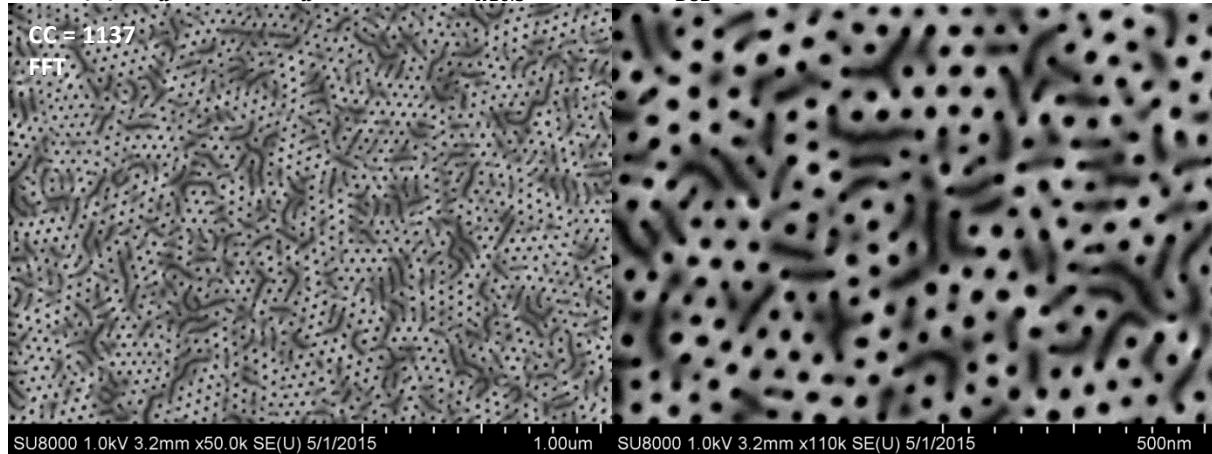


**W15B (U) –  $T_a = 210^\circ\text{C}$ ,  $t_a = 1 \text{ h}$ ;  $h_{R10.5} = 8.1 \text{ nm}$ ;  $h_{B82} = 43.4 \text{ nm}$**

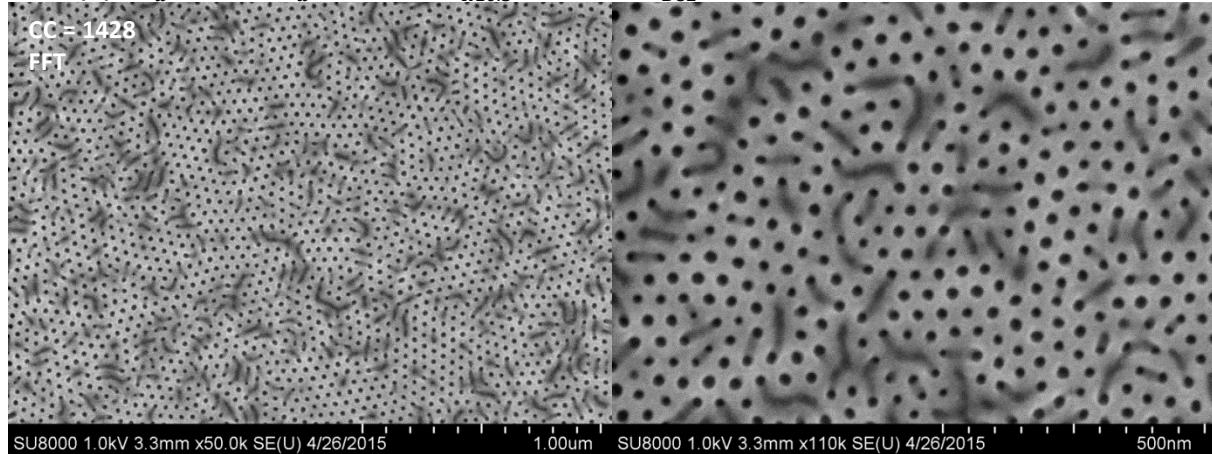


**A2.4 Effects of RTP  $t_a$  at  $T_a = 230^\circ\text{C}$  for B82 ( $h_{B82} \approx L_{0,B82}$ ) samples**

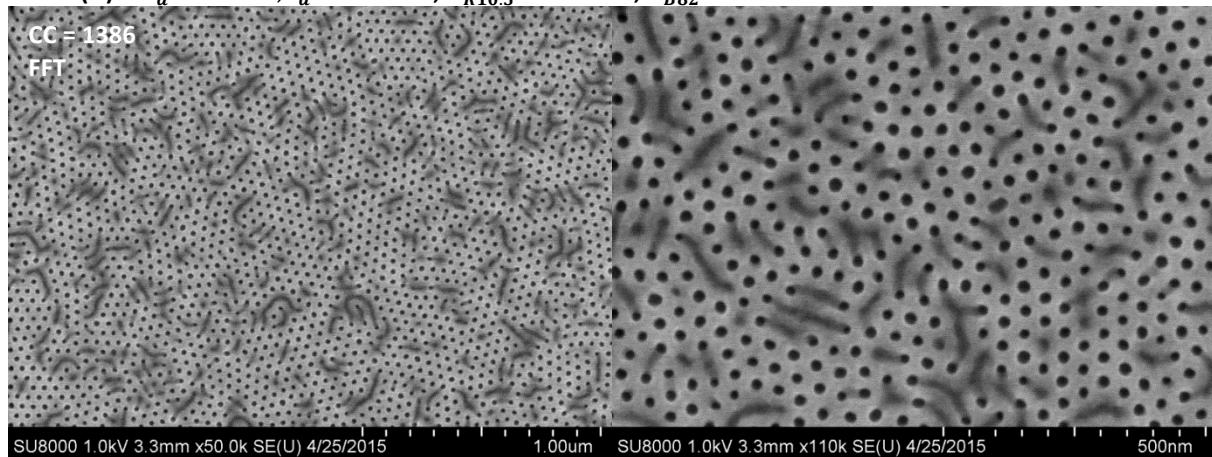
W23D (U) –  $T_a = 230^\circ\text{C}$ ,  $t_a = 7.5$  min;  $h_{R10.5} = 8.0$  nm;  $h_{B82} = 38.6$  nm



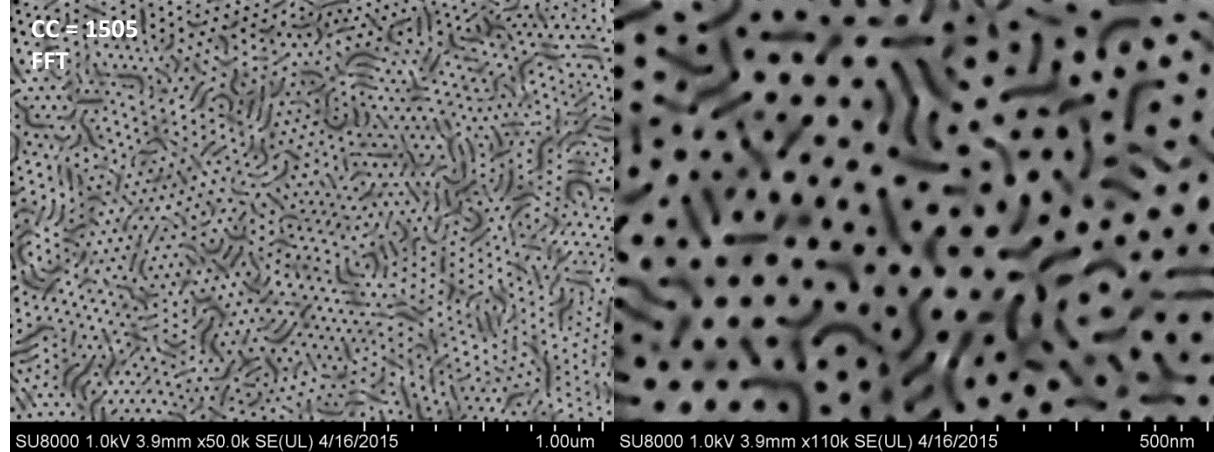
W21E (U) –  $T_a = 230^\circ\text{C}$ ,  $t_a = 15$  min;  $h_{R10.5} = 7.7$  nm;  $h_{B82} = 39.1$  nm



W21B (U) –  $T_a = 230^\circ\text{C}$ ,  $t_a = 30$  min;  $h_{R10.5} = 7.7$  nm;  $h_{B82} = 39.2$  nm

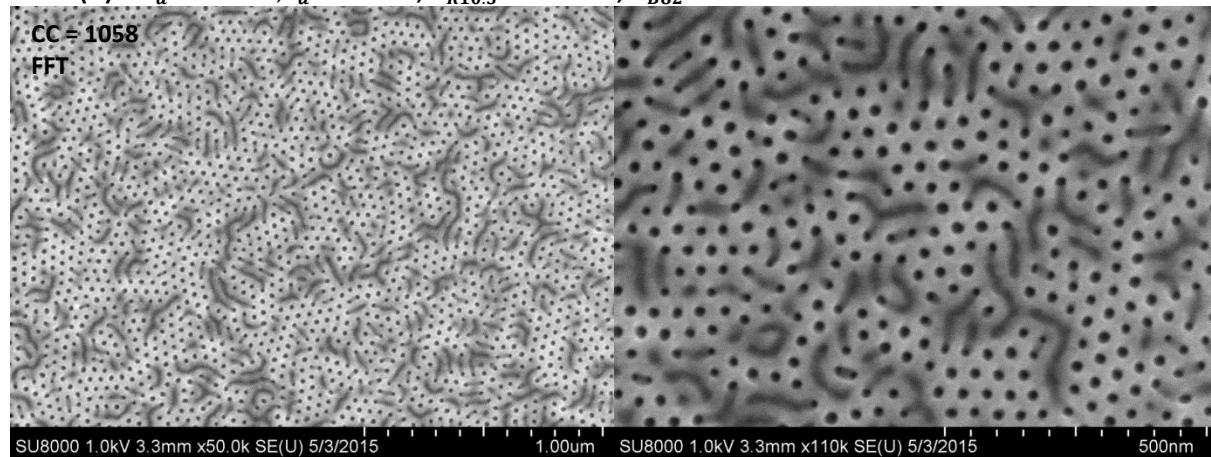


**W15D (U) –  $T_a = 230^\circ\text{C}$ ,  $t_a = 1 \text{ h}$ ;  $h_{R10.5} = 8.1$ ;  $h_{B82} = 43.1 \text{ nm}$**

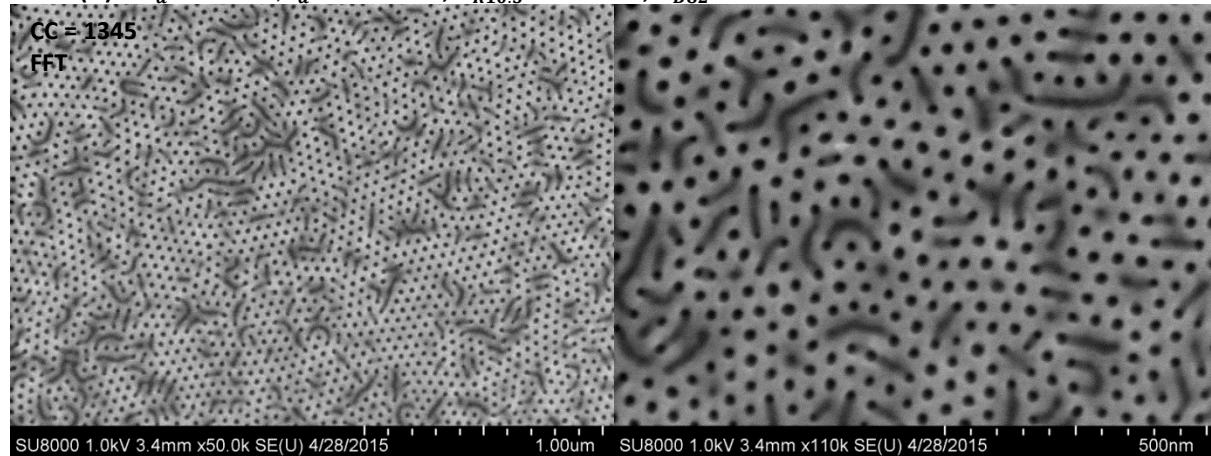


**A2.5 Effects of RTP  $t_a$  at  $T_a = 250^\circ\text{C}$  for B82 ( $h_{B82} \approx L_{0,B82}$ ) samples**

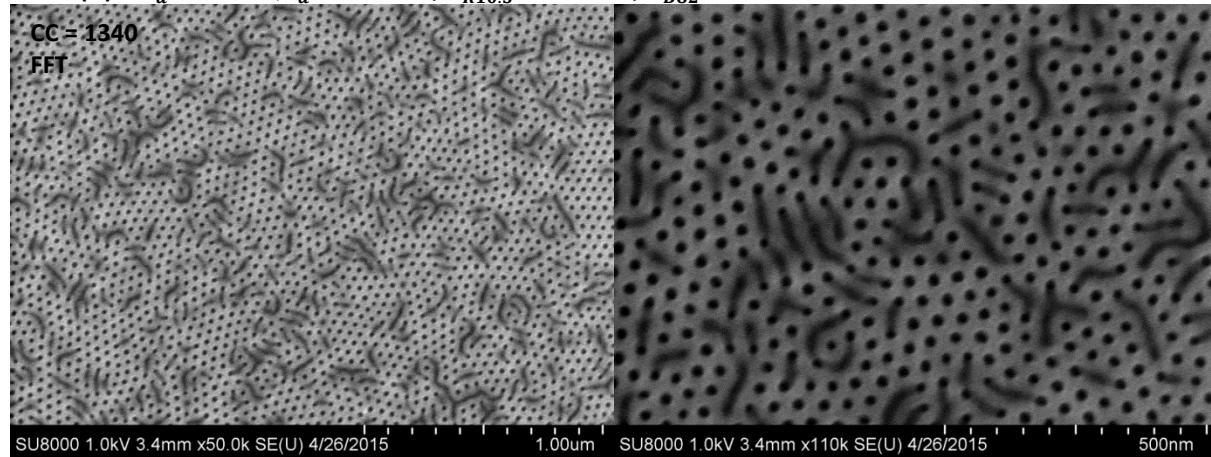
W23F (U) –  $T_a = 250^\circ\text{C}$ ,  $t_a = 3$  min;  $h_{R10.5} = 8.0$  nm;  $h_{B82} = 38.8$  nm



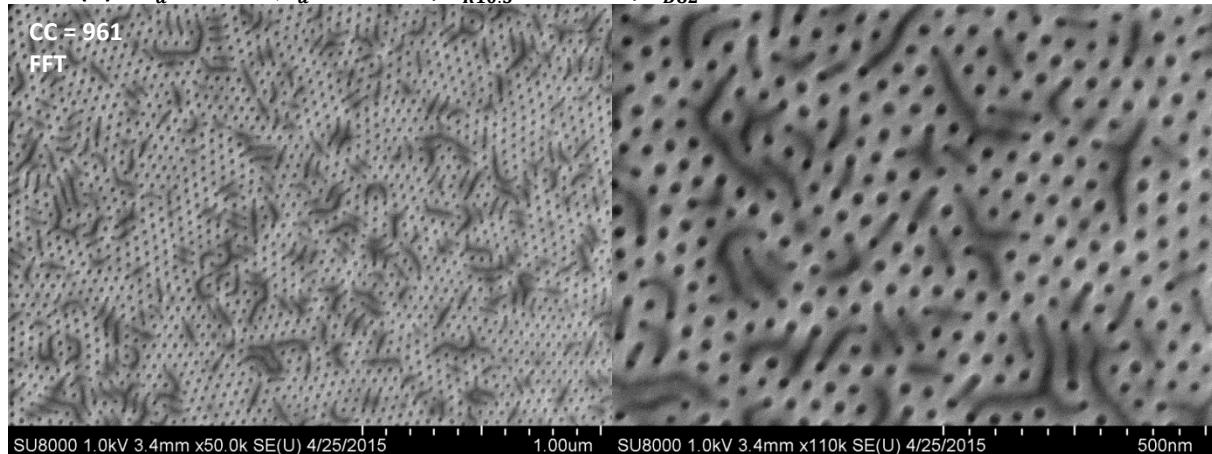
W22F (U) –  $T_a = 250^\circ\text{C}$ ,  $t_a = 7.5$  min;  $h_{R10.5} = 8.1$  nm;  $h_{B82} = 39.4$  nm



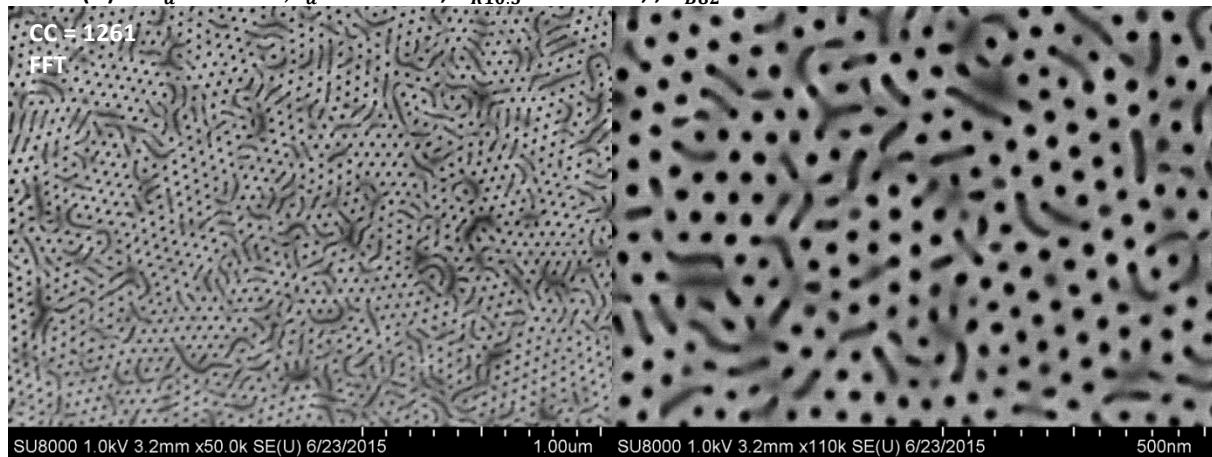
W21F (U) –  $T_a = 250^\circ\text{C}$ ,  $t_a = 15$  min;  $h_{R10.5} = 7.7$  nm;  $h_{B82} = 39.5$  nm



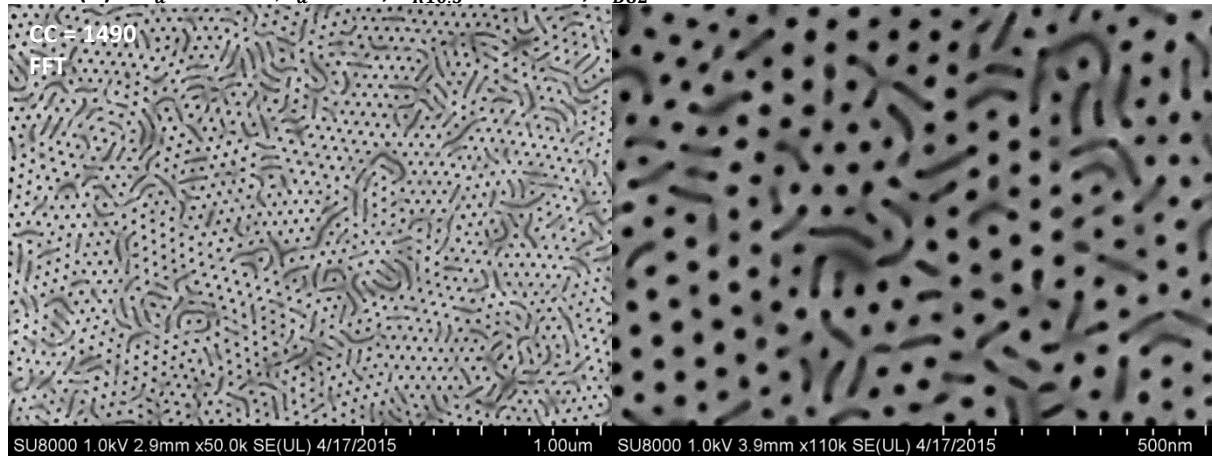
**W21C (U) –  $T_a = 250^\circ\text{C}$ ,  $t_a = \text{30 min}$ ;  $h_{R10.5} = 7.7 \text{ nm}$ ;  $h_{B82} = 39.4 \text{ nm}$**



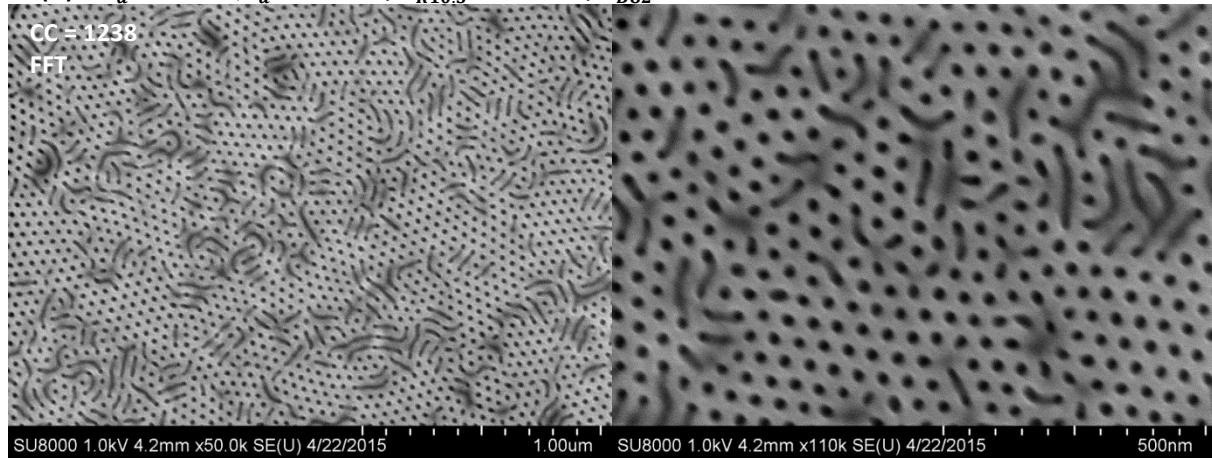
**W39A (U) –  $T_a = 250^\circ\text{C}$ ,  $t_a = \text{30 min}$ ;  $h_{R10.5} = 7.8 \text{ nm}$ ;  $h_{B82} = 44.9 \text{ nm}$**



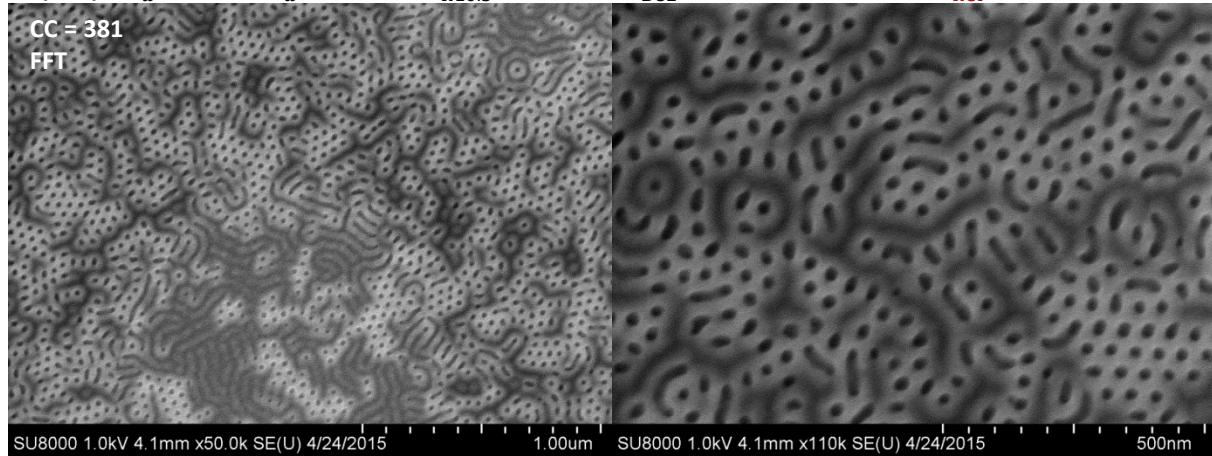
**W15E (U) –  $T_a = 250^\circ\text{C}$ ,  $t_a = \text{1 h}$ ;  $h_{R10.5} = 8.1 \text{ nm}$ ;  $h_{B82} = 43.2 \text{ nm}$**



S4 (U) –  $T_a = 250^\circ\text{C}$ ,  $t_a = 2 \times 1 \text{ h}$ ;  $h_{R10.5} = 6.9 \text{ nm}$ ;  $h_{B82} = 45.7 \text{ nm}$

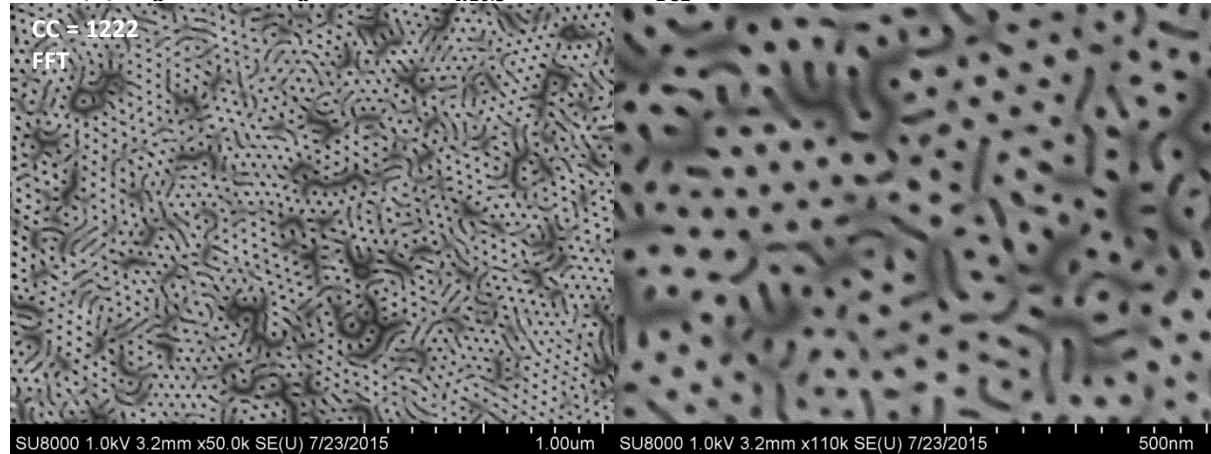


S5 (N-U) –  $T_a = 250^\circ\text{C}$ ,  $t_a = 3 \times 1 \text{ h}$ ;  $h_{R10.5} = 6.0 \text{ nm}$ ;  $h_{B82} = 46.3 \text{ nm}$  – NB: Low  $h_{RCP}$  value!

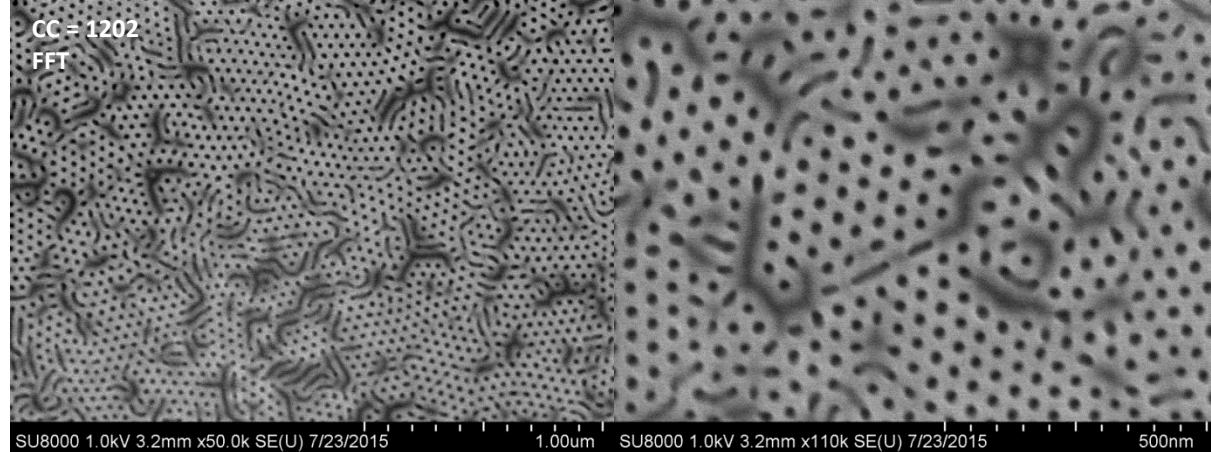


**A2.6 Effects of RTP  $t_a$  at  $T_a = 270^\circ\text{C}$  for B82 ( $h_{B82} \approx L_{0,B82}$ ) samples**

W40C (U) -  $T_a = 270^\circ\text{C}$ ,  $t_a = 15$  min;  $h_{R10.5} = 7.7$  nm;  $h_{B82} = 45.5$  nm

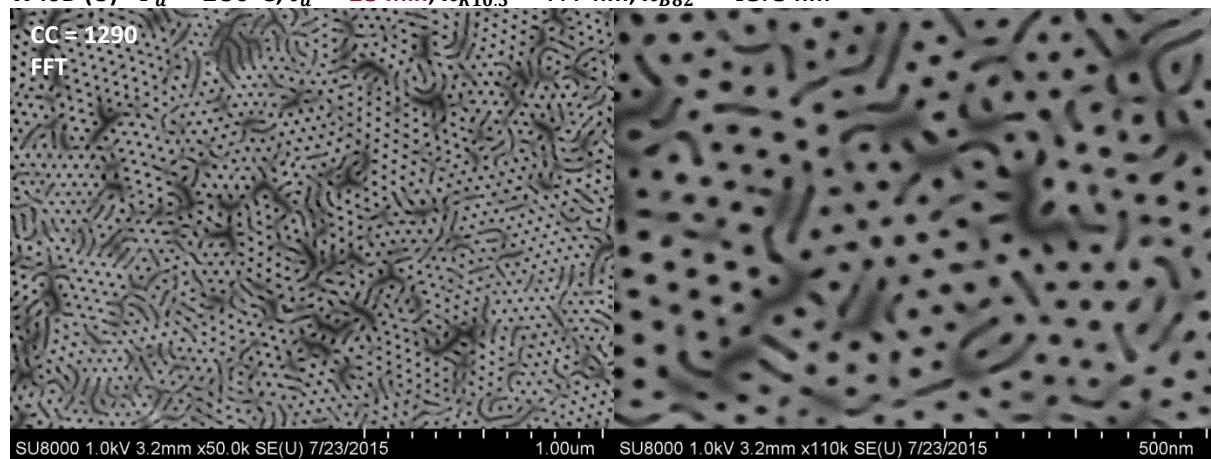


W40A ( $\approx$ U) -  $T_a = 270^\circ\text{C}$ ,  $t_a = 1$  h;  $h_{R10.5} = 7.7$  nm;  $h_{B82} = 45.5$  nm

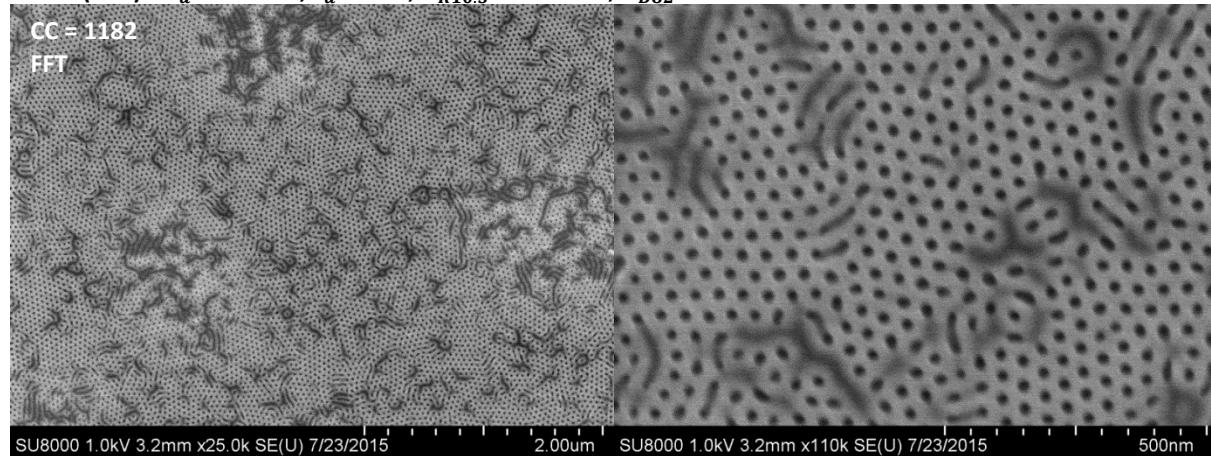


**A2.7 Effects of RTP  $t_a$  at  $T_a = 280^\circ\text{C}$  for B82 ( $h_{B82} \approx L_{0,B82}$ ) samples**

W40D (U) -  $T_a = 280^\circ\text{C}$ ,  $t_a = 15$  min;  $h_{R10.5} = 7.7$  nm;  $h_{B82} = 45.5$  nm

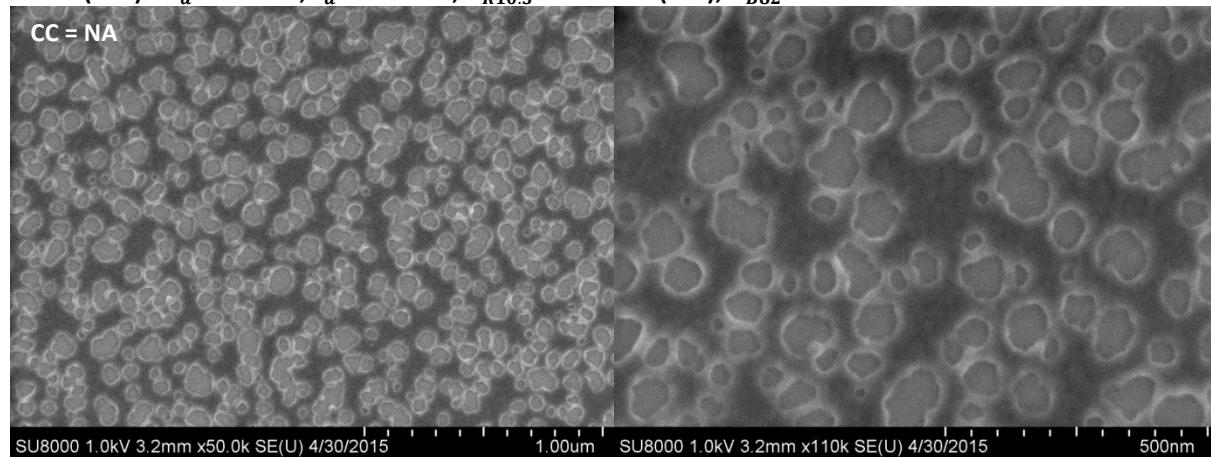


W40B (N-U) -  $T_a = 280^\circ\text{C}$ ,  $t_a = 1$  h;  $h_{R10.5} = 7.7$  nm;  $h_{B82} = 45.5$  nm

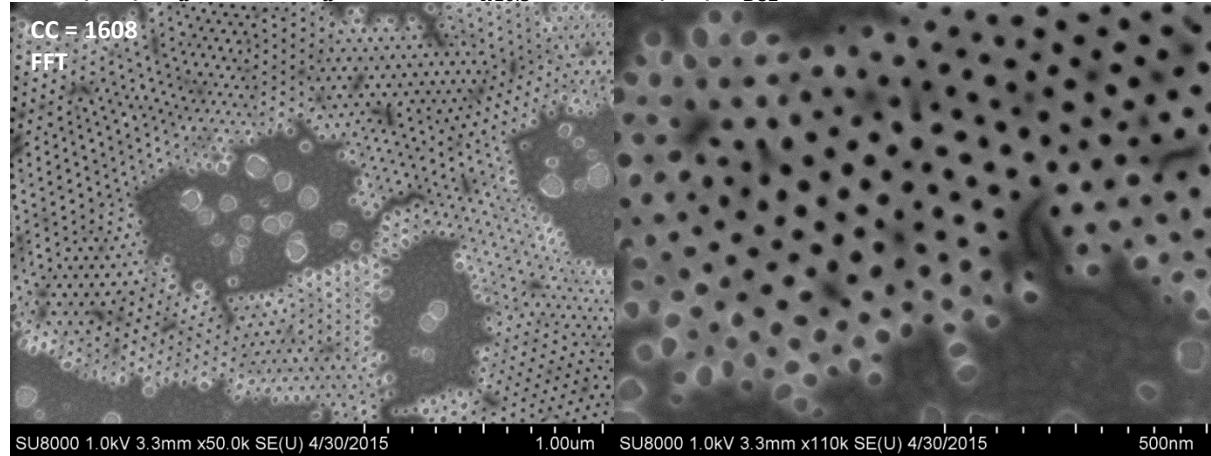


**A2.8** Importance of  $h_{B82}$  on morphology orientation after RTP anneal of B82 samples

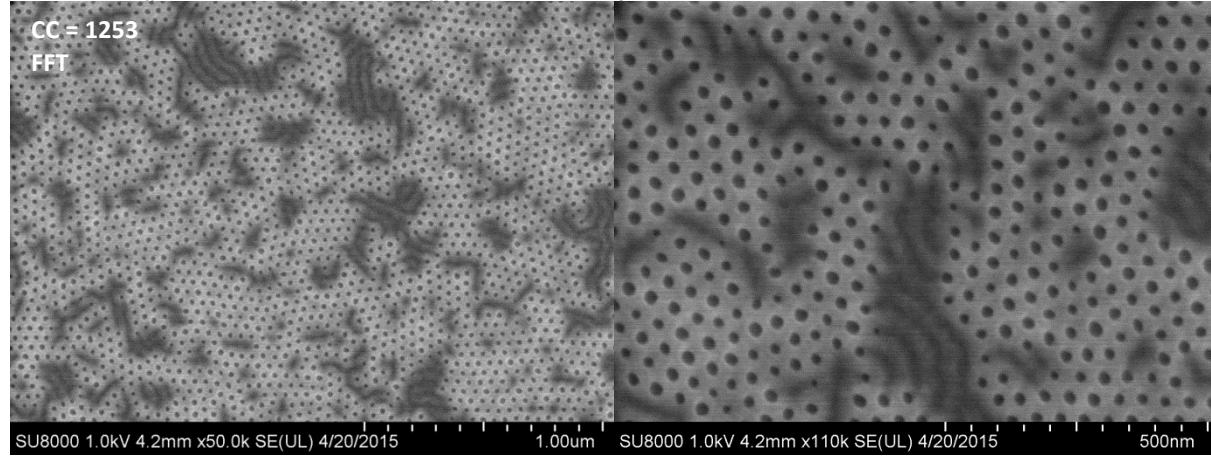
W24A (N-U) -  $T_a = 250^\circ\text{C}$ ;  $t_a = 15 \text{ min}$ ;  $h_{R10.5} = 8.5 \text{ nm (AW)}$ ;  $h_{B82} = 17.8 \text{ nm}$



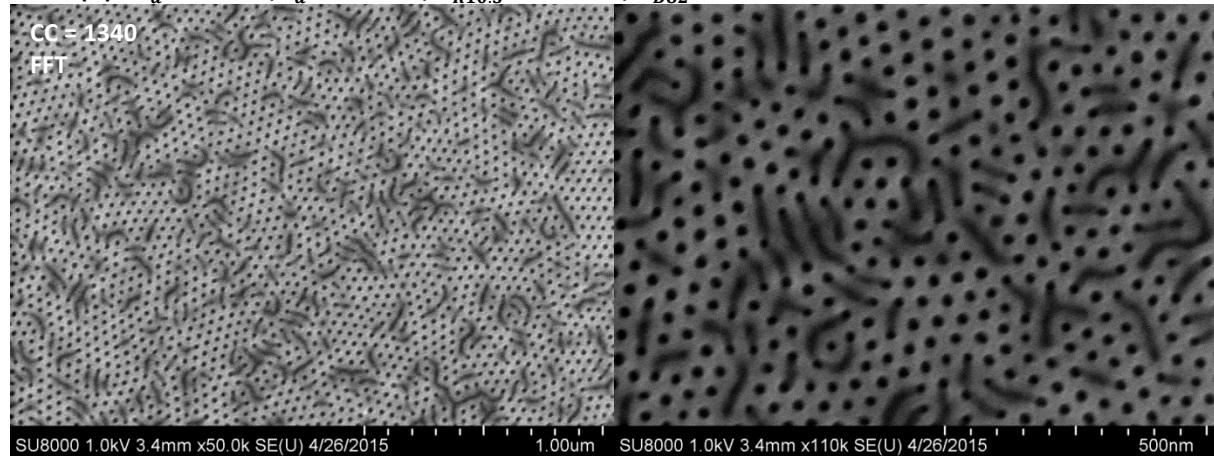
W24C (N-U) -  $T_a = 250^\circ\text{C}$ ;  $t_a = 15 \text{ min}$ ;  $h_{R10.5} = 8.4 \text{ nm (AW)}$ ;  $h_{B82} = 27.6 \text{ nm}$



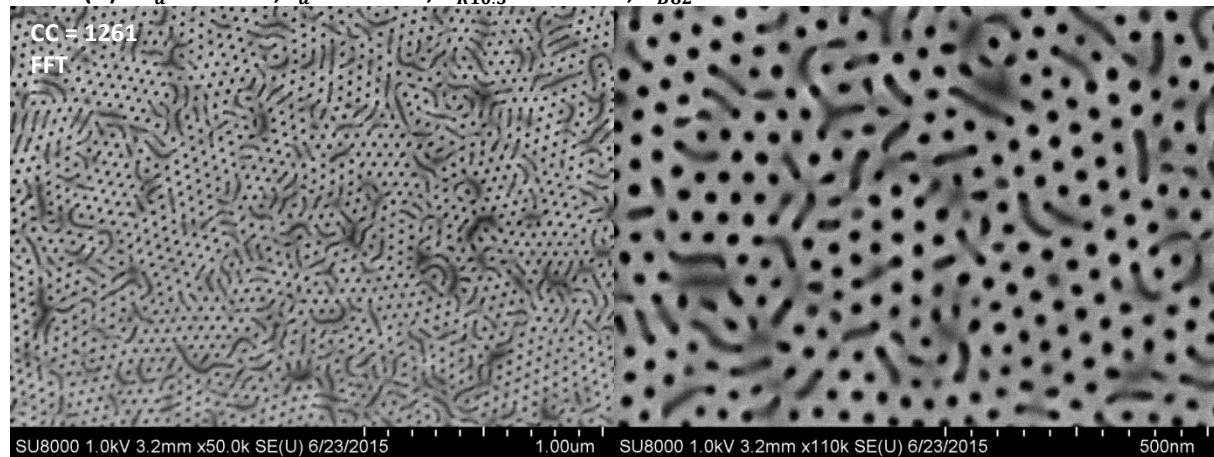
D18 (=U) -  $T_a = 250^\circ\text{C}$ ;  $t_a = 1 \text{ h}$ ;  $h_{R10.5} \leq 7.9 \text{ nm}$ ;  $h_{B82} = 31.7 \text{ nm}$



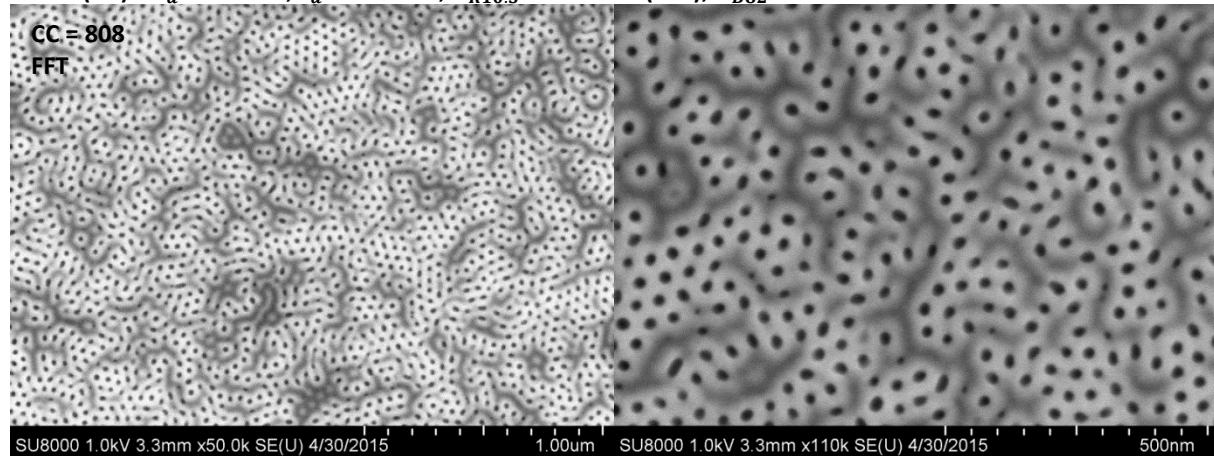
**W21F (U) -  $T_a = 250^\circ\text{C}$ ;  $t_a = 15 \text{ min}$ ;  $h_{R10.5} = 7.7 \text{ nm}$ ;  $h_{B82} = 39.5 \text{ nm}$**



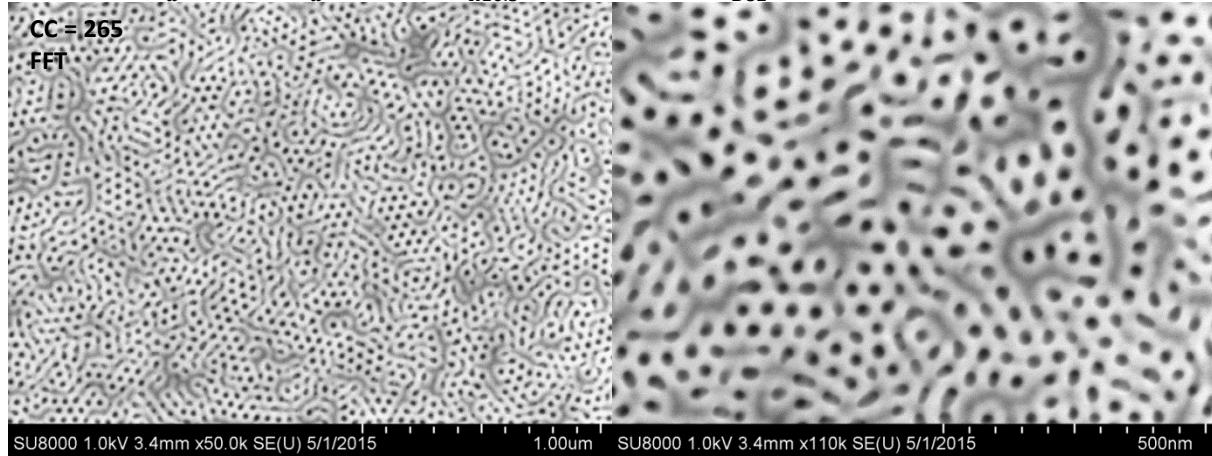
**W39A (U) -  $T_a = 250^\circ\text{C}$ ;  $t_a = 30 \text{ min}$ ;  $h_{R10.5} = 7.8 \text{ nm}$ ;  $h_{B82} = 44.9 \text{ nm}$**



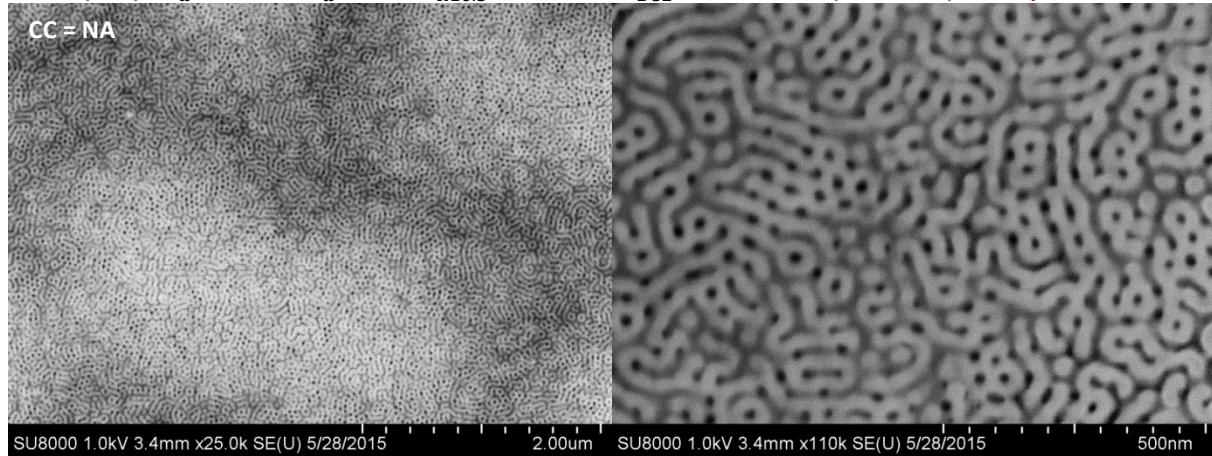
**W24B ( $\approx$ U) -  $T_a = 250^\circ\text{C}$ ;  $t_a = 15 \text{ min}$ ;  $h_{R10.5} = 8.1 \text{ nm (AW)}$ ;  $h_{B82} = 60.9 \text{ nm}$**



**W24D ( $\approx$ U) -  $T_a = 250^\circ\text{C}$ ;  $t_a = 15 \text{ min}$ ;  $h_{R10.5} = 8.0 \text{ nm (AW)}$ ;  $h_{B82} = 92.1 \text{ nm}$**

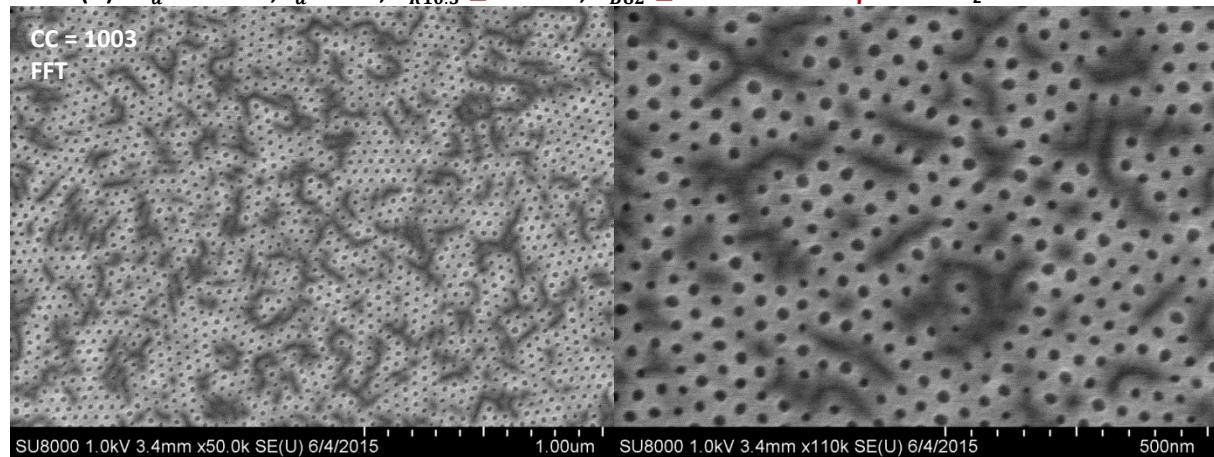


**W33D (N-U) -  $T_a = 250^\circ\text{C}$ ;  $t_a = 1 \text{ h}$ ;  $h_{R10.5} = 8.7 \text{ nm}$ ;  $h_{B82} = 126.2 \text{ nm (MSE = 8.1)}$  – 14 s pre-dev. O<sub>2</sub> RIE**

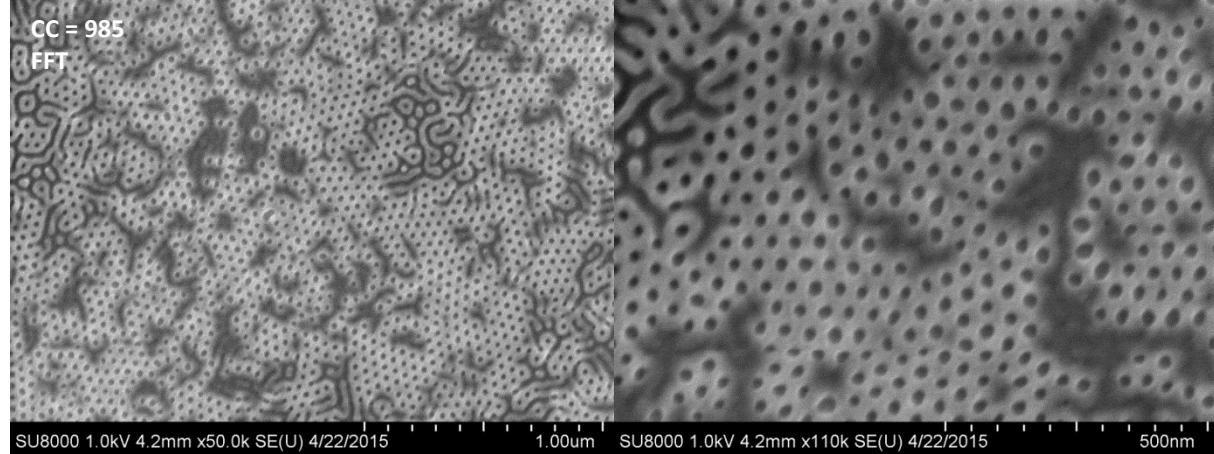


**A2.9 Effects of Pre-/Post-development O<sub>2</sub> plasma thinning of B82 samples**

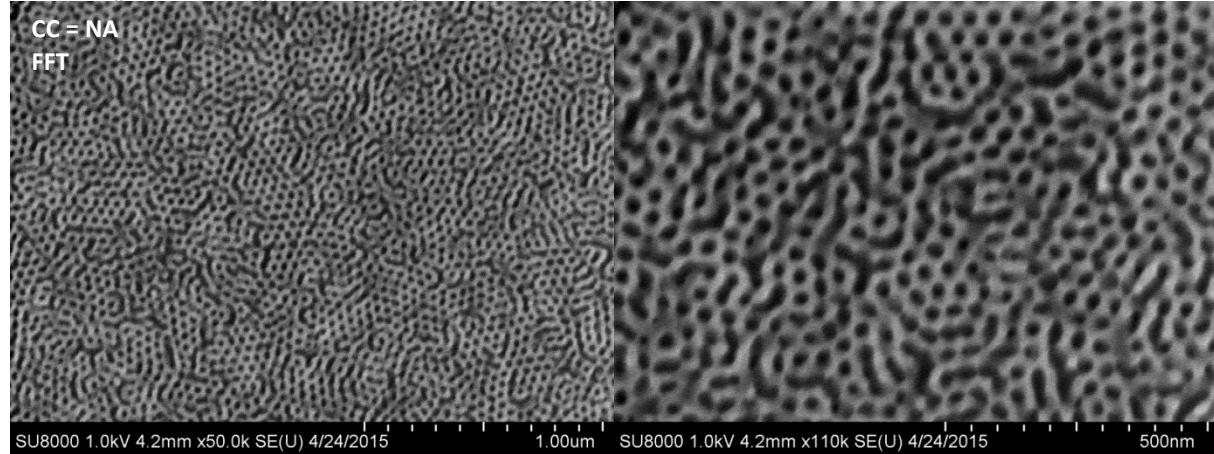
W33E (U) -  $T_a = 250^\circ\text{C}$ ;  $t_a = 1 \text{ h}$ ;  $h_{R10.5} \leq 8.7 \text{ nm}$ ;  $h_{B82} \geq 40.8 \text{ nm}$  – **10 s pre-dev. O<sub>2</sub> RIE**



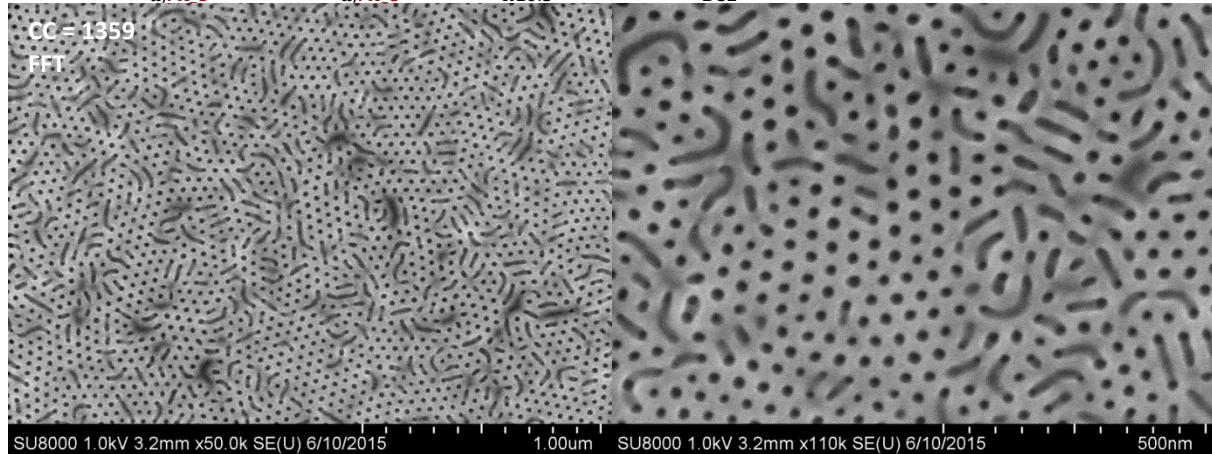
S6 (N-U) -  $T_a = 250^\circ\text{C}$ ;  $t_a = 1 \text{ h}$ ;  $h_{R10.5} = 6.6 \text{ nm}$ ;  $h_{B82} = 41.0 \text{ nm}$  – **15 s pre-dev. O<sub>2</sub> RIE**



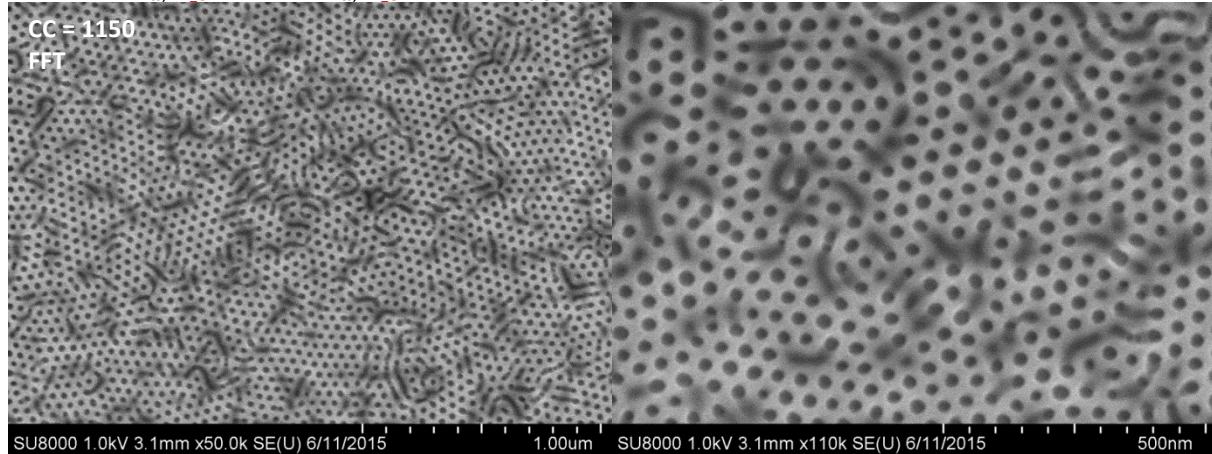
S7 (U) -  $T_a = 250^\circ\text{C}$ ;  $t_a = 1 \text{ h}$ ;  $h_{R10.5} = 6.7 \text{ nm}$ ;  $h_{B82} = 85.8 \text{ nm}$  – **60 s pre-dev. O<sub>2</sub> RIE**



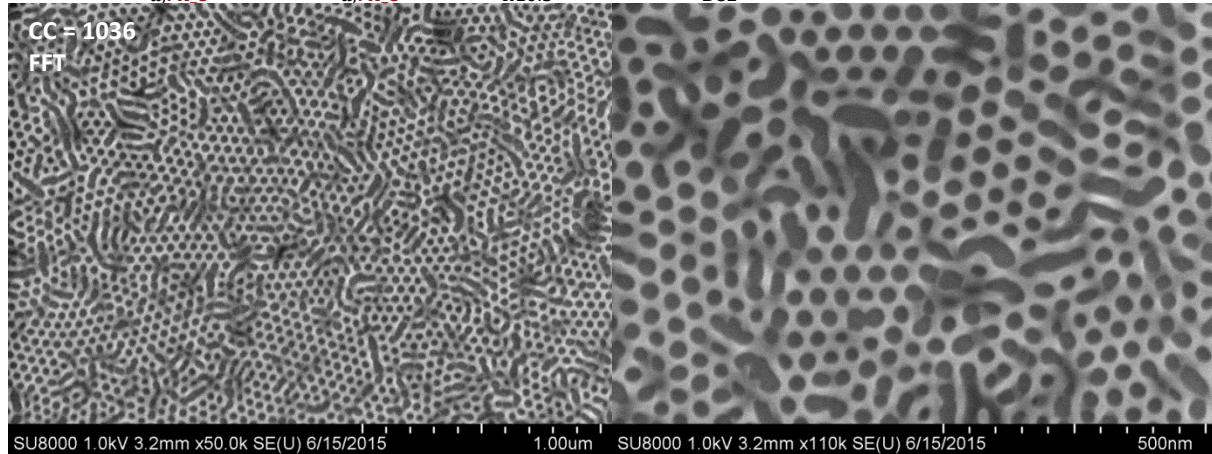
**W35C (U) -  $T_{a,VA,C} = 190^\circ\text{C}$ ;  $t_{a,VA,C} = 2 \text{ h}$ ;  $h_{R10.5} = 8.5 \text{ nm}$ ;  $h_{B82} = 42.4 \text{ nm}$  – No pre/post-dev. O<sub>2</sub> RIE**



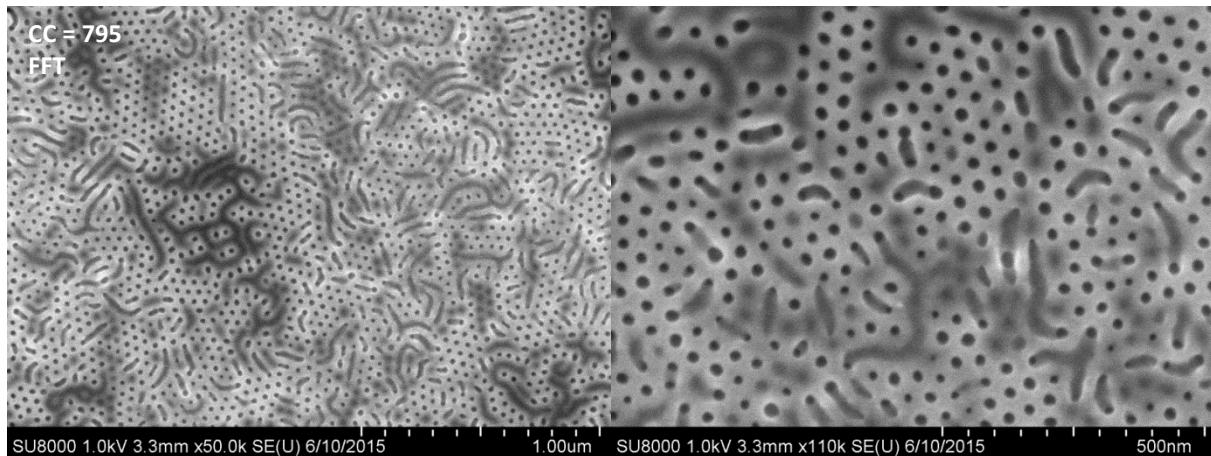
**W35C (U) -  $T_{a,VA,C} = 190^\circ\text{C}$ ;  $t_{a,VA,C} = 2 \text{ h}$ ;  $h_{R10.5} = 8.5 \text{ nm}$ ;  $h_{B82} = 42.4 \text{ nm}$  – 12 s post-dev. O<sub>2</sub> RIE**



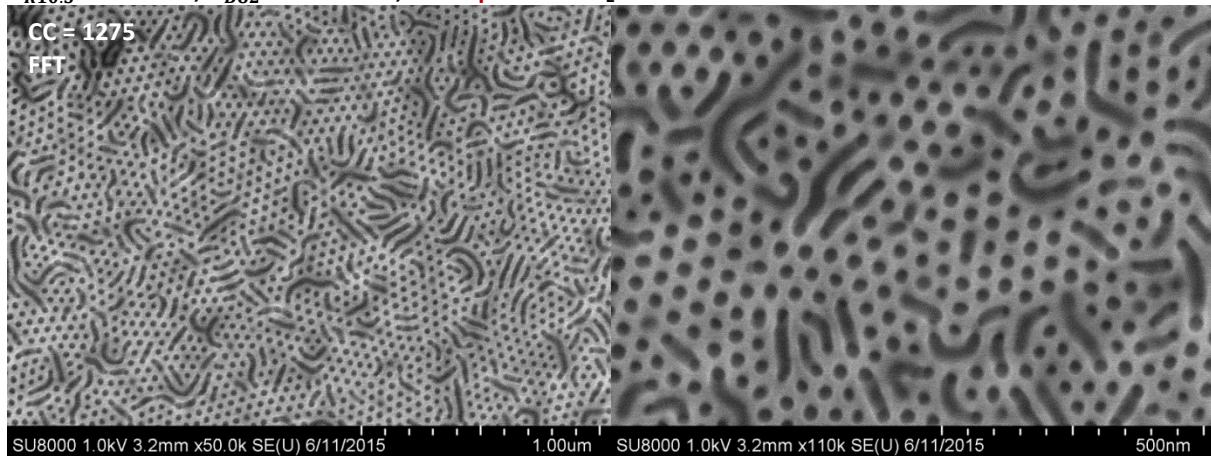
**W35C (U) -  $T_{a,VA,C} = 190^\circ\text{C}$ ;  $t_{a,VA,C} = 2 \text{ h}$ ;  $h_{R10.5} = 8.5 \text{ nm}$ ;  $h_{B82} = 42.4 \text{ nm}$  – 12 s + 12 s post-dev. O<sub>2</sub> RIE**



**W33F (N-U) -  $T_{a,RTP} = 250^\circ\text{C}$ ;  $t_{a,RTP} = 30 \text{ min}$ ;  $T_{a,VA\_C} = 190^\circ\text{C}$ ;  $t_{a,VA\_C} = 2 \text{ h}$ ;  $h_{R10.5} \leq 8.7 \text{ nm}$ ;  $h_{B82} = 41.7 \text{ nm}$**

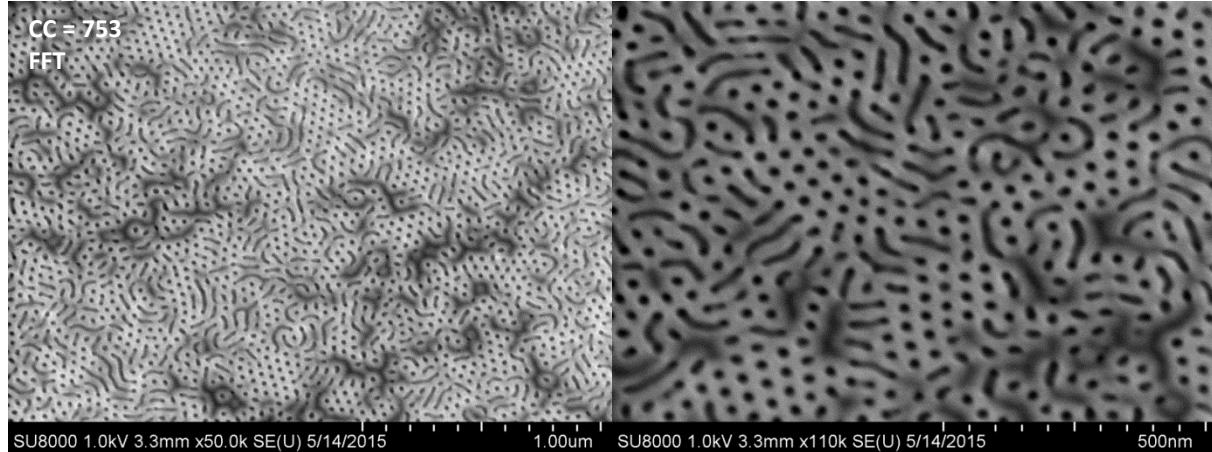


**W33F ( $\approx$ U) -  $T_{a,RTP} = 250^\circ\text{C}$ ;  $t_{a,RTP} = 30 \text{ min}$ ;  $T_{a,VA\_C} = 190^\circ\text{C}$ ;  $t_{a,VA\_C} = 2 \text{ h}$ ;  
 $h_{R10.5} \leq 8.7 \text{ nm}$ ;  $h_{B82} = 41.7 \text{ nm}$ ; – 12 s post-dev. O<sub>2</sub> RIE**

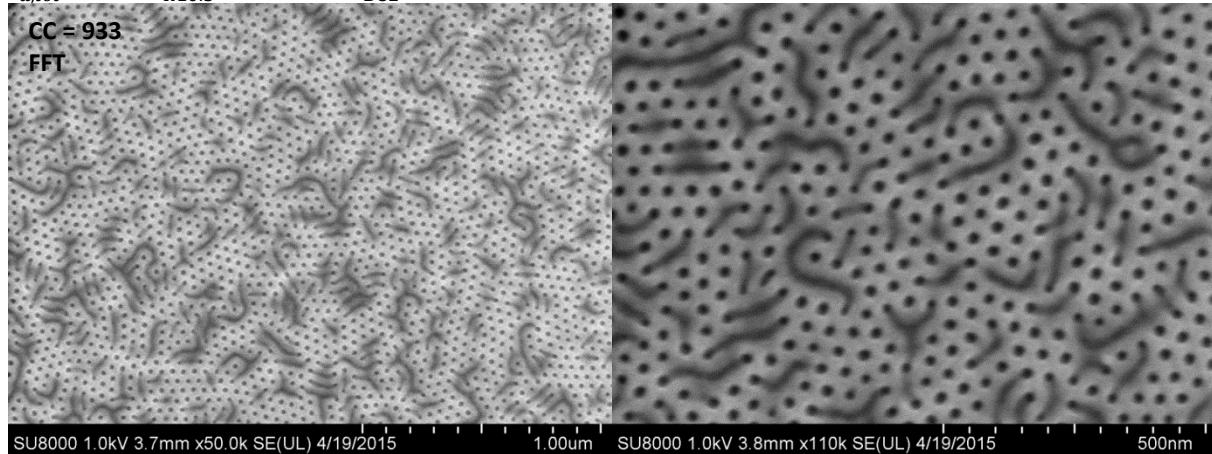


### A2.10 Multi-tiered RTP annealing programs for B82 samples

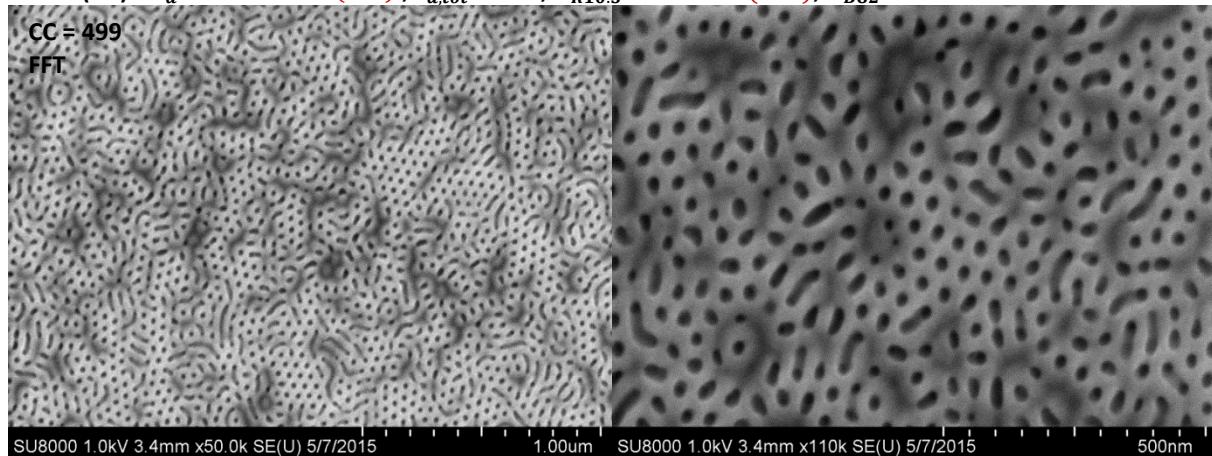
**W28F (N-U) -  $T_a = 250^\circ\text{C}$  (8m)  $\rightarrow 170^\circ\text{C}$  (50m);  $t_{a,tot} = 1$  h;  
 $h_{R10.5} = 8.6$  nm (AW);  $h_{B82} = 44.0$  nm**



**W17C (U) -  $T_a = 280^\circ\text{C}$  (5m)  $\rightarrow 250^\circ\text{C}$  (25m)  $\rightarrow 220^\circ\text{C}$  (10m)  $\rightarrow 190^\circ\text{C}$  (10m);  
 $t_{a,tot} = 1$  h;  $h_{R10.5} = 7.9$  nm;  $h_{B82} = 38.7$  nm**

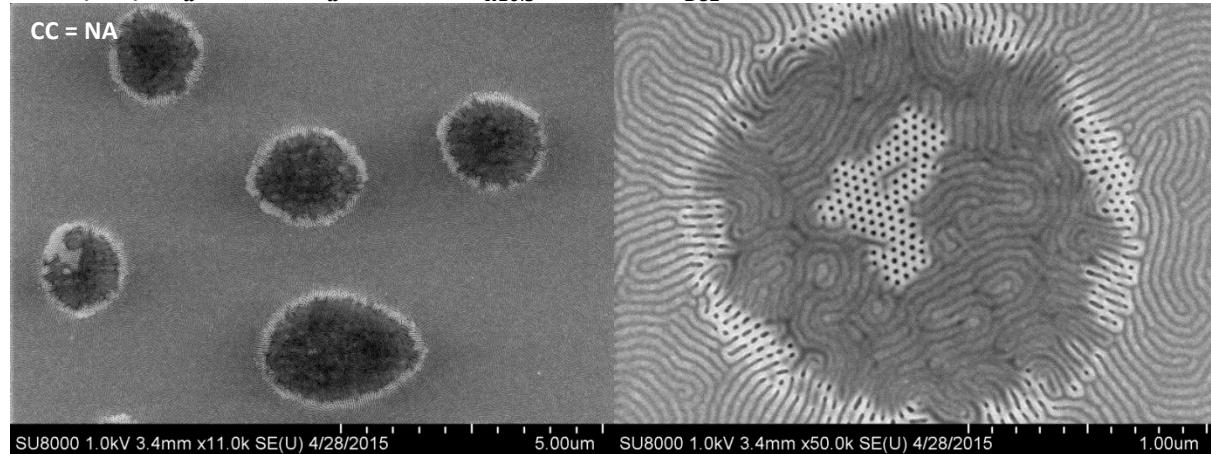


**W27A ( $\approx$ U) -  $T_a = 3 \times 250^\circ\text{C}$  (3m);  $t_{a,tot} = 1$  h;  $h_{R10.5} = 7.5$  nm (AW);  $h_{B82} = 44.4$  nm**



**A2.11 Graphite, instead of Si, carrier wafer in the RTP anneal of B82 sample**

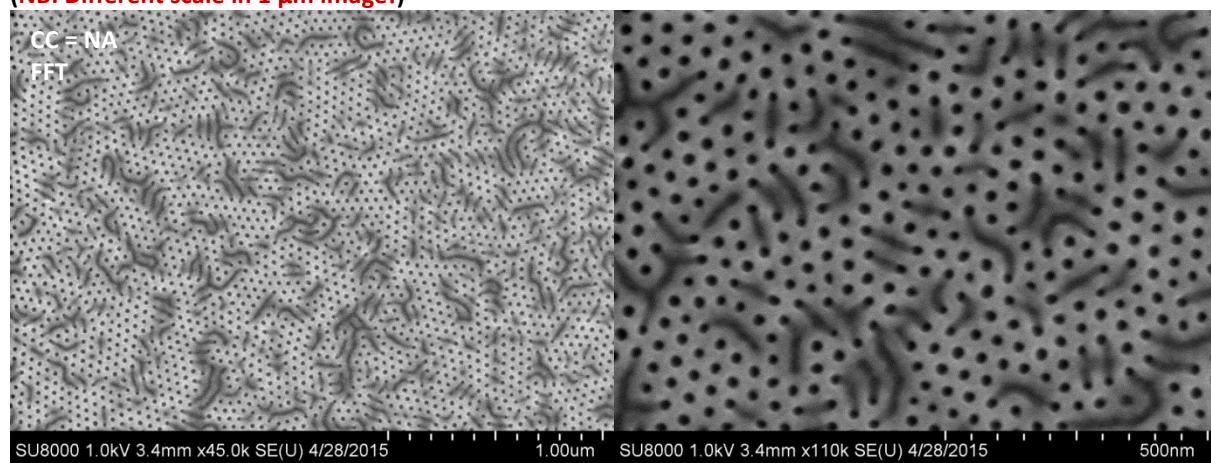
W23C (N-U) -  $T_a = 250^\circ\text{C}$ ;  $t_a = 15 \text{ min}$ ;  $h_{R10.5} = 8.0 \text{ nm}$ ;  $h_{B82} = 38.9 \text{ nm}$



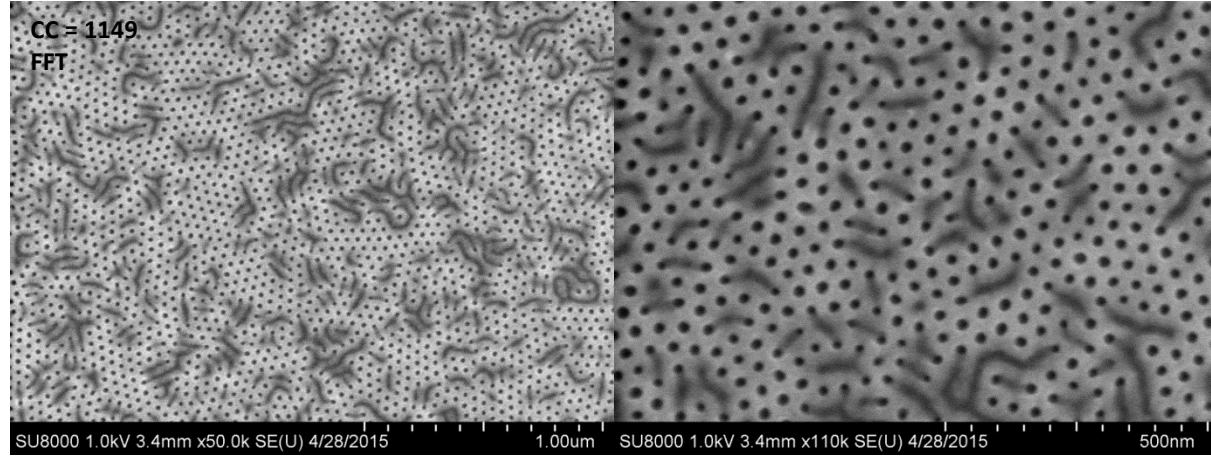
**A2.12 Effects of heating rate ( $\frac{dT}{dt}$ ) during the ramp-up of the RTP anneal of B82 samples**

W23B (U) -  $T_a = 250^\circ\text{C}$ ;  $t_a = 15 \text{ min}$ ;  $dT/dt = 5^\circ\text{C/s}$ ;  $h_{R10.5} = 8.0 \text{ nm}$ ;  $h_{B82} = 38.7 \text{ nm}$

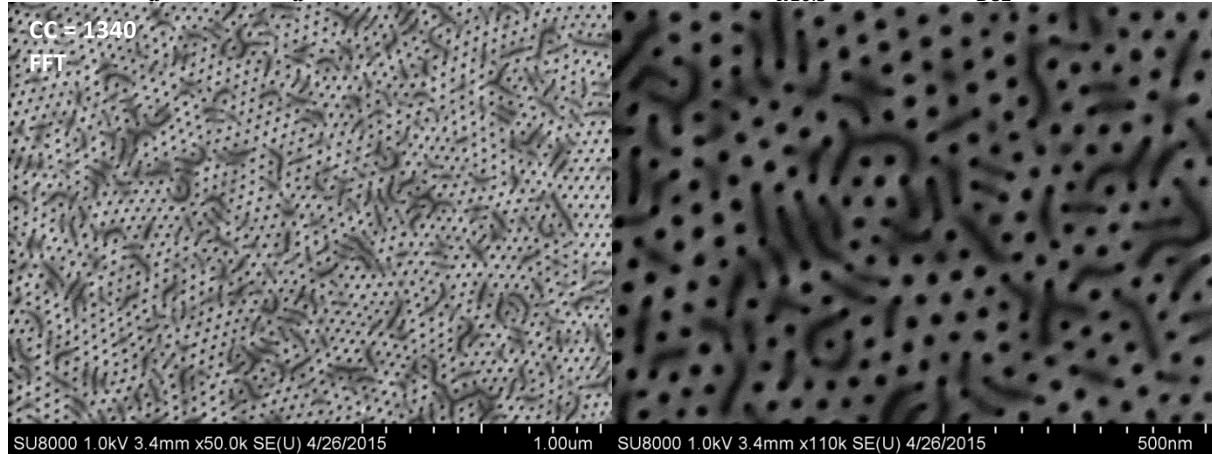
(NB: Different scale in 1 μm image!)



W23A (U) -  $T_a = 250^\circ\text{C}$ ;  $t_a = 15 \text{ min}$ ;  $dT/dt = 10^\circ\text{C/s}$ ;  $h_{R10.5} = 8.0 \text{ nm}$ ;  $h_{B82} = 38.5 \text{ nm}$



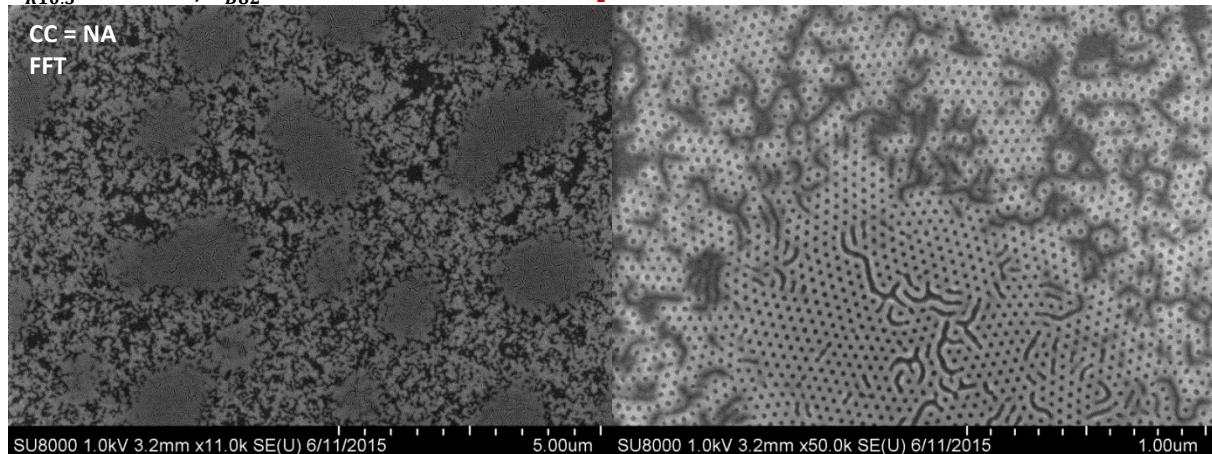
**W21F (U) -  $T_a = 250^\circ\text{C}$ ;  $t_a = 15 \text{ min}$ ;  $dT/dt = 18^\circ\text{C/s (Standard)}$ ;  $h_{R10.5} = 7.7 \text{ nm}$ ;  $h_{B82} = 39.5 \text{ nm}$**



### A3.13 TOPHEAT option during RTP anneal of B82 samples

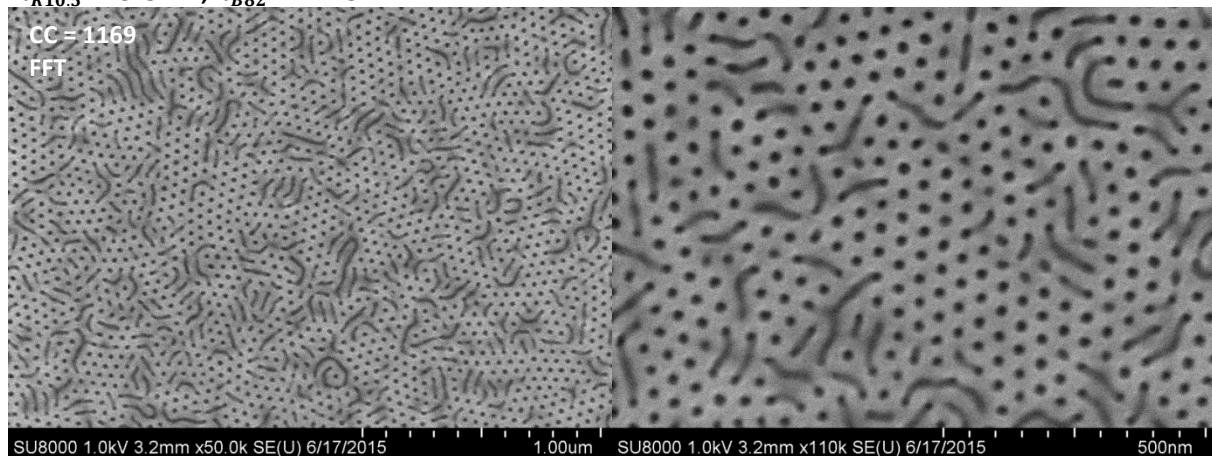
**W35A (N-U) -  $T_a = 250^\circ\text{C}$ ;  $t_a = 30 \text{ min}$ ; TOPHEAT during ramp-up;**

**$h_{R10.5} = 8.5 \text{ nm}$ ;  $h_{B82} = 42.1 \text{ nm}$  - 12 s Pre. Dev. O<sub>2</sub> RIE**

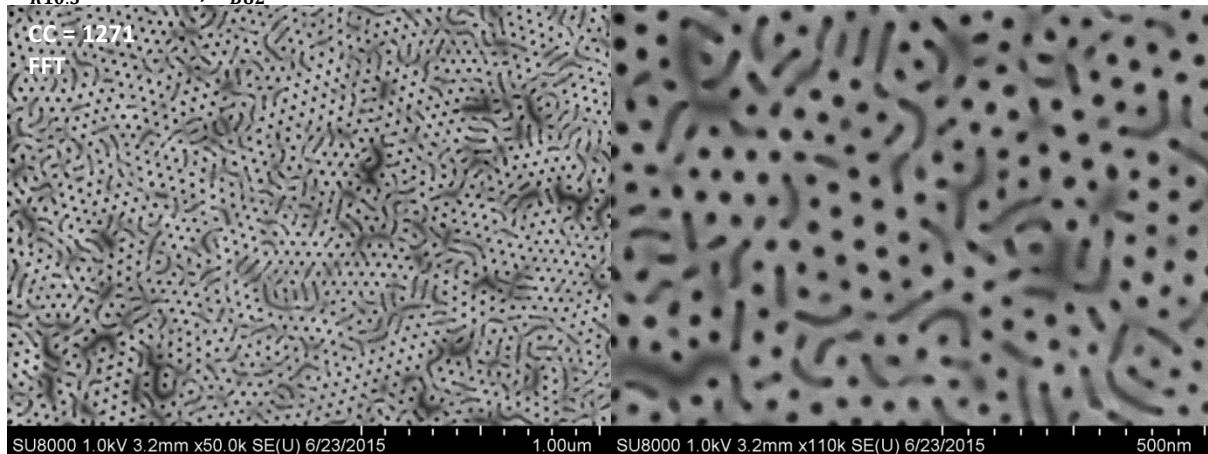


**W35D (U) -  $T_a = 230^\circ\text{C}$ ;  $t_a = 1 \text{ h}$ ;  $dT/dt = 10^\circ\text{C/s}$ ; TOPHEAT during entire anneal;**

**$h_{R10.5} = 8.5 \text{ nm}$ ;  $h_{B82} = 42.3 \text{ nm}$**

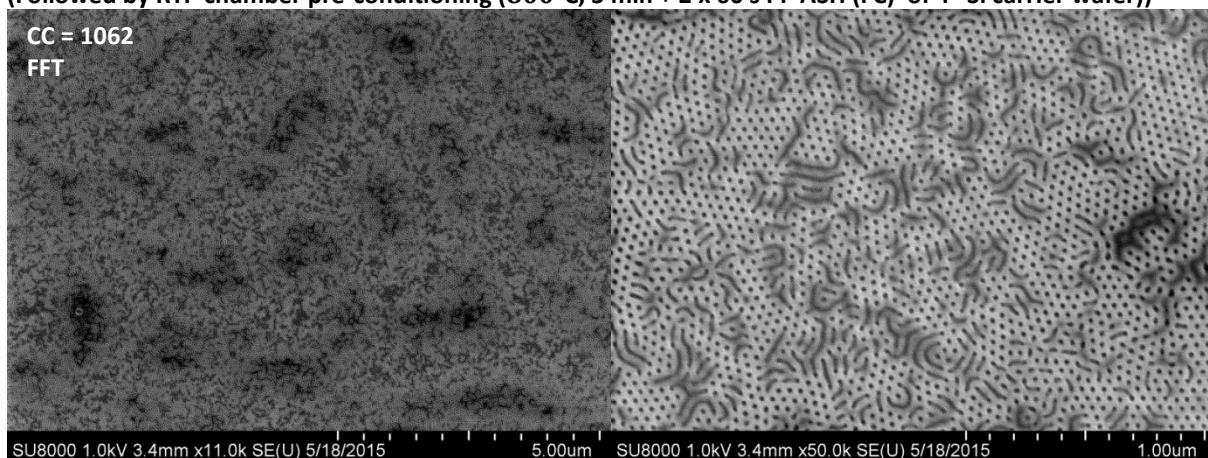


**W39C (U) -  $T_a = 230^\circ\text{C}$ ;  $t_a = 30 \text{ min}$ ;  $dT/dt = 5^\circ\text{C/s}$ ; TOPHEAT during ramp-up;  
 $h_{R10.5} = 7.8 \text{ nm}$ ;  $h_{B82} = 44.9 \text{ nm}$**

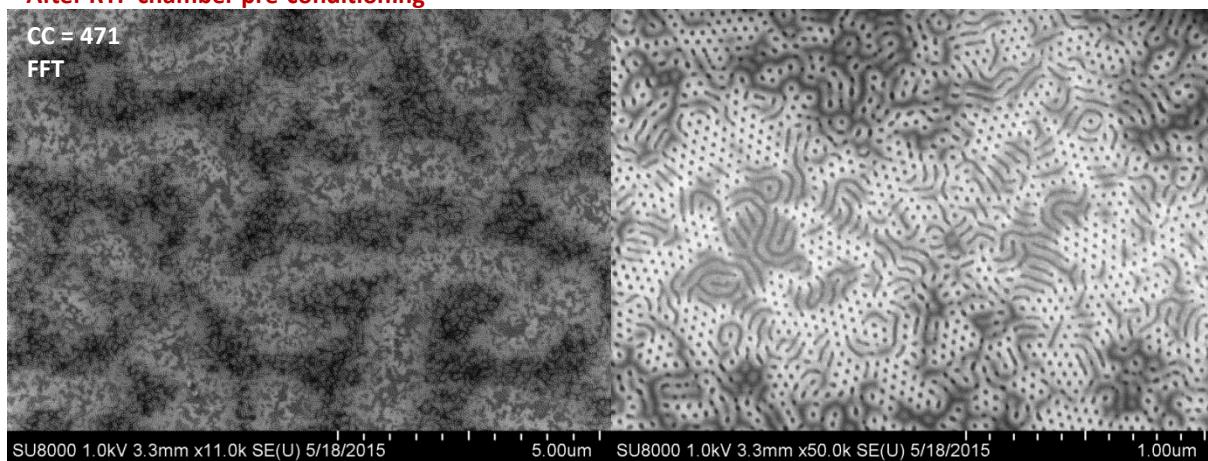


#### A2.14 Effect of RTP chamber preconditioning prior to anneal of B82 samples

**W29B (N-U) -  $T_a = 250^\circ\text{C}$ ;  $t_a = 30 \text{ min}$ ;  $h_{R10.5} = 8.6 \text{ nm}$ ;  $h_{B82} = 43.1 \text{ nm}$  – Reference sample  
(Followed by RTP chamber pre-conditioning ( $800^\circ\text{C}$ , 5 min +  $2 \times 60 \text{ s}$  PP ASH (FC) of 4" Si carrier wafer))**



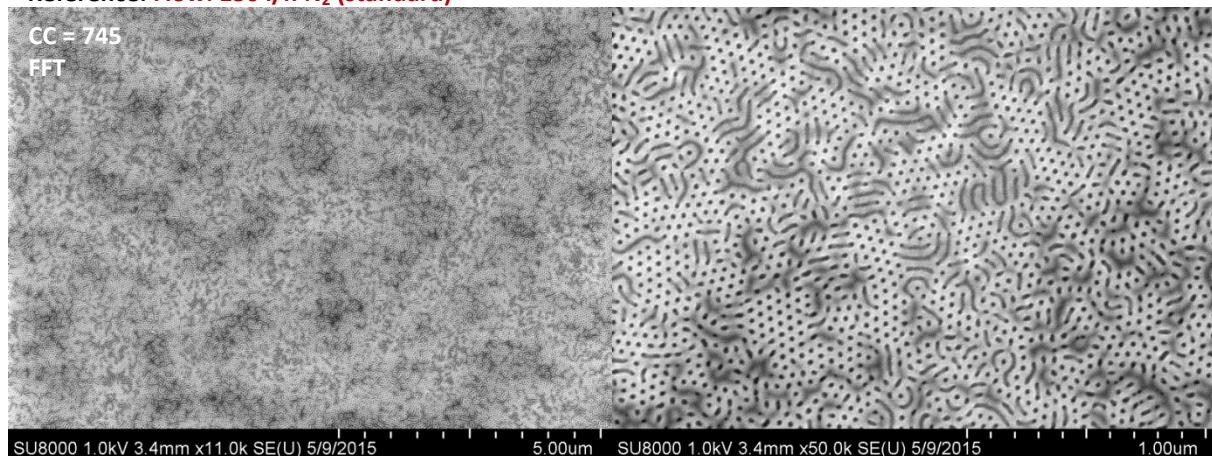
**W29C (N-U) -  $T_a = 250^\circ\text{C}$ ;  $t_a = 30 \text{ min}$ ;  $h_{R10.5} = 8.6 \text{ nm}$ ;  $h_{B82} = 44.3 \text{ nm}$   
– After RTP chamber pre-conditioning**



### A2.15 Effect of alternative gas flow during RTP anneal of B82 samples

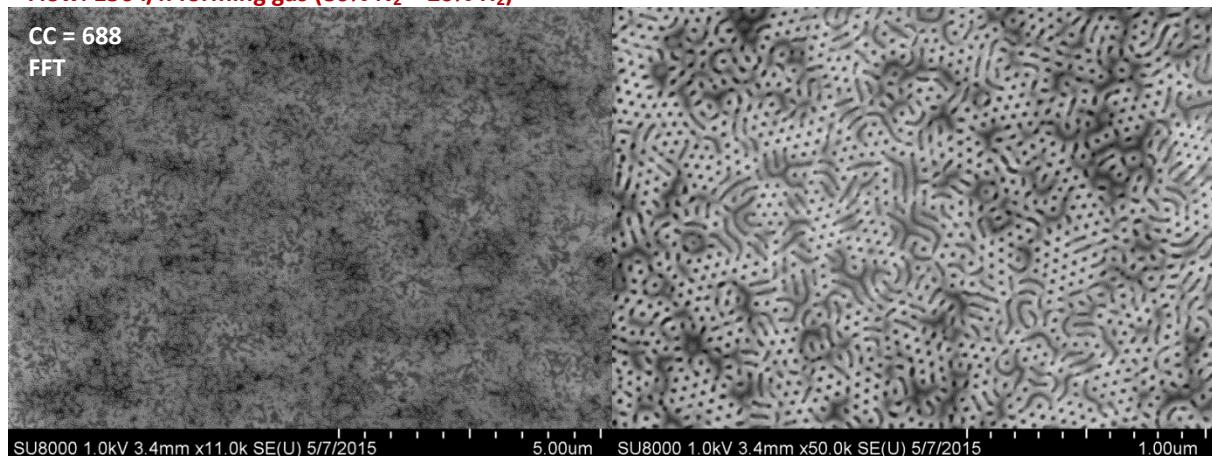
W27F (N-U) -  $T_a = 250^\circ\text{C}$ ;  $t_a = 1 \text{ h}$ ;  $h_{R10.5} = 7.5 \text{ nm}$ ;  $h_{B82} = 44.3 \text{ nm}$

– Reference: Flow: 150 l/h N<sub>2</sub> (standard)

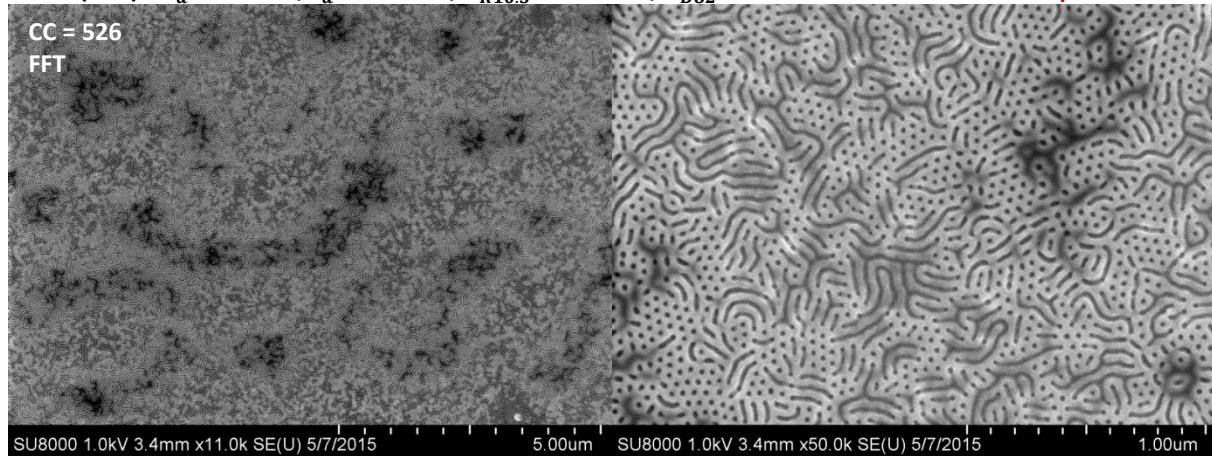


W27B (N-U) -  $T_a = 250^\circ\text{C}$ ;  $t_a = 30 \text{ min}$ ;  $h_{R10.5} = 7.5 \text{ nm}$ ;  $h_{B82} = 44.3 \text{ nm}$

– Flow: 150 l/h forming gas (80% N<sub>2</sub> + 20% H<sub>2</sub>)

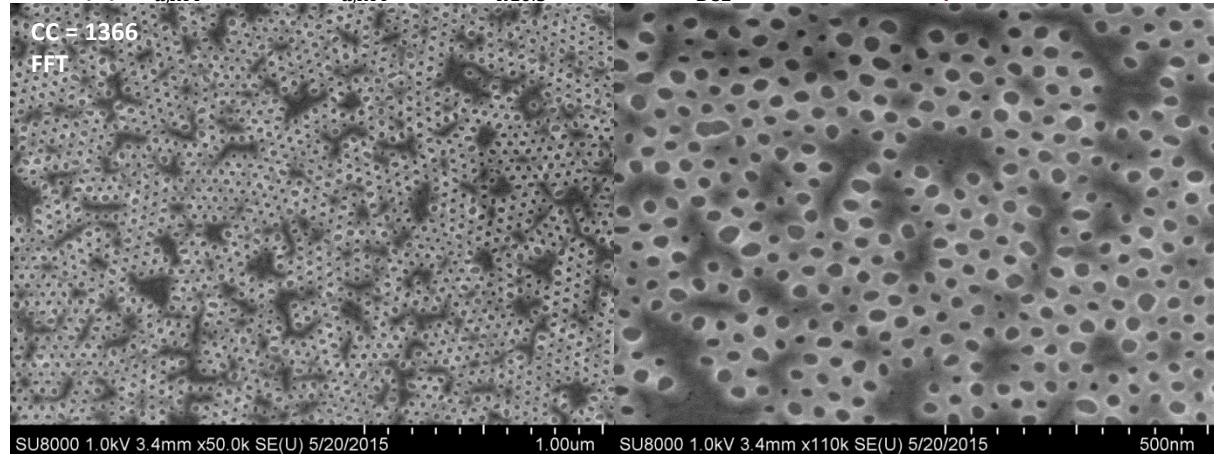


W27C (N-U) -  $T_a = 250^\circ\text{C}$ ;  $t_a = 30 \text{ min}$ ;  $h_{R10.5} = 7.5 \text{ nm}$ ;  $h_{B82} = 44.2 \text{ nm}$  – RTP “Vacuum” option

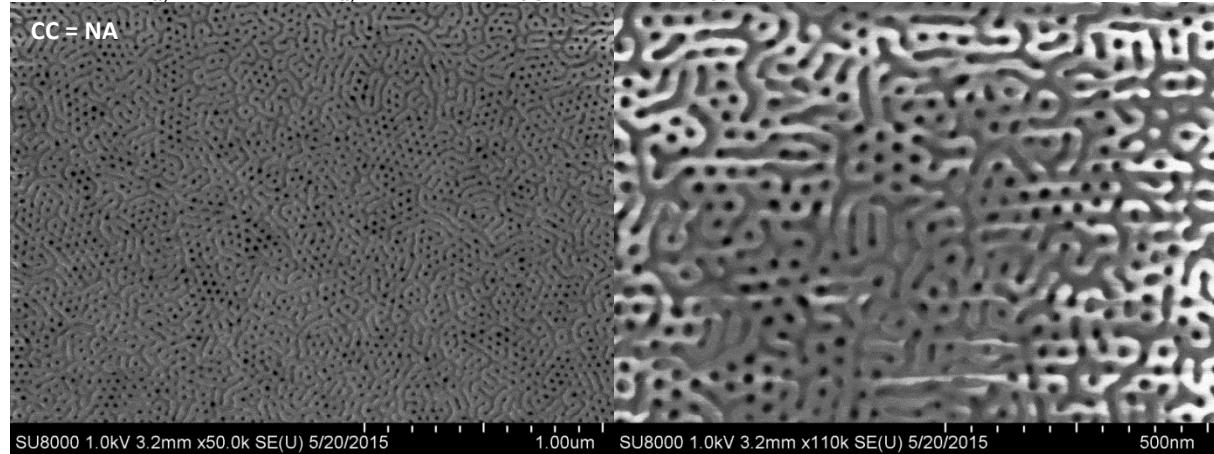


**A2.16 Double layered Al foil as an O<sub>2</sub> barrier during anneal of B82/B67 samples**

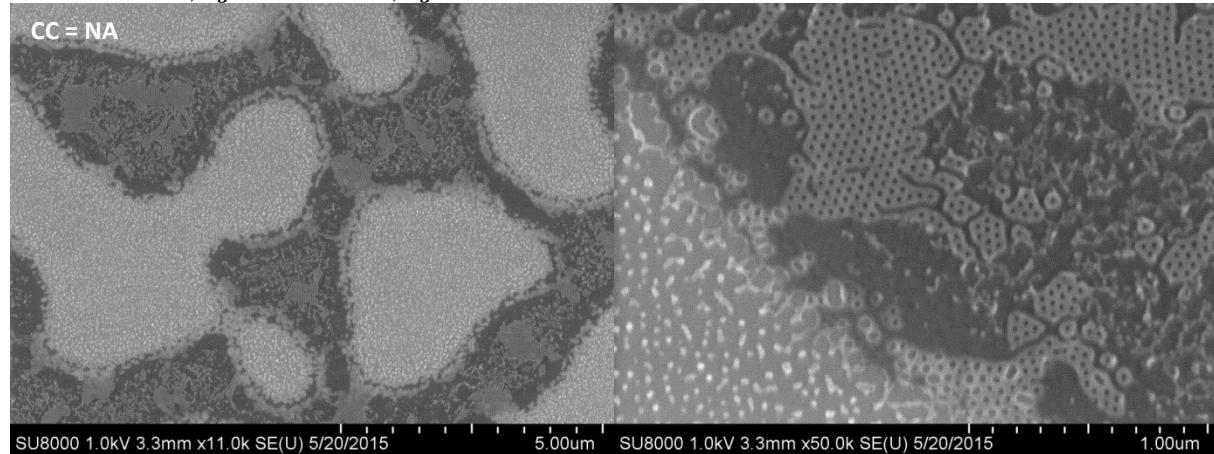
**W30A (U) -  $T_{a,RTP} = 250^\circ\text{C}$ ;  $t_{a,RTP} = 1 \text{ h}$ ;  $h_{R10.5} = 8.7 \text{ nm}$ ;  $h_{B82} = 36.0 \text{ nm}$  – 15 s pre-dev. O<sub>2</sub> RIE**



**W30C (U) -  $T_{a,RTP} = 250^\circ\text{C}$ ;  $t_{a,RTP} = 1 \text{ h}$ ;  $h_{R10.5} = 8.7 \text{ nm}$ ;  $h_{B69} = 146.1 \text{ nm}$  – 15 s pre-dev. O<sub>2</sub> RIE**

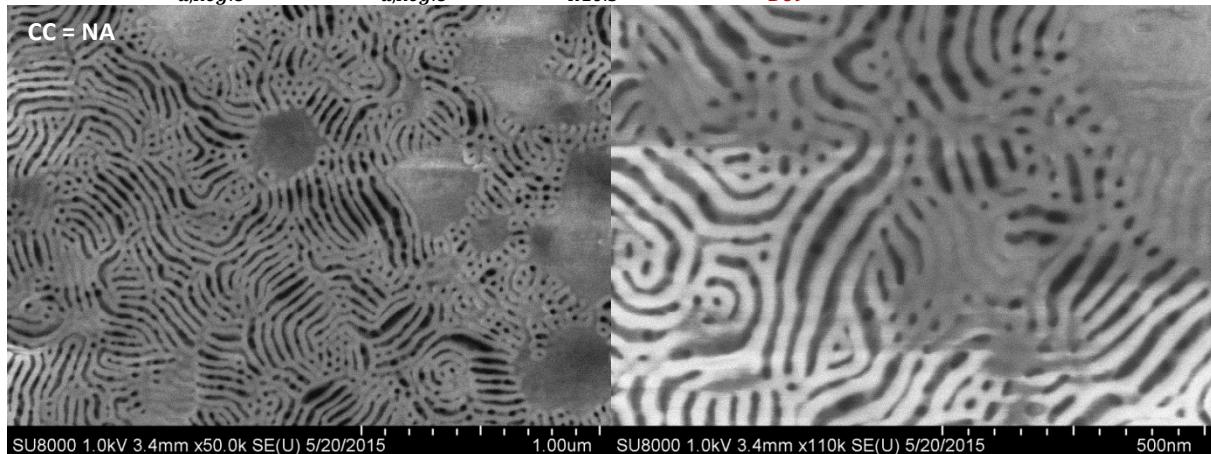


**W30B (N-U) -  $T_{a,Reg.O} = 190^\circ\text{C}$ ;  $t_{a,Reg.O} = 24 \text{ h}$ ;  $h_{R10.5} = 8.7 \text{ nm}$ ;  $h_{B82} = 37.3 \text{ nm}$  – 15 s pre-dev. O<sub>2</sub> RIE**



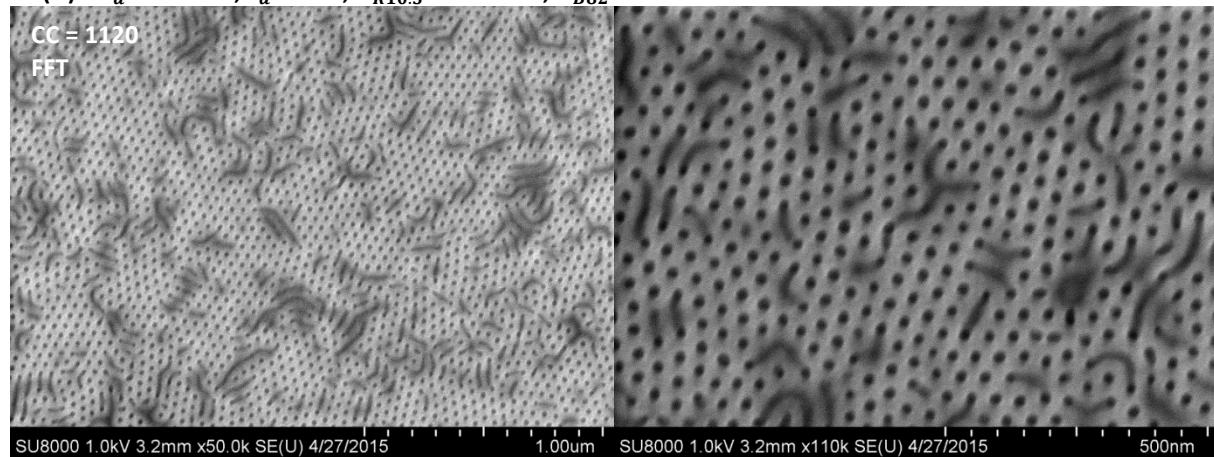
**W30D (N-U) -  $T_{a,Reg.0} = 190^\circ\text{C}$ ;  $t_{a,Reg.0} = 24 \text{ h}$ ;  $h_{R10.5} = 8.7 \text{ nm}$ ;  $h_{B69} = 145.7 \text{ nm}$  – 15 s pre-dev. O<sub>2</sub> RIE**

CC = NA

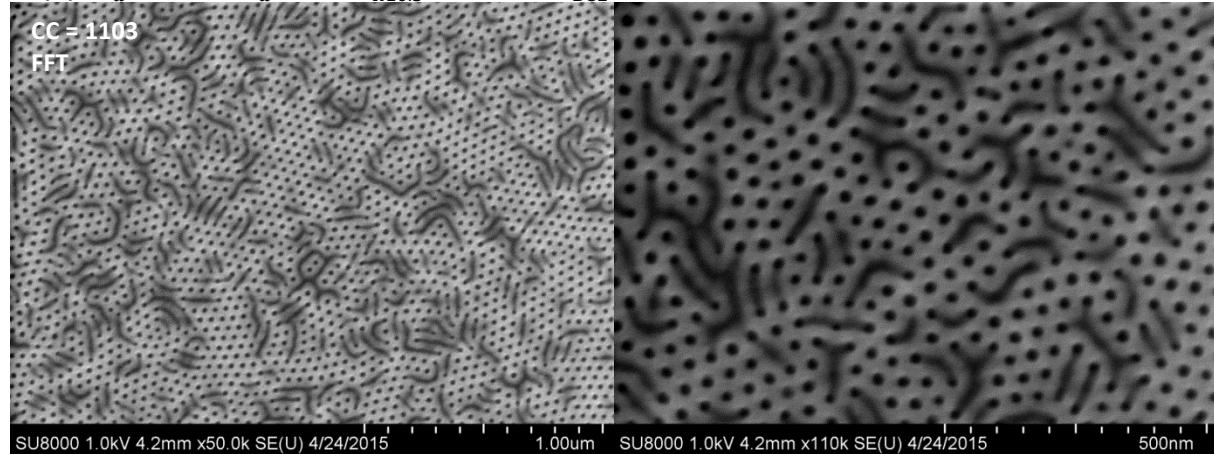


**A2.17 Detrimental effects of post-SC soft-bake (on hotplate in ambient atmosphere)?**

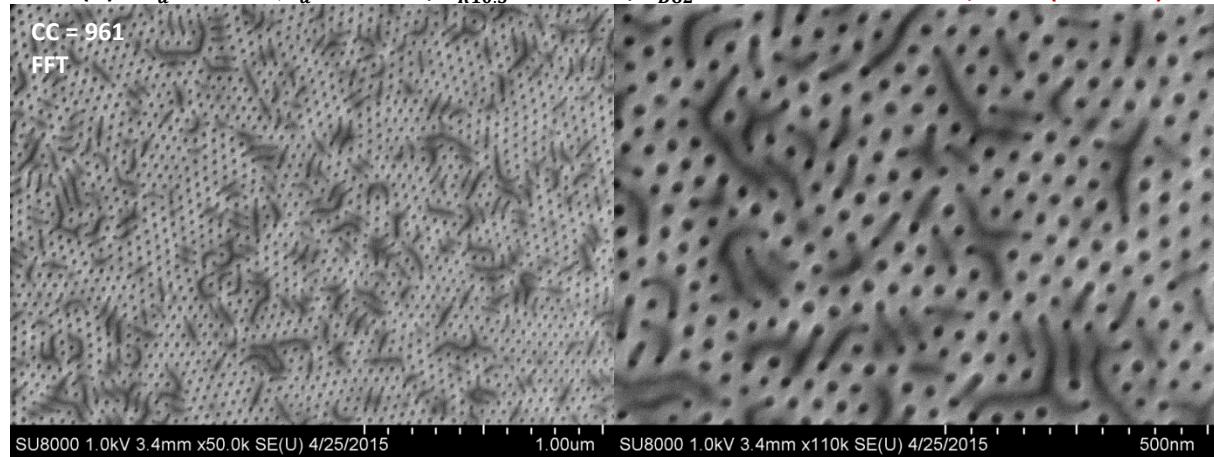
**S3 (U) -  $T_a = 250^\circ\text{C}$ ;  $t_a = 1 \text{ h}$ ;  $h_{R10.5} = 7.0 \text{ nm}$ ;  $h_{B82} = 39.9 \text{ nm}$  – SB: None**



**S2 (U) -  $T_a = 250^\circ\text{C}$ ;  $t_a = 1 \text{ h}$ ;  $h_{R10.5} = 7.3 \text{ nm}$ ;  $h_{B82} = 40.4 \text{ nm}$  – SB:  $50^\circ\text{C}$ , 3 min**

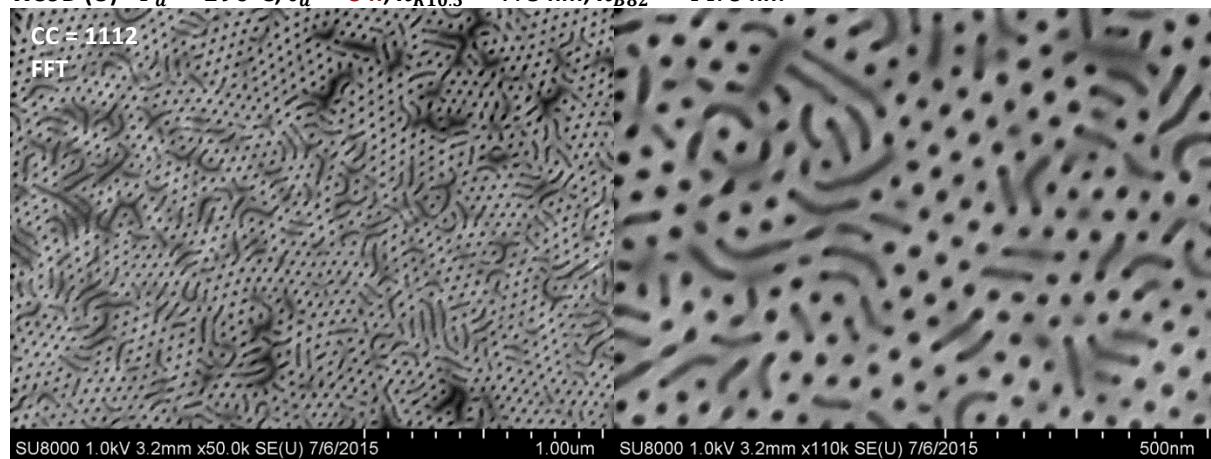


**W21C (U) -  $T_a = 250^\circ\text{C}$ ,  $t_a = 30 \text{ min}$ ;  $h_{R10.5} = 7.7 \text{ nm}$ ;  $h_{B82} = 39.4 \text{ nm}$  – SB:  $100^\circ\text{C}$ , 1 min (standard)**

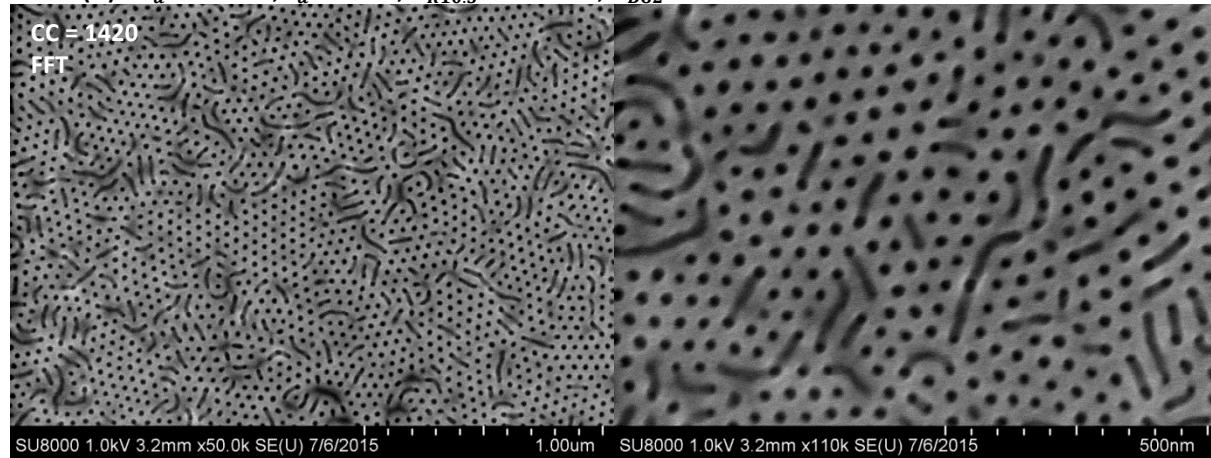


**A2.18 Extended vacuum oven anneals of B82 samples**

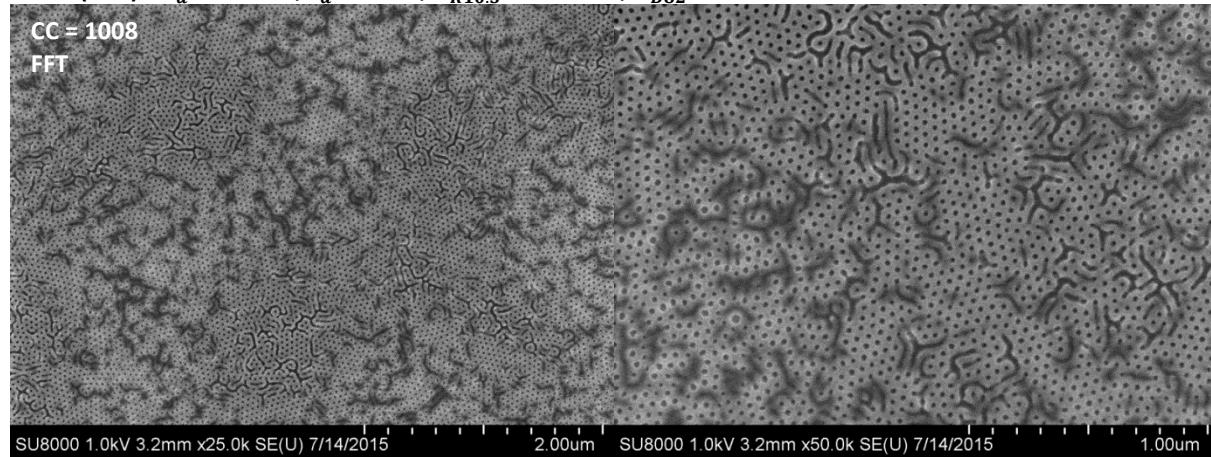
**W39D (U) -  $T_a = 190^\circ\text{C}$ ;  $t_a = 6 \text{ h}$ ;  $h_{R10.5} = 7.8 \text{ nm}$ ;  $h_{B82} = 44.6 \text{ nm}$**



**W39B (U) -  $T_a = 190^\circ\text{C}$ ;  $t_a = 24 \text{ h}$ ;  $h_{R10.5} = 7.8 \text{ nm}$ ;  $h_{B82} = 44.7 \text{ nm}$**



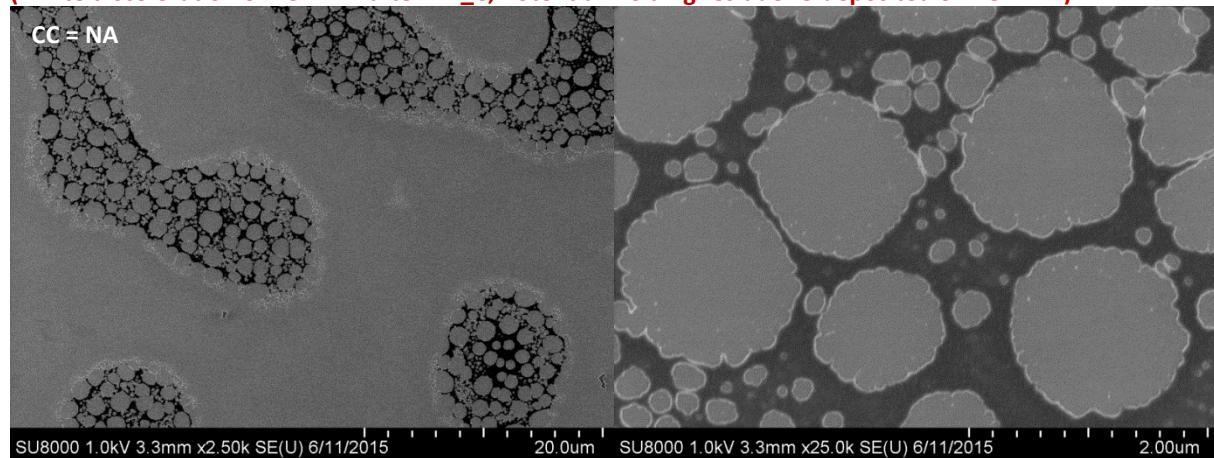
**W39F (N-U) -  $T_a = 200^\circ\text{C}$ ;  $t_a = 48 \text{ h}$ ;  $h_{R10.5} = 7.8 \text{ nm}$ ;  $h_{B82} = 44.5 \text{ nm}$**



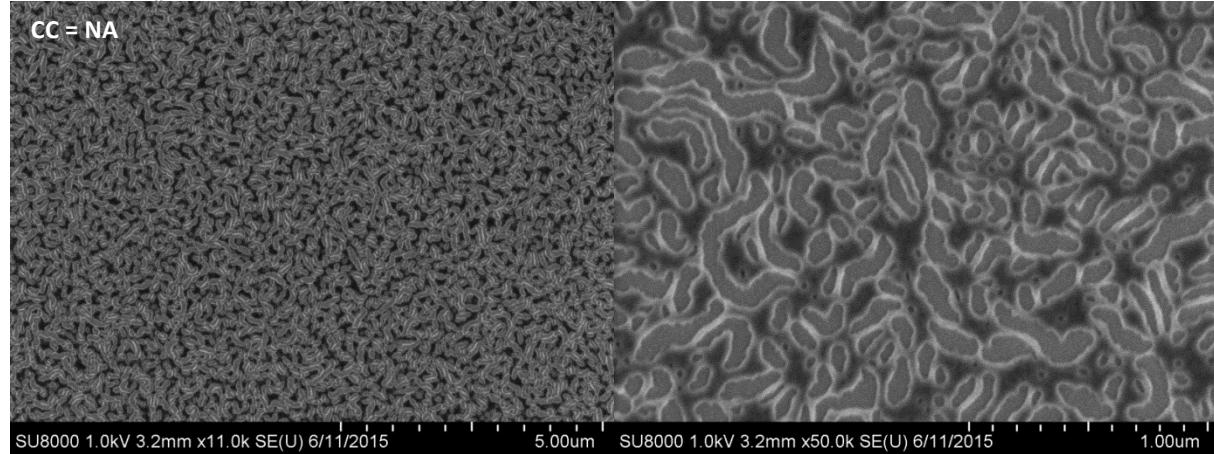
**A2.19** Extended vacuum anneal, in custom-built ovenproof chamber (v. 1.0), of B82 samples

W34A (N-U) -  $T_a = 190^\circ\text{C}$ ;  $t_a = 24 \text{ h}$ ;  $h_{R10.5} \leq 8.5 \text{ nm}$ ;  $h_{B82} = 41.6 \text{ nm}$

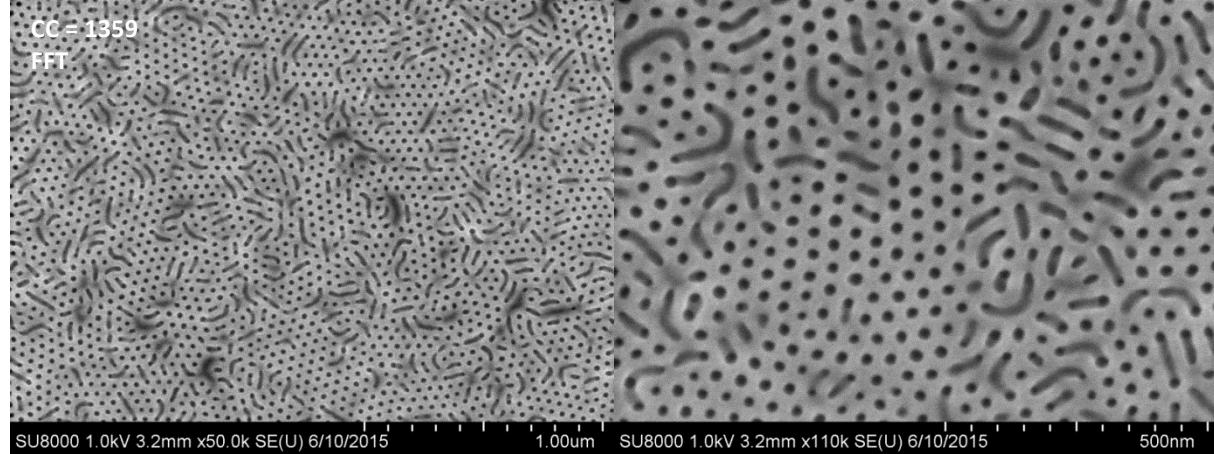
(White discoloration of B82 film after VA\_C; Potential welding residue re-deposited on B82 film)



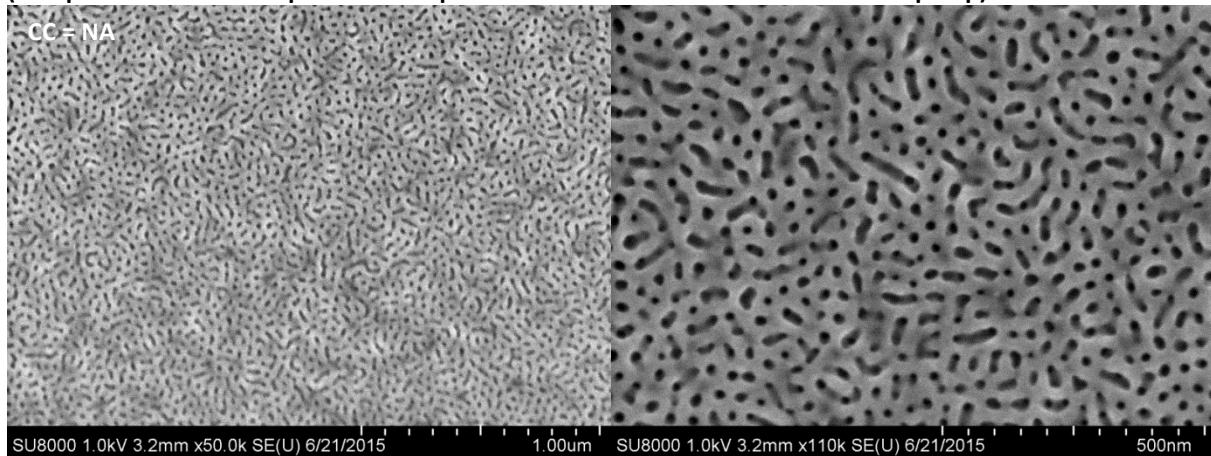
W35B (U) -  $T_a = 170^\circ\text{C}$ ;  $t_a = 24 \text{ h}$ ;  $h_{R10.5} \leq 8.5 \text{ nm}$ ;  $h_{B82} = 42.4 \text{ nm}$  – Presumable O<sub>2</sub> damage/thinning



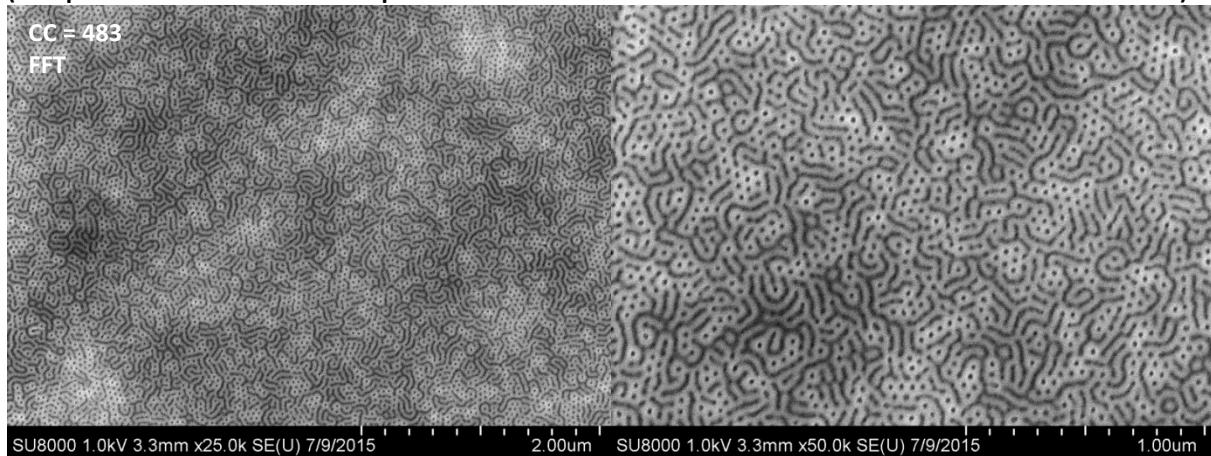
W35C ( $\approx$ U) -  $T_a = 190^\circ\text{C}$ ;  $t_a = 2 \text{ h}$ ;  $h_{R10.5} \leq 8.5 \text{ nm}$ ;  $h_{B82} = 42.4 \text{ nm}$



**W35F (U) -  $T_a \approx 170^\circ\text{C}$  (Hotplate setpoint =  $200^\circ\text{C}$ );  $t_a = 6 \text{ h}$ ;  $h_{R10.5} \leq 8.5 \text{ nm}$ ;  $h_{B82} = 42.1 \text{ nm}$**   
**(Pumped-down chamber placed on hotplate whilst still attached to turbo vacuum pump)**

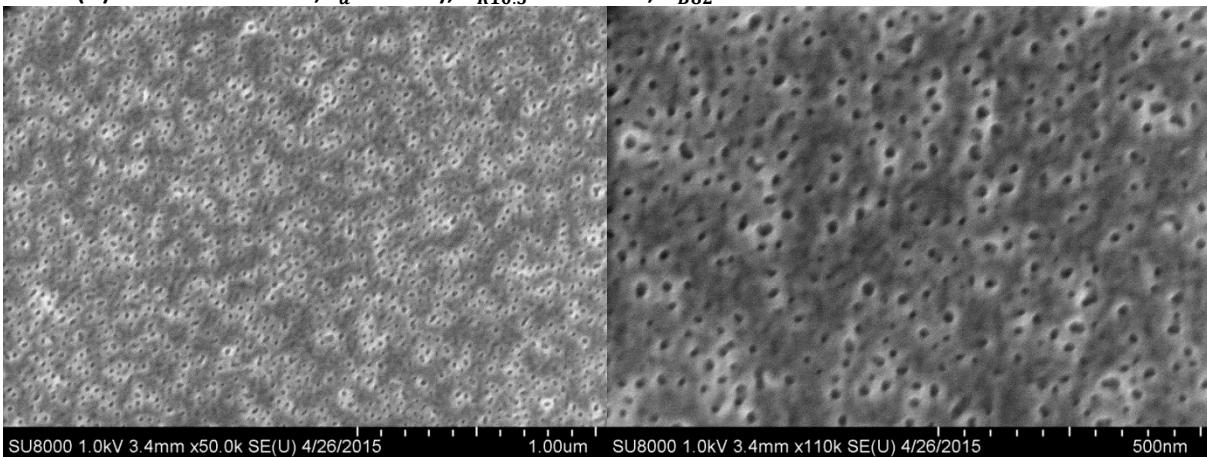


**W39E (N-U) -  $T_a = 190^\circ\text{C}$ ;  $t_a = 24 \text{ h}$ ;  $h_{R10.5} = 7.8 \text{ nm}$ ;  $h_{B82} = 44.6 \text{ nm}$**   
**(Pumped-down vacuum chamber placed inside vacuum oven and unloaded whilst the oven was still warm)**

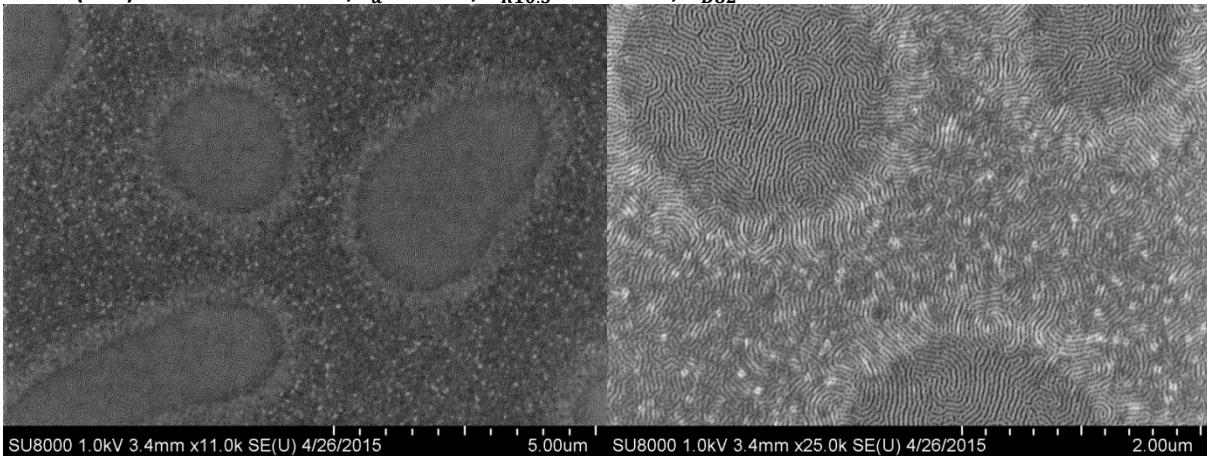


**A2.20** 24h SVA at  $T_a = RT$  ( $21 - 23^\circ\text{C}$ ) of B82 samples

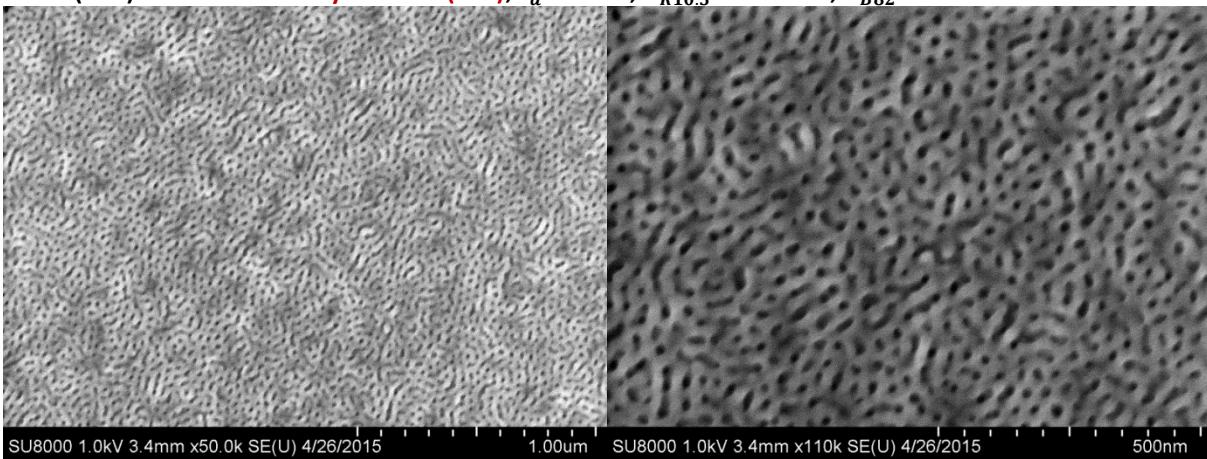
W22A (U) – Solvent: **Anisole**;  $t_a = 24 \text{ h}$ ;  $h_{R10.5} = 8.1 \text{ nm}$ ;  $h_{B82} = 39.2 \text{ nm}$



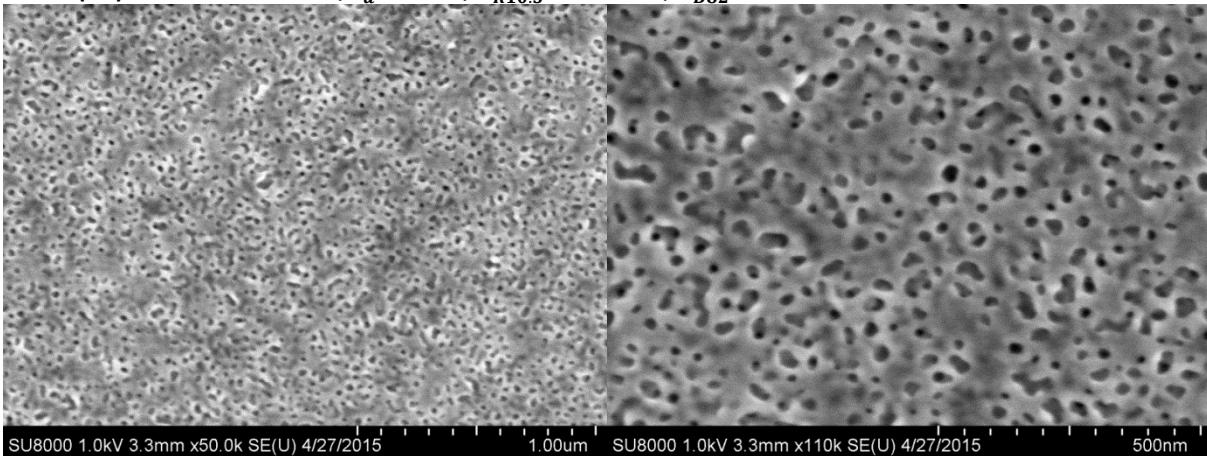
W22B (N-U) – Solvent: **Toluene**;  $t_a = 24 \text{ h}$ ;  $h_{R10.5} = 8.1 \text{ nm}$ ;  $h_{B82} = 40.8 \text{ nm}$



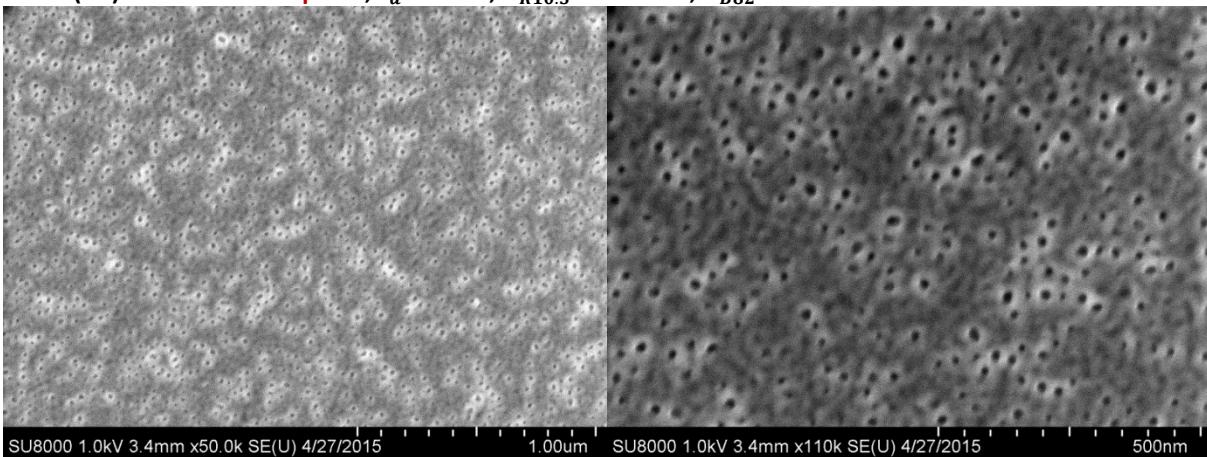
W22C ( $\approx$ U\*) – Solvent: **Tetrahydrofuran (THF)**;  $t_a = 24 \text{ h}$ ;  $h_{R10.5} = 8.1 \text{ nm}$ ;  $h_{B82} = 39.2 \text{ nm}$



**W22D ( $\approx$ U) – Solvent: Acetone;  $t_a = 24$  h;  $h_{R10.5} = 8.1$  nm;  $h_{B82} = 39.6$  nm**

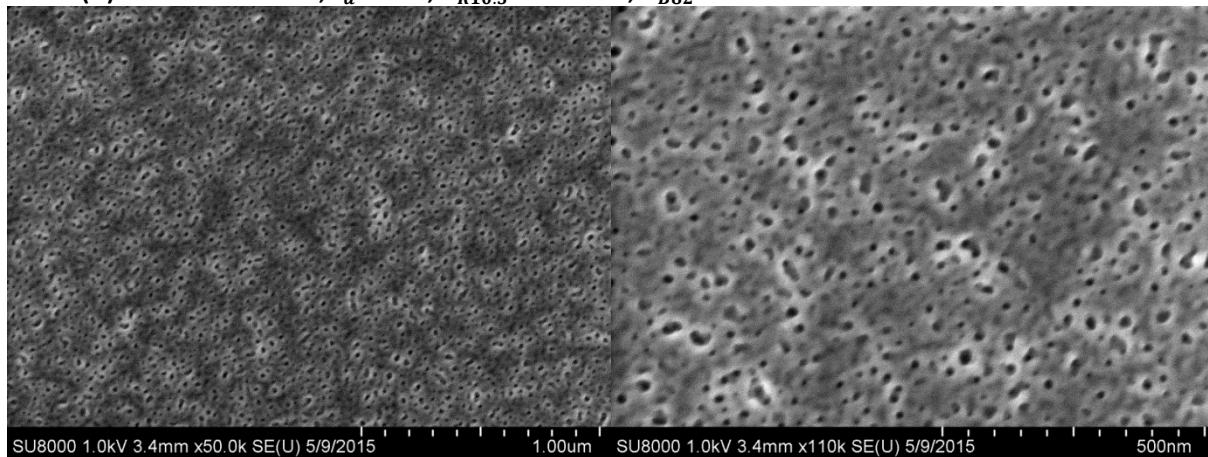


**W22E ( $\approx$ U) – Solvent: 2-Propanol;  $t_a = 24$  h;  $h_{R10.5} = 8.1$  nm;  $h_{B82} = 40.1$  nm**

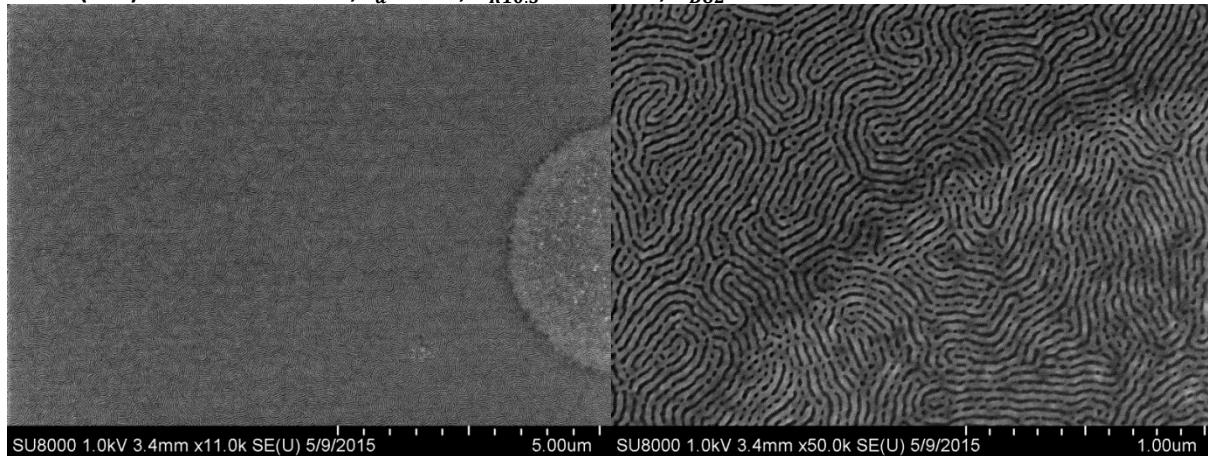


**A2.21** 4h SVA at  $T_a = RT$  ( $21 - 23^\circ\text{C}$ ) of B82 samples

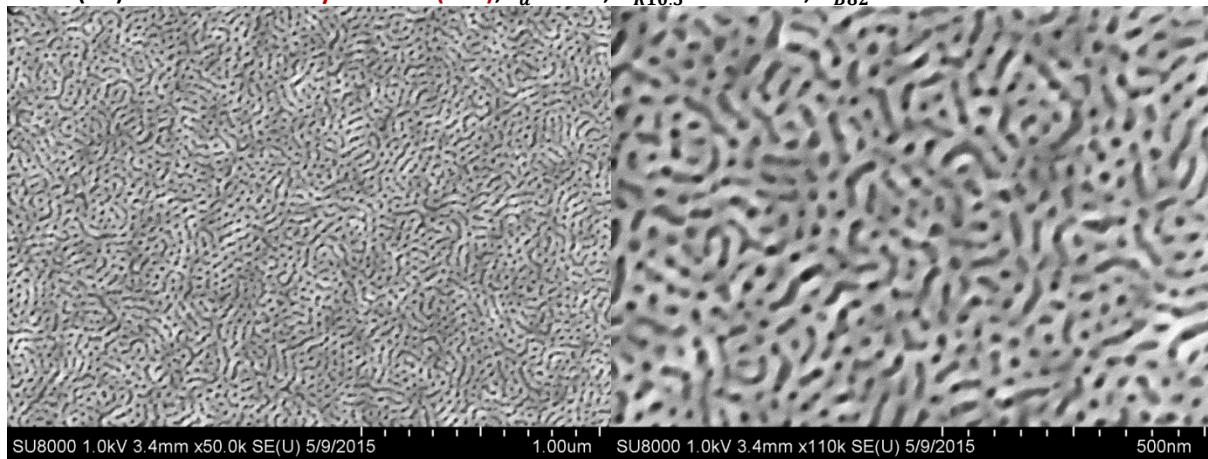
W28D (U) – Solvent: **Anisole**;  $t_a = 4 \text{ h}$ ;  $h_{R10.5} = 8.6 \text{ nm}$ ;  $h_{B82} = 44.6 \text{ nm}$



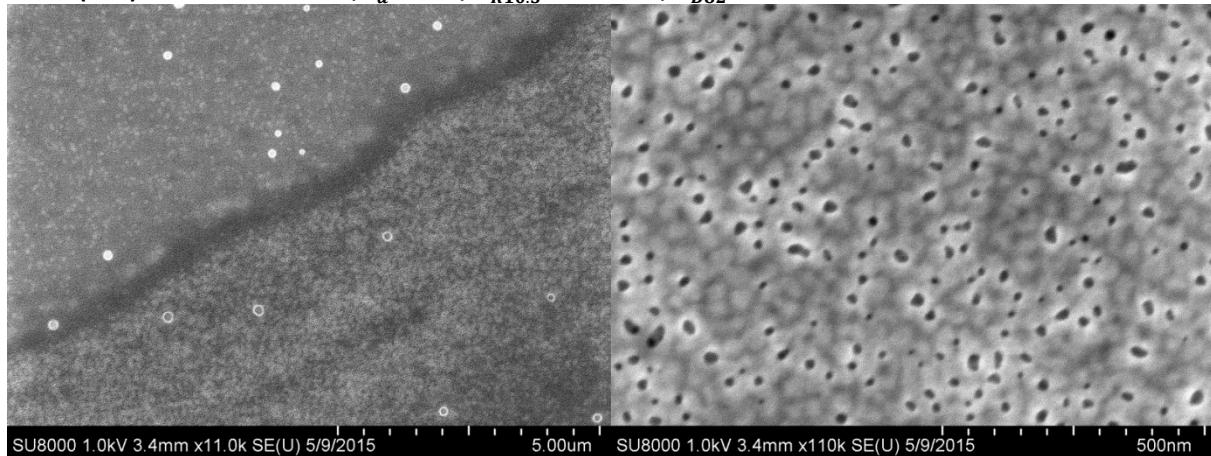
W28B (N-U) – Solvent: **Toluene**;  $t_a = 4 \text{ h}$ ;  $h_{R10.5} = 8.6 \text{ nm}$ ;  $h_{B82} = 44.0 \text{ nm}$



W28E (U\*) – Solvent: **Tetrahydrofuran (THF)**;  $t_a = 4 \text{ h}$ ;  $h_{R10.5} = 8.6 \text{ nm}$ ;  $h_{B82} = 44.6 \text{ nm}$

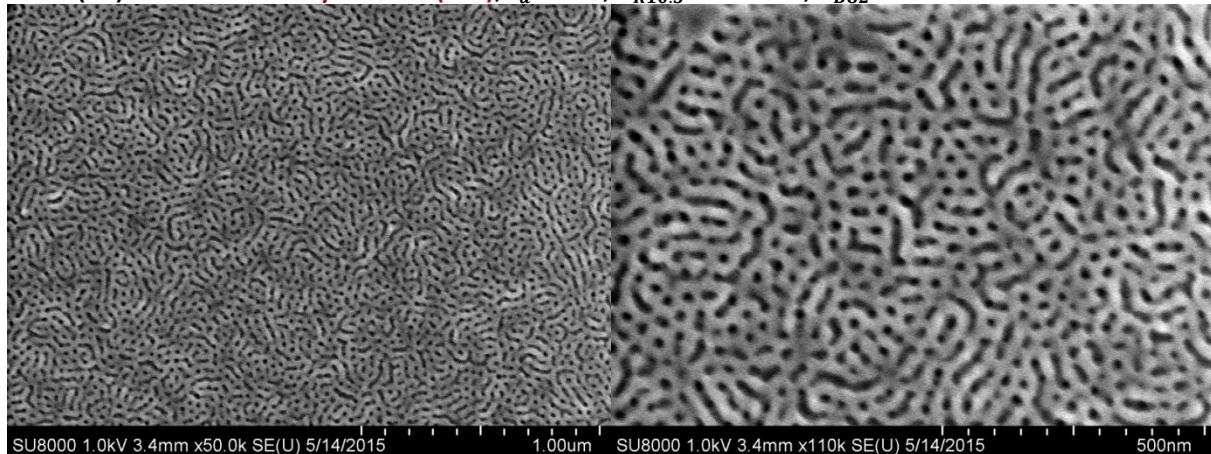


**W28C (N-U) – Solvent: Acetone;  $t_a = 4$  h;  $h_{R10.5} = 8.6$  nm;  $h_{B82} = 44.8$  nm**



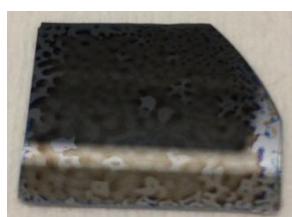
**A2.22** 1h SVA  $T_a = RT$  (21 – 23°C) of B82 samples

**W27E (U\*) – Solvent: Tetrahydrofuran (THF);  $t_a = 1$  h;  $h_{R10.5} = 7.5$  nm;  $h_{B82} = 44.4$  nm**



**A2.23** SVA – Post-development overview photos

W22D – Acetone, 24h



W28D – Anisole, 4h



W28B – Toluene, 4h



W28E – THF, 4h



W28C – Acetone, 4h



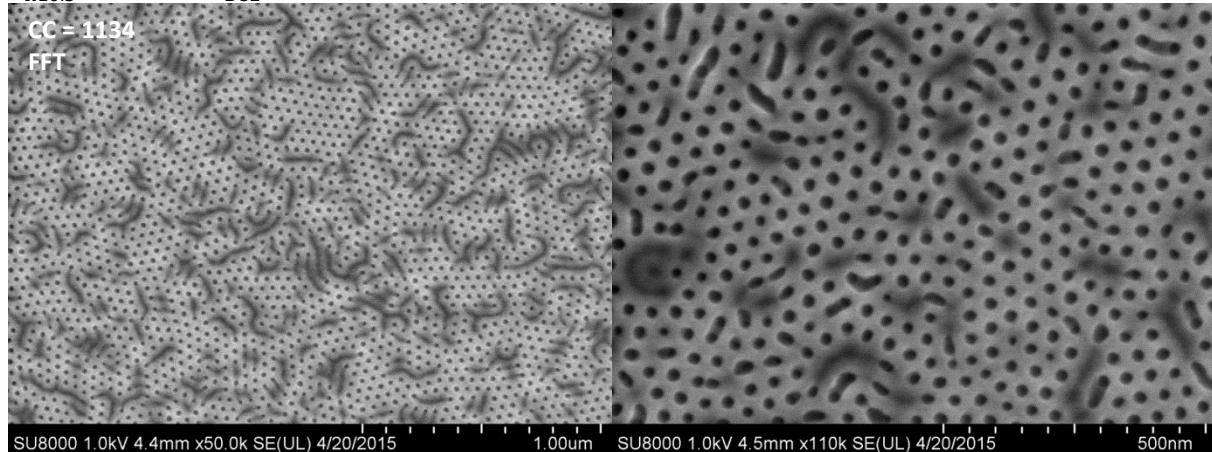
W27E – THF, 1h



**A2.24 Sequential anneal in RTP and regular lab oven or VO of B82 samples**

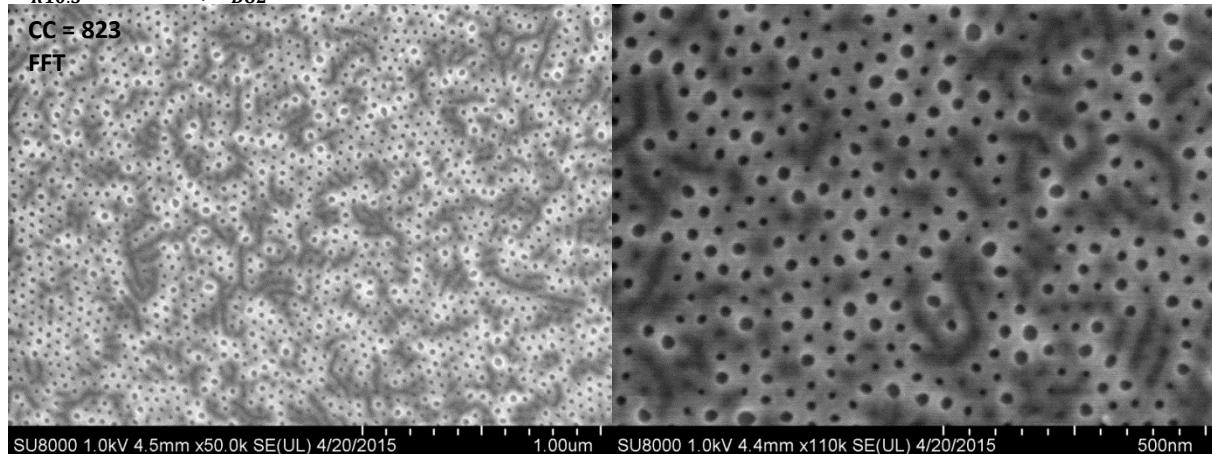
**W17D (≈U) -  $T_{a,RTP} = 250^\circ\text{C}$ ;  $t_{a,RTP} = 1 \text{ h} \rightarrow T_{a,Reg.O} = 100^\circ\text{C}$ ;  $t_{a,Reg.O} = 18 \text{ h}$ ;**

$h_{R10.5} \leq 7.9 \text{ nm}$ ;  $h_{B82} = 38.2 \text{ nm}$



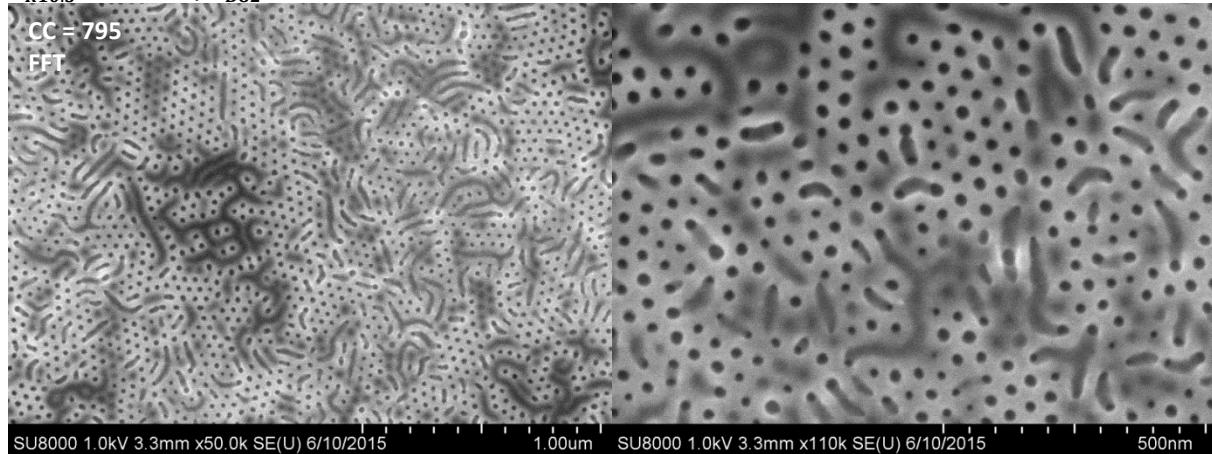
**W17E (≈U) -  $T_{a,RTP} = 250^\circ\text{C}$ ;  $t_{a,RTP} = 1 \text{ h} \rightarrow T_{a,Reg.O} = 150^\circ\text{C}$ ;  $t_{a,Reg.O} = 18 \text{ h}$ ;**

$h_{R10.5} \leq 7.9 \text{ nm}$ ;  $h_{B82} = 37.7 \text{ nm}$



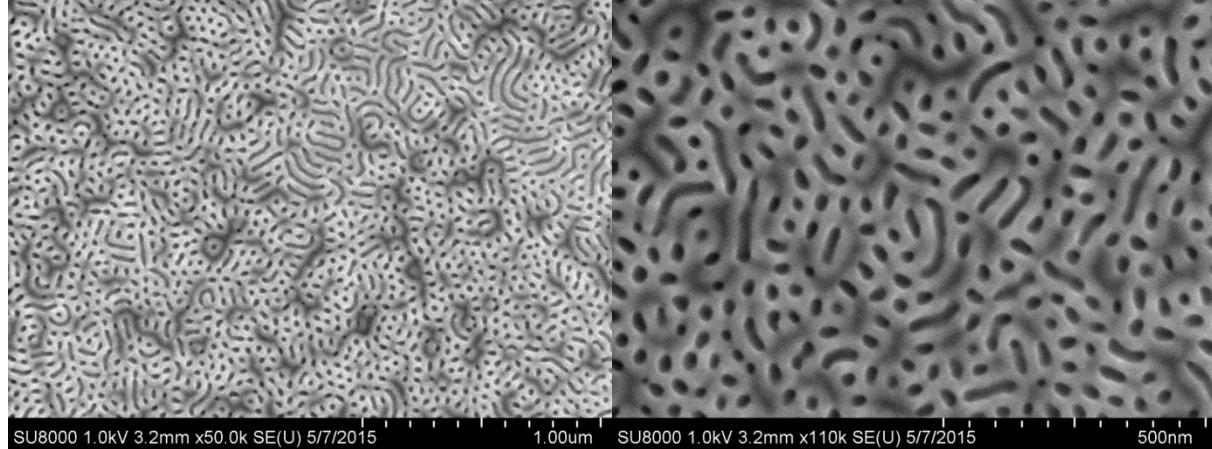
**W33F (N-U) -  $T_{a,RTP} = 250^\circ\text{C}$ ;  $t_{a,RTP} = 30 \text{ min} \rightarrow T_{a,VA\_C} = 190^\circ\text{C}$ ;  $t_{a,VA\_C} = 2 \text{ h}$ ;**

$h_{R10.5} \leq 8.7 \text{ nm}$ ;  $h_{B82} = 41.7 \text{ nm}$



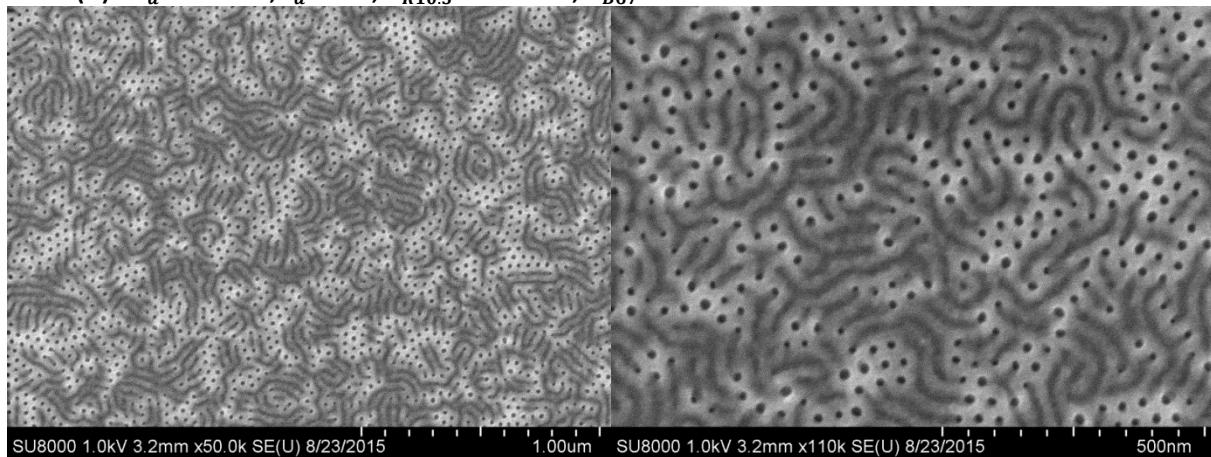
**A2.25 Sequential RTP-SVA-RTP anneal of B82 sample**

W27D ( $\approx$ U) –  $T_{a,RTP1} = 250^\circ\text{C}$ ,  $t_{a,RTP1} = 15\text{ min} \rightarrow$  SVA: Anisole,  $T_{a,SVA} = 60^\circ\text{C}$ ,  $t_{a,SVA} = 20\text{ min} \rightarrow$   $T_{a,RTP1} = 250^\circ\text{C}$ ,  $t_{a,RTP1} = 15\text{ min}$ ;  $h_{R10.5} = 7.5\text{ nm}$ ;  $h_{B82} = 44.0\text{ nm}$

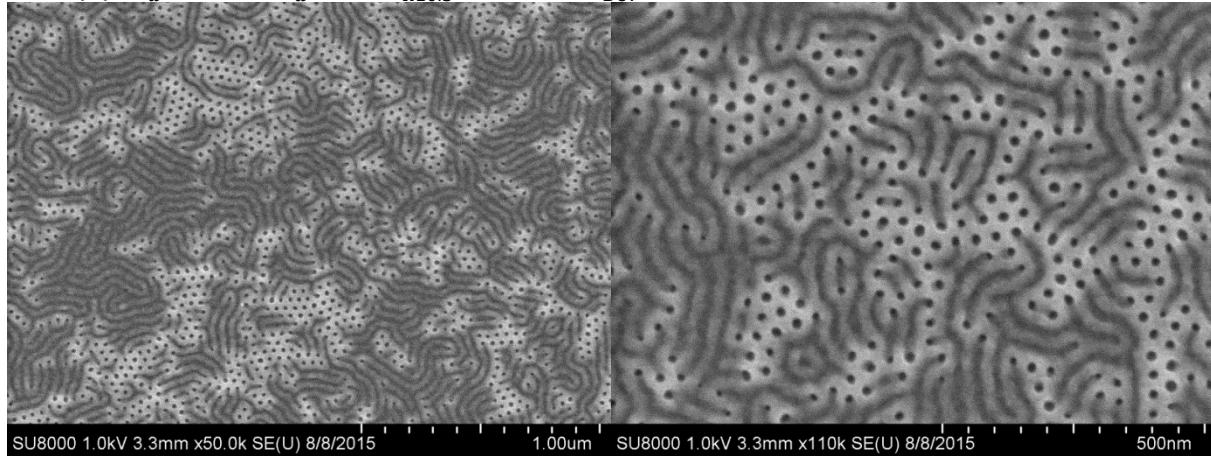


**A2.26 RTP temperature ( $T_a$ ) sweep of B67 ( $h_{B67} \approx L_{0,B67}$ ) samples**

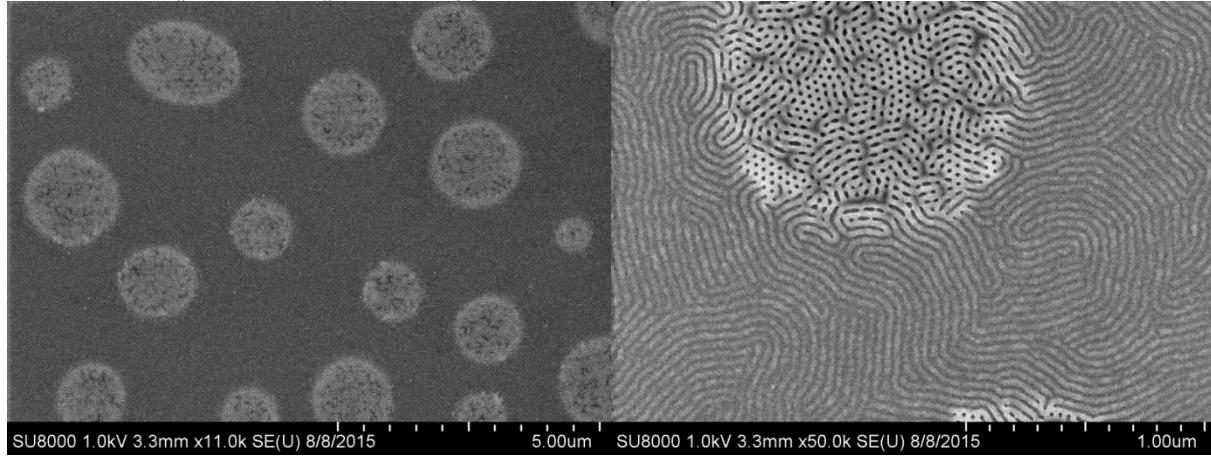
W51F (U) -  $T_a = 210^\circ C$ ;  $t_a = 1\text{h}$ ;  $h_{R10.5} = 7.4\text{ nm}$ ;  $h_{B67} = 35.0\text{ nm}$



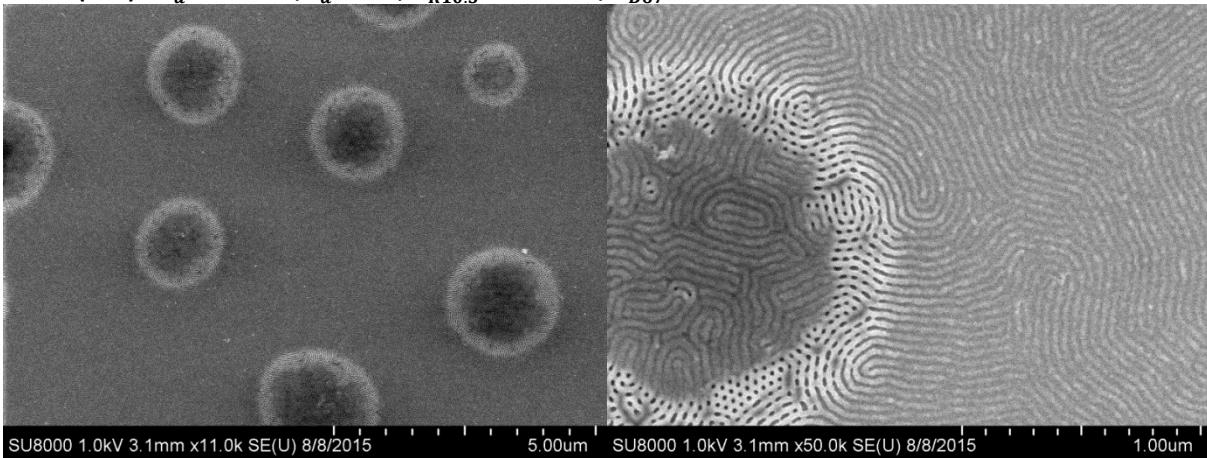
W51E (U) -  $T_a = 230^\circ C$ ;  $t_a = 1\text{h}$ ;  $h_{R10.5} = 7.4\text{ nm}$ ;  $h_{B67} = 35.0\text{ nm}$



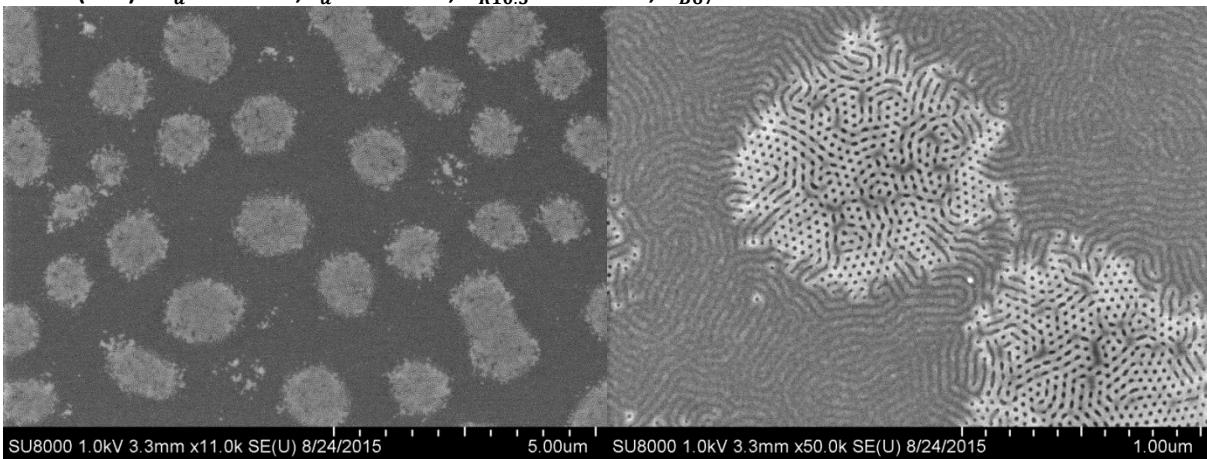
W51C (N-U) -  $T_a = 250^\circ C$ ;  $t_a = 1\text{h}$ ;  $h_{R10.5} = 7.4\text{ nm}$ ;  $h_{B67} = 35.0\text{ nm}$



**W51D (N-U) -  $T_a = 270^\circ C$ ;  $t_a = 1\text{h}$ ;  $h_{R10.5} = 7.4\text{ nm}$ ;  $h_{B67} = 35.0\text{ nm}$**

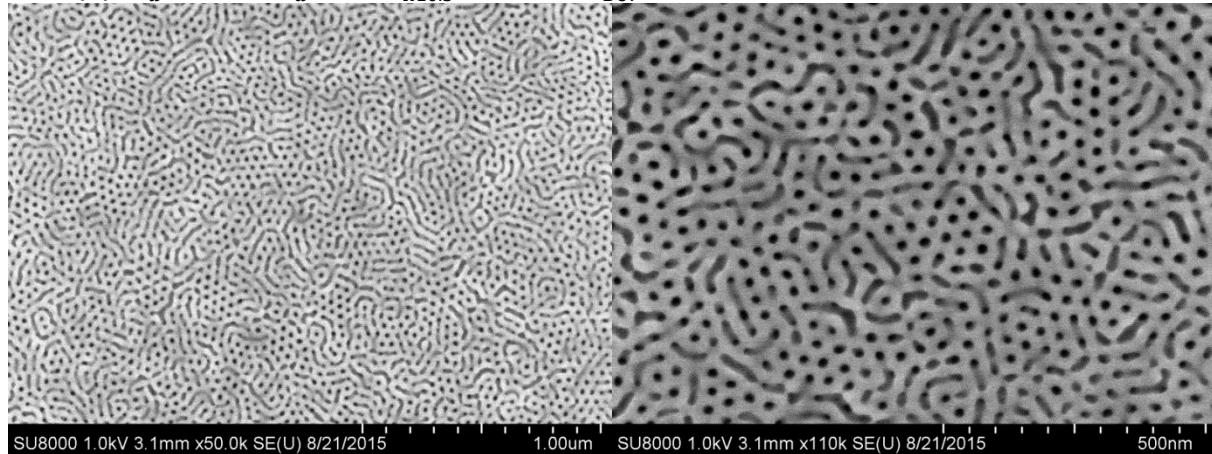


**W51H (N-U) -  $T_a = 270^\circ C$ ;  $t_a = 10\text{ min}$ ;  $h_{R10.5} = 7.4\text{ nm}$ ;  $h_{B67} = 35.0\text{ nm}$**

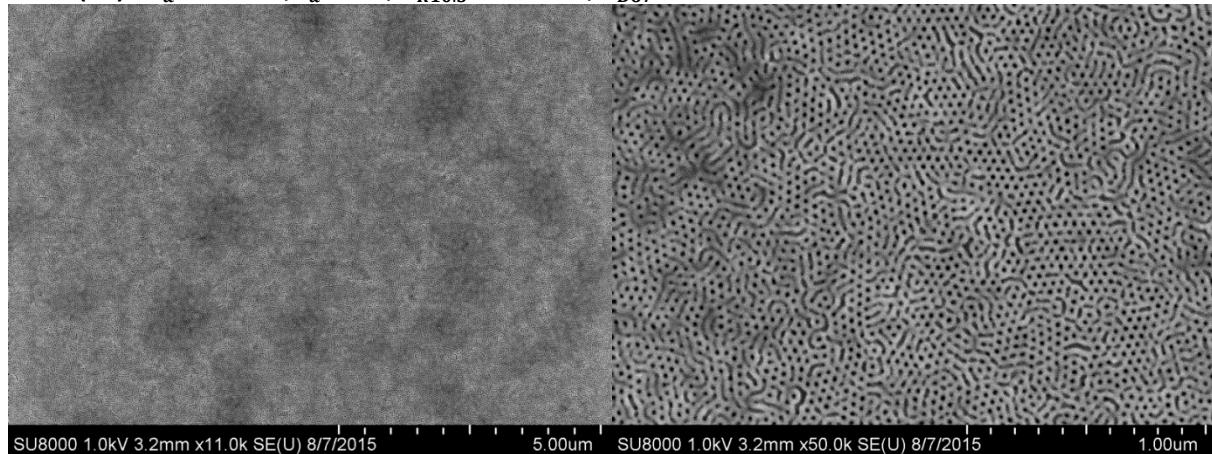


**A2.27 RTP temperature ( $T_a$ ) sweep of B67 ( $h_{B67} \approx 2L_{0,B67}$ ) samples**

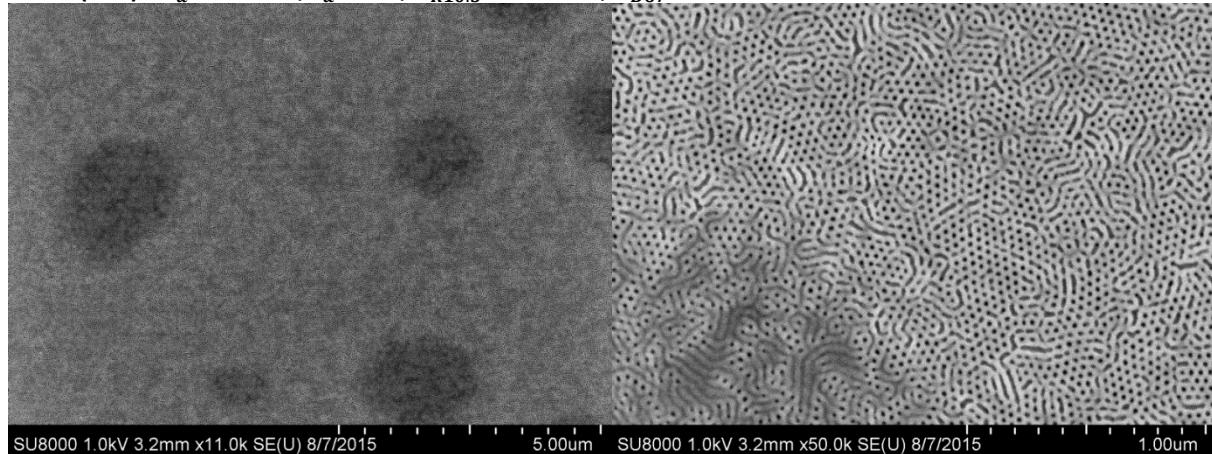
W50F (U) -  $T_a = 210^\circ C$ ;  $t_a = 1\text{h}$ ;  $h_{R10.5} = 7.8\text{ nm}$ ;  $h_{B67} = 73.0\text{ nm}$



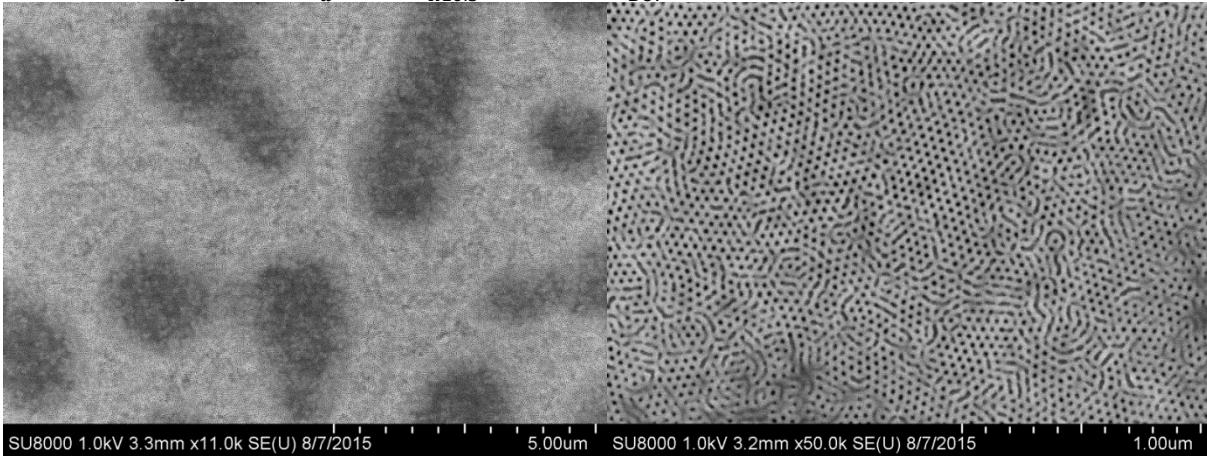
W50E (≈U) -  $T_a = 230^\circ C$ ;  $t_a = 1\text{h}$ ;  $h_{R10.5} = 7.8\text{ nm}$ ;  $h_{B67} = 73.0\text{ nm}$



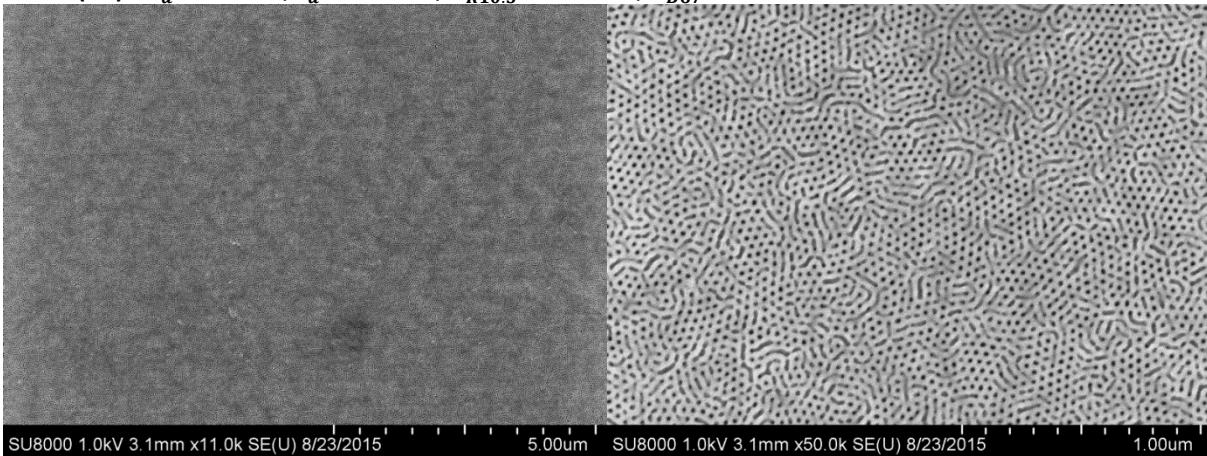
W50C (N-U) -  $T_a = 250^\circ C$ ;  $t_a = 1\text{h}$ ;  $h_{R10.5} = 7.8\text{ nm}$ ;  $h_{B67} = 73.0\text{ nm}$



**W50D (N-U) -  $T_a = 270^\circ C$ ;  $t_a = 1\text{h}$ ;  $h_{R10.5} = 7.8\text{ nm}$ ;  $h_{B67} = 73.0\text{ nm}$**

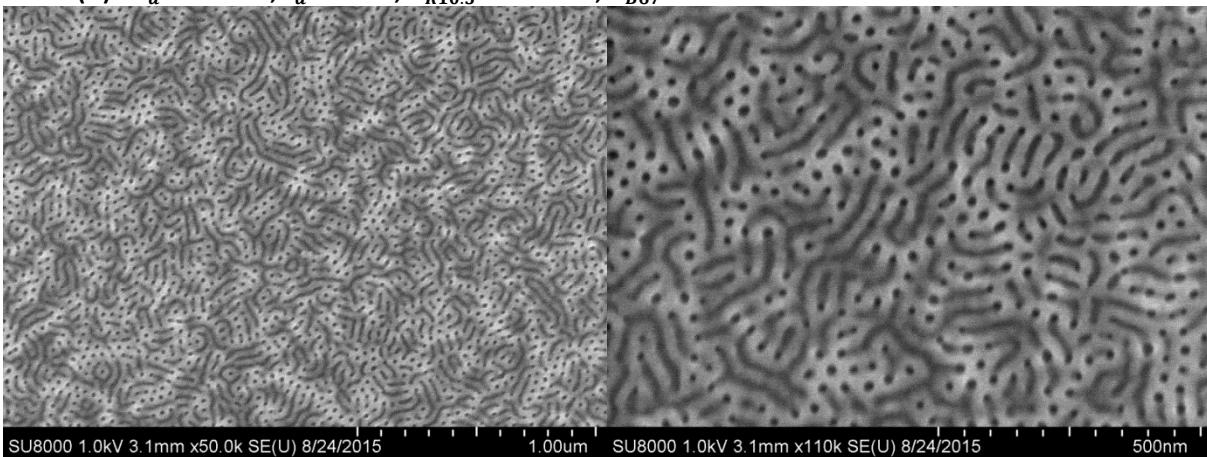


**W50H ( $\approx$ U) -  $T_a = 270^\circ C$ ;  $t_a = 10\text{ min}$ ;  $h_{R10.5} = 7.8\text{ nm}$ ;  $h_{B67} = 73.0\text{ nm}$**

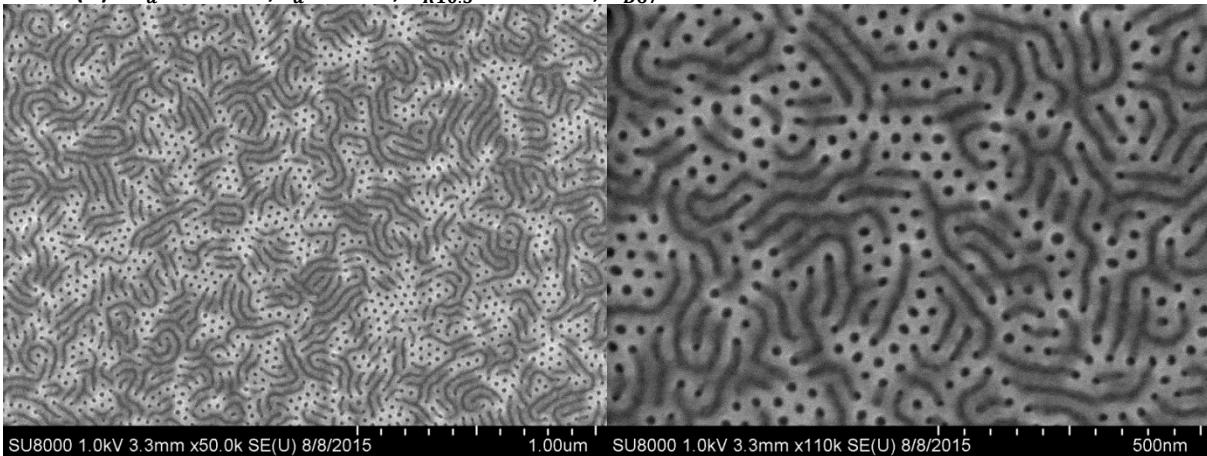


**A2.28** Vacuum oven  $T_a$ -sweep at  $t_a = 24$  h of B67 ( $h_{B67} \approx L_{0,B67}$ ) samples

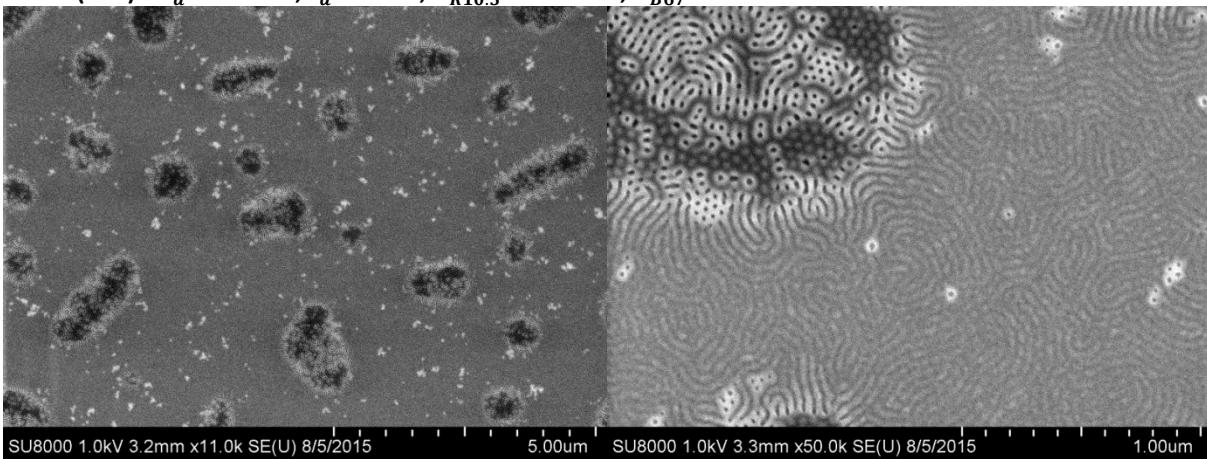
W51G (U) -  $T_a = 150^\circ\text{C}$ ;  $t_a = 24$  h;  $h_{R10.5} = 7.4$  nm;  $h_{B67} = 35.0$  nm



W51B (U) -  $T_a = 170^\circ\text{C}$ ;  $t_a = 25$  h;  $h_{R10.5} = 7.4$  nm;  $h_{B67} = 35.0$  nm

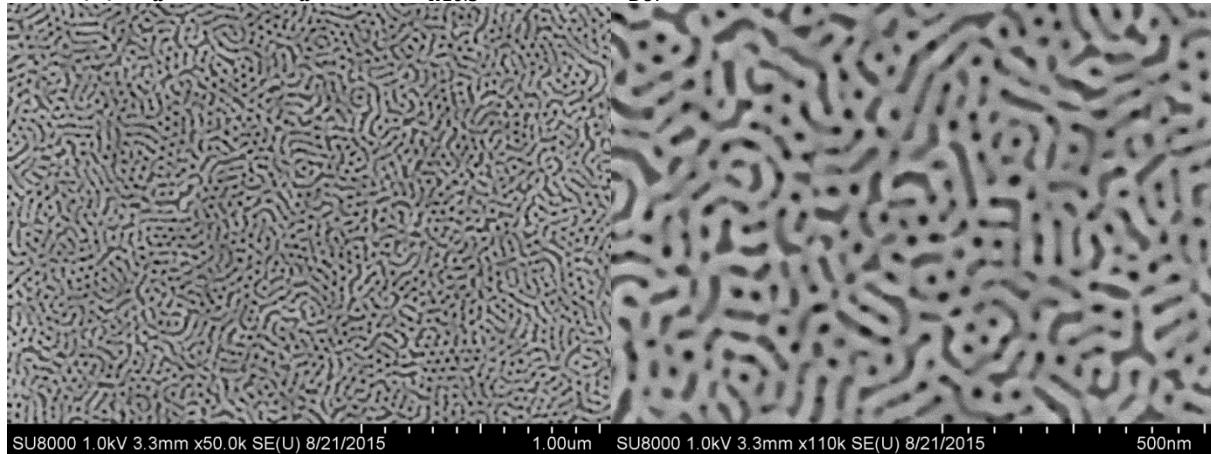


W51A (N-U) -  $T_a = 190^\circ\text{C}$ ;  $t_a = 24$  h;  $h_{R10.5} = 7.4$  nm;  $h_{B67} = 35.0$  nm

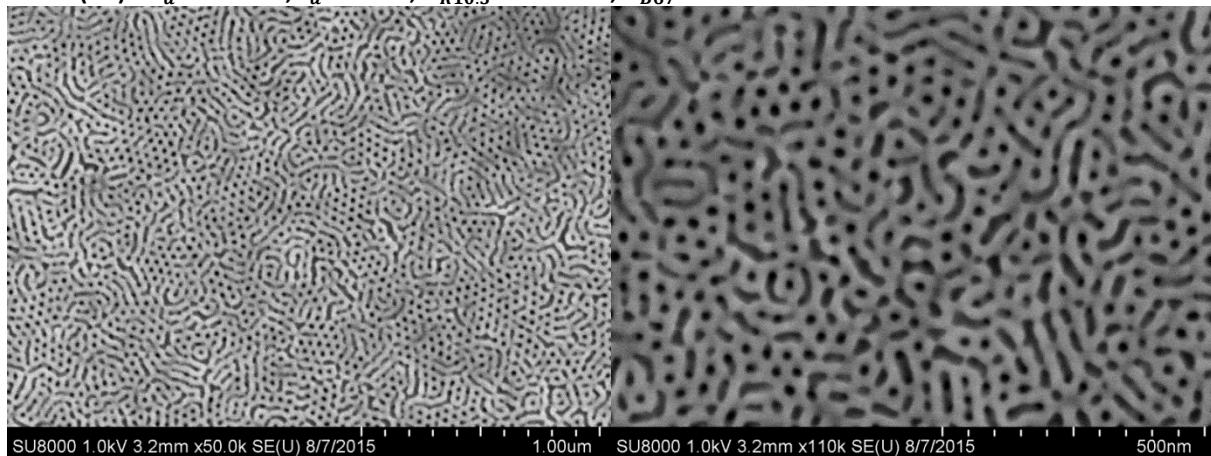


**A2.29** Vacuum oven  $T_a$ -sweep at  $t_a = 24$  h of B67 ( $h_{B67} \approx 2L_{0,B67}$ ) samples

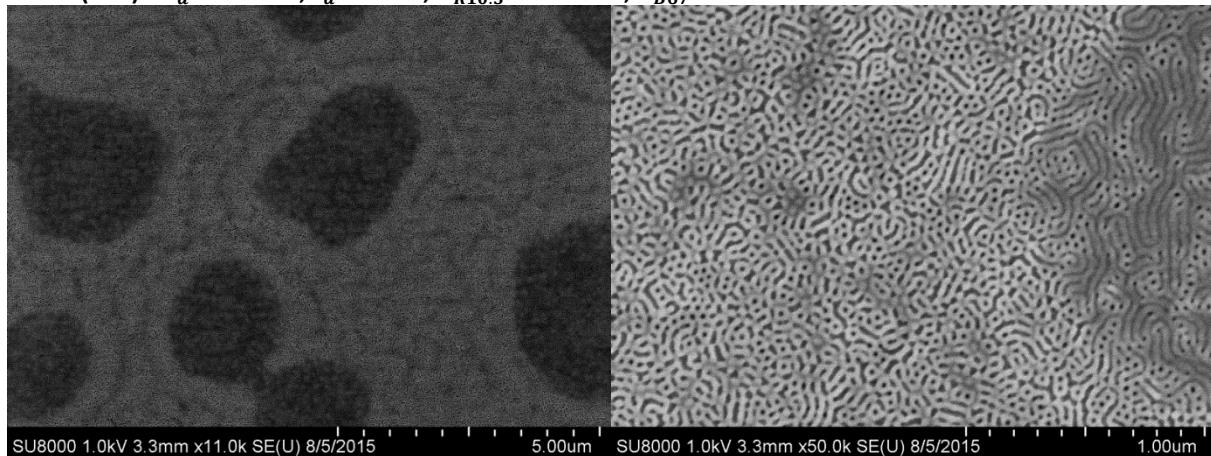
W50G (U) -  $T_a = 150^\circ\text{C}$ ;  $t_a = 24$  h;  $h_{R10.5} = 7.8$  nm;  $h_{B67} = 73.0$  nm



W50B ( $\approx$ U) -  $T_a = 170^\circ\text{C}$ ;  $t_a = 25$  h;  $h_{R10.5} = 7.8$  nm;  $h_{B67} = 73.0$  nm

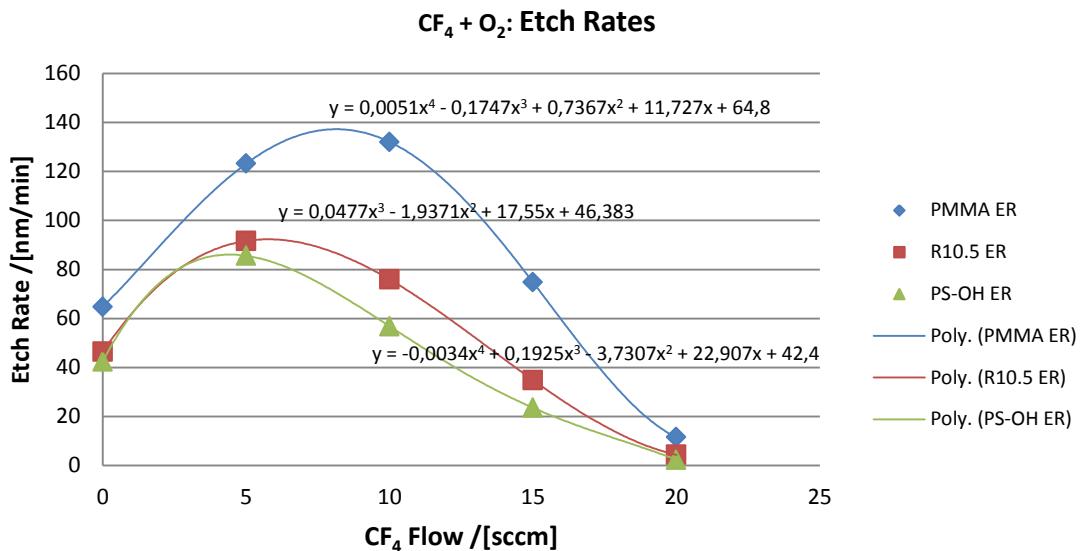


W50A (N-U) -  $T_a = 190^\circ\text{C}$ ;  $t_a = 24$  h;  $h_{R10.5} = 7.8$  nm;  $h_{B67} = 73.0$  nm

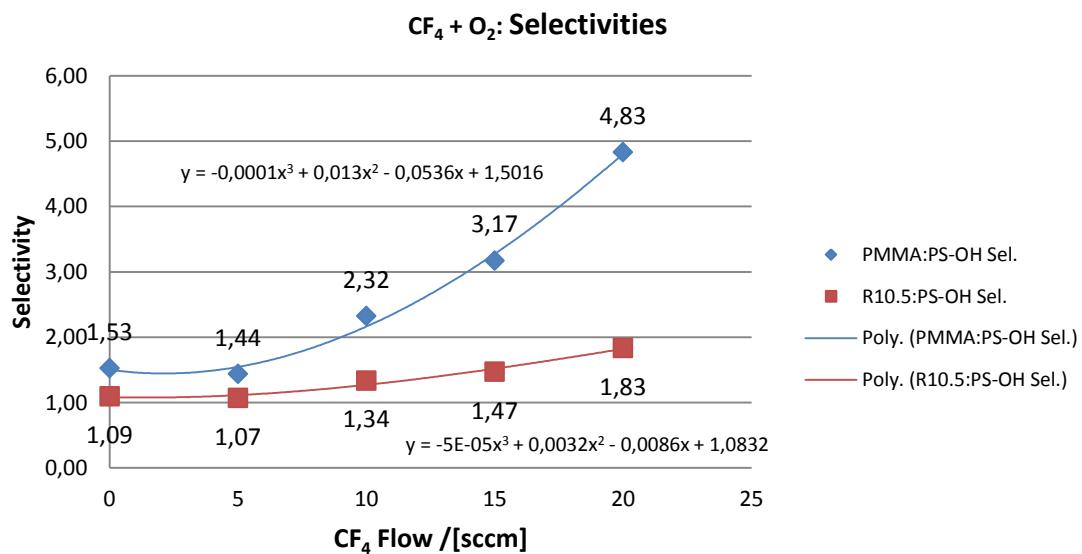


**APPENDIX A3**  
**Selective Block and Brush**  
**Removal Using RIE**

### A3.1 CF<sub>4</sub>/O<sub>2</sub> RIE Screening – ER Plot



### A3.2 CF<sub>4</sub>/O<sub>2</sub> RIE Screening – Selectivity Plot



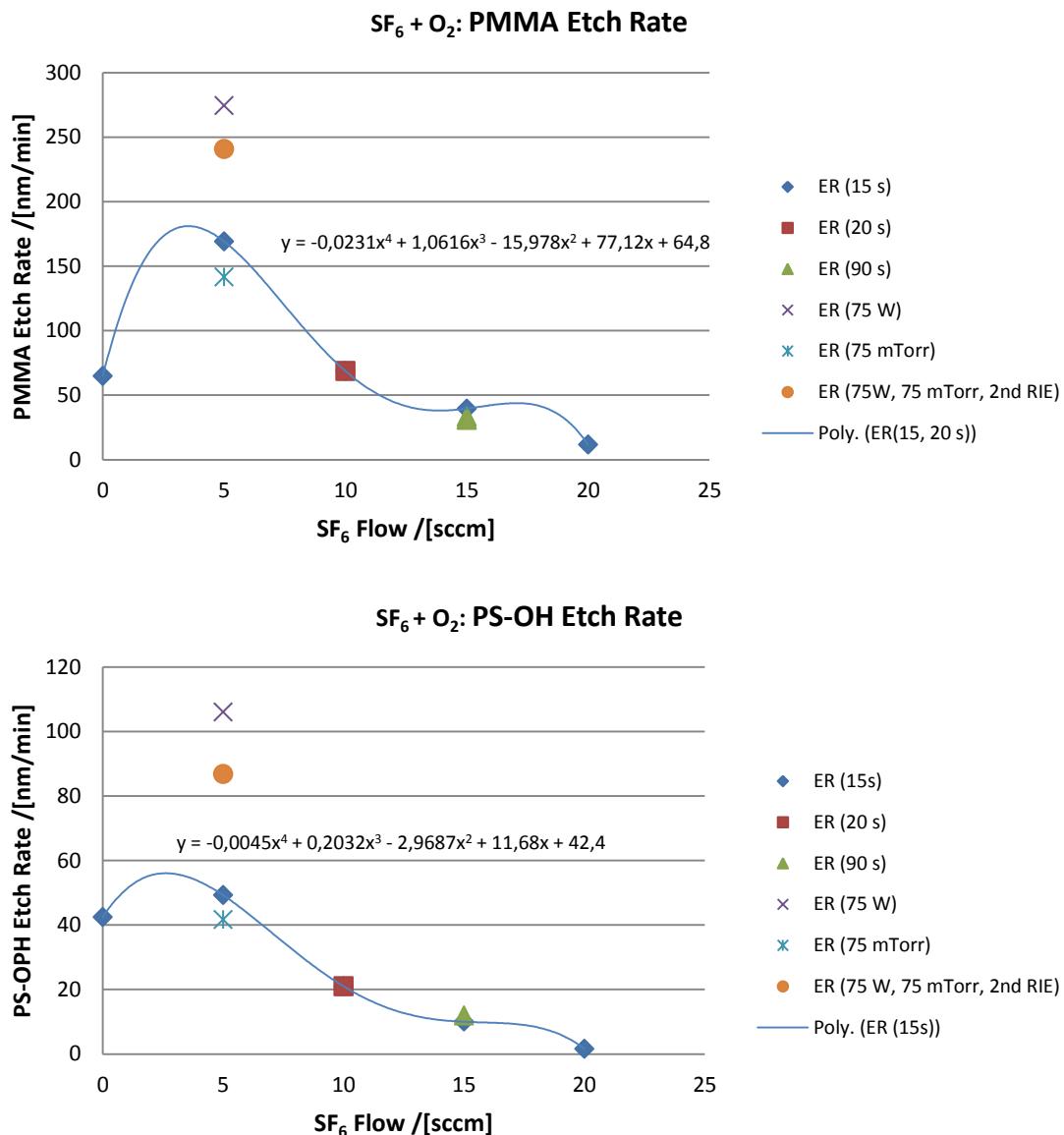
### A3.3 CF<sub>4</sub>/O<sub>2</sub> RIE Screening – Selectivities

Exp. #	Samples in run	Time /[s]	Power /[W] (Nom./Frwd./Ref.)	Pressure /[mTorr]	O <sub>2</sub> /[sccm]	CF <sub>4</sub> /[sccm]	Selectivity PMMA:PS-OH	Selectivity R10.5:PS-OH
1	W1A;W3A;W4A	15	30/18-19/0	100	20	0	1.53	1.09
2	W1B;W3B;W4B	15	30/18-19/3	100	15	5	1.44	1.07
3	W1C;W3C;W4C	15	30/19/3-5	100	10	10	2.32	1.34
4	W2A;W3E;W4E	15	30/18-19/2-7	100	5	15	3.17	1.47
5	W2B;W3F;W4F	15	30/18-19/0	100	0	20	4.83	1.83

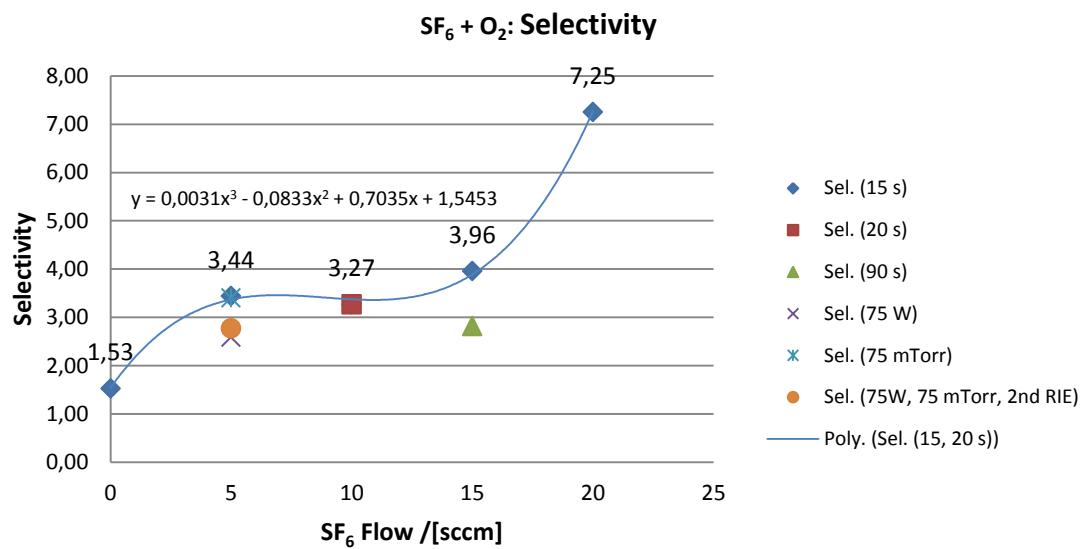
### A3.4 CF<sub>4</sub>/O<sub>2</sub> RIE Screening – Etch Rates

Exp. #	Sample #	Material	Time /[s]	Power /[W] (Nom./Fwd./Ref.)	Pressure /[mTorr]	O <sub>2</sub> /[sccm]	CF <sub>4</sub> /[sccm]	Before h <sub>1</sub> /[nm]	After h <sub>2</sub> /[nm]	Δh /[nm]	Etch rate /[nm min <sup>-1</sup> ]
1	W1A	PMMA	15	30/18-19/0	100	20	0	224.6	208.4	16.2	64.8
2	W1B	PMMA	15	30/18-19/3	100	15	5	224.9	194.1	30.8	123.2
3	W1C	PMMA	15	30/19/3-5	100	10	10	224.6	191.6	33	132
4	W2A	PMMA	15	30/18-19/2-7	100	5	15	224	205.3	18.7	74.8
5	W2B	PMMA	15	30/18-19/0	100	0	20	224.4	221.5	2.9	11.6
1	W3A	R10.5	15	30/18-19/0	100	20	0	38.5	26.9	11.6	46.4
2	W3B	R10.5	15	30/18-19/3	100	15	5	38.7	15.8	22.9	91.6
3	W3C	R10.5	15	30/19/3-5	100	10	10	37.7	18.7	19	76
4	W3E	R10.5	15	30/18-19/2-7	100	5	15	38	29.3	8.7	34.8
5	W3F	R10.5	15	30/18-19/0	100	0	20	37.6	36.5	1.1	4.4
1	W4A	PS-OH	15	30/18-19/0	100	20	0	37.2	26.6	10.6	42.4
2	W4B	PS-OH	15	30/18-19/3	100	15	5	36.6	15.2	21.4	85.6
3	W4C	PS-OH	15	30/19/3-5	100	10	10	36.9	22.7	14.2	56.8
4	W4E	PS-OH	15	30/18-19/2-7	100	5	15	36.7	30.8	5.9	23.6
5	W4F	PS-OH	15	30/18-19/0	100	0	20	37.1	36.5	0.6	2.4

### A3.5 SF<sub>6</sub>/O<sub>2</sub> RIE Screening – ER Plots



### A3.6 SF<sub>6</sub>/O<sub>2</sub> RIE Screening – Selectivity Plot



### A3.7 SF<sub>6</sub>/O<sub>2</sub> RIE Screening – Selectivities

Exp. #	Samples in run	Time /[s]	Power /[W] (Nom./Fwd./Ref.)	Pressure /[mTorr]	O <sub>2</sub> /[sccm]	SF <sub>6</sub> /[sccm]	Selectivity PMMA:PS-OH
1	W1A;W3A;W4A	15	30/18-19/0	100	20	0	1,53
2	W2C;W7A	15	30/19/1	100	15	5	3,44
3	W2D;W7B	15	30/18-19/1	100	5	15	3,96
4	W5A;W7C	15	30/19/1	100	0	20	7,25
5	W6C;W8E	90	30/19/1	100	5	15	2,82
6	<b>W5C 2nd RIE;W7E 2nd RIE</b>	90	30/19/1	100	5	15	2,71
7	W6D;W8F	20	30/18-19/1	100	10	10	3,27
8	W10C;W9E	15	<b>75/64-65/1-4</b>	100	15	5	2,59
9	W10D;W9F	15	30/19/1	<b>75</b>	15	5	3,40
10	W6D 2nd RIE; W8F 2nd RIE	15	<b>75/64/5-8</b>	<b>75</b>	15	5	2,77

### A3.8 SF<sub>6</sub>/O<sub>2</sub> RIE Screening – PMMA (50 kg/mol) Etch Rates

Exp. #	Sample #	Material	Time /[s]	Power /[W] (Nom./Frwd./Ref.)	Pressure /[mTorr]	O <sub>2</sub> /[sccm]	SF <sub>6</sub> /[sccm]	Before h <sub>1</sub> /[nm]	After h <sub>2</sub> /[nm]	Δh /[nm]	Etch rate /[nm min <sup>-1</sup> ]
2	W2C	PMMA	15	30/19/1	100	15	5	224,4	182,1	42,3	169,2
3	W2D	PMMA	15	30/18-19/1	100	5	15	225,5	215,6	9,9	39,6
4	W5A	PMMA	15	30/19/1	100	0	20	223	220,1	2,9	11,6
5	W6C	PMMA	90	30/19/1	100	5	15	221,7	171,5	50,2	33,5
6	<b>W5C 2nd RIE</b>	PMMA	90	30/19/1	100	5	15	197,4	150,8	46,6	31,1
7	W6D	PMMA	20	30/18-19/1	100	10	10	220,6	197,7	22,9	68,7
8	W10C	PMMA	15	<b>75/64-65/1-4</b>	100	15	5	216,1	147,5	68,6	274,4
9	W10D	PMMA	15	30/19/1	<b>75</b>	15	5	216,1	180,7	35,4	141,6
10	<b>W6D 2nd RIE</b>	PMMA	15	<b>75/64/5-8</b>	<b>75</b>	15	5	197,7	137,5	60,2	240,8

### A3.9 SF<sub>6</sub>/O<sub>2</sub> RIE Screening – PS-OH (1.2 kg/mol) Etch Rates

Exp. #	Sample #	Material	Time /[s]	Power / [W] (Nom./Frwd./Ref.)	Pressure /[mTorr]	O <sub>2</sub> /[sccm]	SF <sub>6</sub> /[sccm]	Before h <sub>1</sub> /[nm]	After h <sub>2</sub> /[nm]	Δh / [nm]	Etch rate / [nm min <sup>-1</sup> ]
2	W7A	PS-OH	15	30/19/1	100	15	5	36,4	24,1	12,3	49,2
3	W7B	PS-OH	15	30/18-19/1	100	5	15	36,5	34	2,5	10
4	W7C	PS-OH	15	30/19/1	100	0	20	36,4	36	0,4	1,6
5	W8E	PS-OH	90	30/19/1	100	5	15	37,2	19,4	17,8	11,9
6	W7E 2nd RIE	PS-OH	90	30/19/1	100	5	15	27,4	10,2	17,2	11,5
7	W8F	PS-OH	20	30/18-19/1	100	10	10	36,8	29,8	7	21
8	W9E	PS-OH	15	75/64-65/1-4	100	15	5	36,3	9,8	26,5	106
9	W9F	PS-OH	15	30/19/1	75	15	5	36,3	25,9	10,4	41,6
10	W8F 2nd RIE	PS-OH	15	75/64/5-8	75	15	5	29,8	8,1	21,7	86,8

### A3.10 SF<sub>6</sub>/O<sub>2</sub> RIE DOE – Selectivities

Exp #	Run Order	Samples in run	Time / [s]	Power / [W] (Nom./Fwd./Ref.)	Pressure / [mTorr]	O <sub>2</sub> / [sccm]	SF <sub>6</sub> / [sccm]	Selectivity PMMA:PS-OH	Selectivity R10.5:PS-OH
1	1	W12A;W18A;W14A	15	30/19/0	75	18	2	1.602	1.122
11	2	W12B;W18B;W14B	20	30/19/1	100	15	5	3.547	1.460
7	3	W12C;W18C;W14C	25	30/18-19/1	75	12	8	3.204	1.408
2	4	W12D;W18D;W14D	15	30/19/0	125	18	2	1.639	1.120
10	5	W12E;W18E;W14E	20	30/19/1	100	15	5	3.611	1.465
2 (2 <sup>nd</sup> )	6	W12F;W18F;W14F	15	30/19/1	125	18	2	2.146	1.269
8	7	W13A;W31A;W32A	25	30/18-19/2	125	12	8	3.289	1.430
3	8	W13B;W31B;W32B	15	30/19/1	75	12	8	3.172	1.422
9	9	W13C;W31C;W32C	20	30/19/1	100	15	5	3.486	1.450
6	10	W13D;W31D;W32D	25	30/18-19/1	125	18	2	2.253	1.288
5	11	W13E;W31E;W32E	25	30/18-19/0-1	75	18	2	2.449	1.346
4	12	W13F;W31F;W32F	15	30/19/1	125	12	8	3.413	1.453
C17	13	W38A;W37A;W36A	20	30/19/1	100	15	5	3.541	1.486
C16	14	W38B;W37B;W36B	25	30/18-19/1	100	15	5	3.649	1.526
C15	15	W38C;W37C;W36C	15	30/18-19/1	100	15	5	3.418	1.445
C13	16	W38D;W37D;W36D	20	30/18-19/0	100	18	2	2.297	1.336
C14	17	W38E;W37E;W36E	20	30/19/1	100	12	8	3.292	1.438
N18	18	W38F;W37F;W36F	12	30/19/1	75	13	7	3.269	1.358
N19	19	W44A;W43A;W42A	9	30/19/1	75	13	7	3.551	1.449
DUV1	20	W44B;W43B;W42B	15	30/19/1	100	15	5	3.213	1.451
DUV2	21	W44C;W43C;W42C	20	30/19/1	100	15	5	3.237	1.450
DUV3	22	W44D;W43D;W42D	20	30/19/1	100	12	8	3.034	1.432
DUV4	23	W44E;W43E;W42E	9	30/18-19/1	75	13	7	3.096	1.519
DUV5	24	W44F;W43F;W42F	6	30/19/1	75	14	6	3,367	1,462

**A3.11** SF<sub>6</sub>/O<sub>2</sub> RIE DOE – Non-DUV Exposed PMMA (50 kg/mol) Etch Data

Exp #	Run Order	Sample #	Material	Time /[s]	Power /[W] (Nom./Fwd./Ref.)	Pressure /[mTorr]	O <sub>2</sub> /[sccm]	SF <sub>6</sub> /[sccm]	Before h <sub>1</sub> /[nm]	After h <sub>2</sub> /[nm]	Δh /[nm]	Etch rate /[nm·min <sup>-1</sup> ]
1	1	W12A	PMMA	15	30/19/0	75	18	2	222.2	202.5	19.7	78.8
11	2	W12B	PMMA	20	30/19/1	100	15	5	223.5	170.3	53.2	159.6
7	3	W12C	PMMA	25	30/18-19/1	75	12	8	223.1	190.1	33.0	79.2
2	4	W12D	PMMA	15	30/19/0	125	18	2	223.0	209.4	13.6	54.4
10	5	W12E	PMMA	20	30/19/1	100	15	5	222.7	170.7	52.0	156.0
2 (2 <sup>nd</sup> )	6	W12F	PMMA	15	30/19/1	125	18	2	222.9	186.2	36.7	146.8
8	7	W13A	PMMA	25	30/18-19/2	125	12	8	220.6	183.1	37.5	90.0
3	8	W13B	PMMA	15	30/19/1	75	12	8	220.0	199.7	20.3	81.2
9	9	W13C	PMMA	20	30/19/1	100	15	5	219.9	171.1	48.8	146.4
6	10	W13D	PMMA	25	30/18-19/1	125	18	2	220.0	150.6	69.4	166.6
5	11	W13E	PMMA	25	30/18-19/0-1	75	18	2	220.4	148.9	71.5	171.6
4	12	W13F	PMMA	15	30/19/1	125	12	8	220.1	194.5	25.6	102.4
C17	13	W38A	PMMA	20	30/19/1	100	15	5	229.2	176.8	52.4	157.2
C16	14	W38B	PMMA	25	30/18-19/1	100	15	5	230.1	173.9	56.2	134.9
C15	15	W38C	PMMA	15	30/18-19/1	100	15	5	229.5	191.9	37.6	150.4
C13	16	W38D	PMMA	20	30/18-19/0	100	18	2	230.9	177.6	53.3	159.9
C14	17	W38E	PMMA	20	30/19/1	100	12	8	230.1	200.8	29.3	87.9
N18	18	W38F	PMMA	12	30/19/1	75	13	7	230	208.1	21.9	109.5
N19	19	W44A	PMMA	9	30/19/1	75	13	7	222.8	205.4	17.4	116.0

**A3.12** SF<sub>6</sub>/O<sub>2</sub> RIE – DUV Exposed PMMA (50 kg/mol) Etch Data

Exp #	Run Order	Sample #	Material	Time /[s]	Power /[W] (Nom./Fwd./Ref.)	Pressure /[mTorr]	O <sub>2</sub> /[sccm]	SF <sub>6</sub> /[sccm]	Before DUV h <sub>1</sub> /[nm]	After DUV h <sub>2</sub> /[nm]	Δh <sub>DUV</sub> /[%]	After RIE h <sub>3</sub> /[nm]	Δh <sub>RIE</sub> /[nm]	Etch rate /[nm min <sup>-1</sup> ]	
DUV1	20	W44B	PMMA	15	30/19/1	100	15	5	222.6	206.7	NA	NA	167.5*	39.2	156.8
DUV2	21	W44C	PMMA	20	30/19/1	100	15	5	222.0	206.1	NA	NA	163.7*	42.4	127.2
DUV3	22	W44D	PMMA	20	30/19/1	100	12	8	222.5	206.6	NA	NA	179.9*	26.7	80.1
DUV4	23	W44E	PMMA	9	30/18-19/1	75	13	7	222.3	206.4	NA	NA	190.3*	16.1	107.3
DUV5	24	W44F	PMMA	6	30/19/1	75	14	6	222.6	206.7	15.9	7.14	190.1	16.6	166.2

### A3.13 SF<sub>6</sub>/O<sub>2</sub> RIE DOE – Non-DUV Exposed R10.5 Etch Data

Exp #	Run Order	Sample #	Material	Time /[s]	Power /[W] (Nom./Fwd./Ref.)	Pressure /[mTorr]	O <sub>2</sub> /[sccm]	SF <sub>6</sub> /[sccm]	Before h <sub>1</sub> /[nm]	After h <sub>2</sub> /[nm]	Δh /[nm]	Etch rate /[nm·min <sup>-1</sup> ]
1	1	W18A	P(S-r-MMA)	15	30/19/0	75	18	2	32.5	18.7	13.8	55.2
11	2	W18B	P(S-r-MMA)	20	30/19/1	100	15	5	32.3	10.4	21.9	65.7
7	3	W18C	P(S-r-MMA)	25	30/18-19/1	75	12	8	31.8	17.3	14.5	34.8
2	4	W18D	P(S-r-MMA)	15	30/19/0	125	18	2	32.9	23.6	9.3	37.2
10	5	W18E	P(S-r-MMA)	20	30/19/1	100	15	5	32.3	11.2	21.1	63.3
2 (2 <sup>nd</sup> )	6	W18F	P(S-r-MMA)	15	30/19/1	125	18	2	32.7	11.0	21.7	86.8
8	7	W31A	P(S-r-MMA)	25	30/18-19/2	125	12	8	39.7	23.4	16.3	39.1
3	8	W31B	P(S-r-MMA)	15	30/19/1	75	12	8	39.6	30.5	9.1	36.4
9	9	W31C	P(S-r-MMA)	20	30/19/1	100	15	5	40.3	20.0	20.3	60.9
6	10	W31D	P(S-r-MMA)	25	30/18-19/1	125	18	2	39.8	0.1	39.7	95.2
E5	11	W31E	P(S-r-MMA)	25	30/18-19/0-1	75	18	2	40.7	1.4	39.3	94.3
4	12	W31F	P(S-r-MMA)	15	30/19/1	125	12	8	40.0	29.1	10.9	43.6
C17	13	W37A	P(S-r-MMA)	20	30/19/1	100	15	5	42.9	20.9	22.0	66.0
C16	14	W37B	P(S-r-MMA)	25	30/18-19/1	100	15	5	42.3	18.8	23.5	56.4
C15	15	W37C	P(S-r-MMA)	15	30/18-19/1	100	15	5	42.7	26.8	15.9	63.6
C13	16	W37D	P(S-r-MMA)	20	30/18-19/0	100	18	2	42.8	11.8	31.0	93.0
C14	17	W37E	P(S-r-MMA)	20	30/19/1	100	12	8	42.3	29.5	12.8	38.4
N18	18	W37F	P(S-r-MMA)	12	30/19/1	75	13	7	42.7	33.6	9.1	45.5
N19	19	W43A	P(S-r-MMA)	9	30/19/1	75	13	7	39.3	32.2	7.1	47.3

### A3.14 SF<sub>6</sub>/O<sub>2</sub> RIE – DUV Exposed R10.5 Etch Data

Exp #	Run Order	Sample #	Material	Time /[s]	Power /[W] (Nom./Fwd./Ref.)	Pressure /[mTorr]	O <sub>2</sub> /[sccm]	SF <sub>6</sub> /[sccm]	Before DUV h <sub>1</sub> /[nm]	After DUV h <sub>2</sub> /[nm]	Δh <sub>DUV</sub> /[nm]	Δh <sub>DUV</sub> /[%]	After RIE h <sub>3</sub> /[nm]	Δh <sub>RIE</sub> /[nm]	Etch rate /[nm min <sup>-1</sup> ]
DUV1	20	W43B	R10.5	15	30/19/1	100	15	5	39.6	37.4	NA	NA	19.7	17.7	70.8
DUV2	21	W43C	R10.5	20	30/19/1	100	15	5	38.9	36.7	NA	NA	17.7	19.0	57.0
DUV3	22	W43D	R10.5	20	30/19/1	100	12	8	39.1	36.9	NA	NA	24.3	12.6	37.8
DUV4	23	W43E	R10.5	9	30/18-19/1	75	13	7	39.5	37.3	NA	NA	29.4	7.9	52.7
DUV5	24	W43F	R10.5	6	30/19/1	75	14	6	39.5	37.5	2	5.06	30.3	7.2	72.2

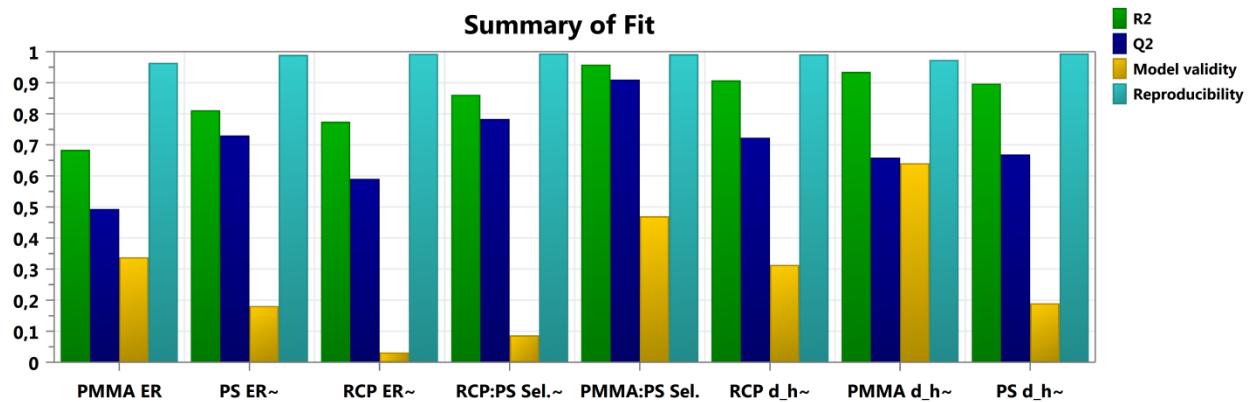
**A3.15 SF<sub>6</sub>/O<sub>2</sub> RIE DOE – Non-DUV Exposed PS-OH (1.2 kg/mol) Etch Data**

Exp #	Run Order	Sample #	Material	Time /[s]	Power /[W] (Nom./Fwd./Ref.)	Pressure /[mTorr]	O <sup>2</sup> /[sccm]	SF <sub>6</sub> /[sccm]	Before h <sup>1</sup> /[nm]	After h <sup>2</sup> /[nm]	Δh /[nm]	Etch rate /[nm·min <sup>-1</sup> ]
1	1	W14A	PS-OH	15	30/19/0	75	18	2	61.7	49.4	12.3	49.2
11	2	W14B	PS-OH	20	30/19/1	100	15	5	61.4	46.4	15.0	45.0
7	3	W14C	PS-OH	25	30/18-19/1	75	12	8	61.4	51.1	10.3	24.7
2	4	W14D	PS-OH	15	30/19/0	125	18	2	61.6	53.3	8.3	33.2
10	5	W14E	PS-OH	20	30/19/1	100	15	5	61.2	46.8	14.4	43.2
2 (2 <sup>nd</sup> )	6	W14F	PS-OH	15	30/19/1	125	18	2	61.4	44.3	17.1	68.4
8	7	W32A	PS-OH	25	30/18-19/2	125	12	8	63.6	52.2	11.4	27.4
3	8	W32B	PS-OH	15	30/19/1	75	12	8	63.7	57.3	6.4	25.6
9	9	W32C	PS-OH	20	30/19/1	100	15	5	63.5	49.5	14.0	42.0
6	10	W32D	PS-OH	25	30/18-19/1	125	18	2	63.5	32.7	30.8	73.9
5	11	W32E	PS-OH	25	30/18-19/0-1	75	18	2	63.5	34.3	29.2	70.1
4	12	W32F	PS-OH	15	30/19/1	125	12	8	63.4	55.9	7.5	30.0
C17	13	W36A	PS-OH	20	30/19/1	100	15	5	65.5	50.7	14.8	44.4
C16	14	W36B	PS-OH	25	30/18-19/1	100	15	5	65.5	50.1	15.4	37.0
C15	15	W36C	PS-OH	15	30/18-19/1	100	15	5	68.0	57.0	11.0	44.0
C13	16	W36D	PS-OH	20	30/18-19/0	100	18	2	66.1	42.9	23.2	69.6
C14	17	W36E	PS-OH	20	30/19/1	100	12	8	65.9	57.0	8.9	26.7
N18	18	W36F	PS-OH	12	30/19/1	75	13	7	67.6	60.9	6.7	33.5
N19	19	W42A	PS-OH	9	30/19/1	75	13	7	68.9	64.0	4.9	32.7

**A3.16 SF<sub>6</sub>/O<sub>2</sub> RIE – DUV Exposed PS-OH (1.2 kg/mol) Etch Data**

Exp #	Run Order	Sample #	Material	Time /[s]	Power /[W] (Nom./Fwd./Ref.)	Pressure /[mTorr]	O <sub>2</sub> /[sccm]	SF <sub>6</sub> /[sccm]	Before DUV h <sub>1</sub> /[nm]	After DUV h <sub>2</sub> /[nm]	Δh <sub>DUV</sub> /[nm]	Δh <sub>DUV</sub> /[%]	After RIE h <sub>3</sub> /[nm]	Δh <sub>RIE</sub> /[nm]	Etch rate /[nm min <sup>-1</sup> ]
DUV1	20	W42B	PS-OH	15	30/19/1	100	15	5	68.9	68.5	NA	NA	56.3	12.2	48.8
DUV2	21	W42C	PS-OH	20	30/19/1	100	15	5	69.4	69	NA	NA	55.9	13.1	39.3
DUV3	22	W42D	PS-OH	20	30/19/1	100	12	8	69.2	68.8	NA	NA	60.0	8.8	26.4
DUV4	23	W42E	PS-OH	9	30/18-19/1	75	13	7	68.9	68.5	NA	NA	63.3	5.2	34.7
DUV5	24	W42F	PS-OH	6	30/19/1	75	14	6	69.4	69	0.4	0.58	64.1	4.9	49.4

### A3.17 SF<sub>6</sub> /O<sub>2</sub> RIE DOE – Summary of Fit



### A3.18 SF<sub>6</sub> /O<sub>2</sub> RIE DOE – Coefficients (Centered and Scaled)

PMMA Etch Rate	Coeff. SC	Std. Err.	P	Conf. int(±)	PS Etch Rate	Coeff. SC	Std. Err.	P	Conf. int(±)
Constant	143,864	9,11097	7,32E-10	19,6831	Constant	1,59481	0,0167322	4,28E-21	0,0358874
SF6 Flow	-18,3121	5,84758	0,00794878	12,6329	SF6 Flow	-0,127739	0,0172191	3,26E-06	0,0369317
Time	11,9798	5,90553	0,063499	12,7581	Time	0,0227649	0,0180227	0,227176	0,0386551
SF6*SF6	-24,3826	7,7104	0,00749208	16,6573	SF6*t	-0,042549	0,0184324	0,0367594	0,0395339
SF6*t	-15,7852	6,15017	0,023443	13,2867					

N = 18	Q2 =	0,494	Cond. no. =	3,163	N = 18	Q2 =	0,73	Cond. no. =	1,358
DF = 13	R2 =	0,684	RSD =	23,18	DF = 14	R2 =	0,812	RSD =	0,07099
Comp. = 2	R2 adj. =	0,587			Comp. = 2	R2 adj. =	0,771		
			Conf. lev. =	0,95				Conf. lev. =	0,95

RCP Etch Rate	Coeff. SC	Std. Err.	P	Conf. int(±)	RCP:PS Selectivity	Coeff. SC	Std. Err.	P	Conf. int(±)
Constant	-1,62479	0,0708003	6,65E-12	0,152955	Constant	4,31913	0,0730575	3,43E-17	0,157831
SF6 Flow	-0,218497	0,0454408	0,00034167	0,098169	SF6 Flow	0,218386	0,0468895	0,00044842	0,101299
Time	0,122809	0,0458912	0,0190422	0,0991419	Time	0,132197	0,0473542	0,0152717	0,102303
SF6*SF6	0,0765118	0,0599166	0,223949	0,129442	SF6*t	-0,319256	0,0618268	0,00018225	0,133569
SF6*t	-0,174281	0,0477923	0,00295623	0,103249					

N = 18	Q2 =	0,591	Cond. no. =	3,163	N = 18	Q2 =	0,783	Cond. no. =	3,163
DF = 13	R2 =	0,774	RSD =	0,1801	DF = 13	R2 =	0,861	RSD =	0,1858
Comp. = 2	R2 adj. =	0,705			Comp. = 2	R2 adj. =	0,818		
			Conf. lev. =	0,95				Conf. lev. =	0,95

PMMA:PS Selectivity	Coeff. SC	Std. Err.	P	Conf. int(±)	RCP $\Delta h$	Coeff. SC	Std. Err.	P	Conf. int(±)
<b>Constant</b>	3,53445	0,0634503	7,41E-17	0,137076	<b>Constant</b>	-1,91284	0,0037318	2,55E-31	0,0080039
<b>SF6 Flow</b>	0,398883	0,0407234	2,29E-07	0,0879777	<b>SF6 Flow</b>	-0,028243	0,0038404	3,60E-06	0,0082368
<b>Time</b>	0,110355	0,0411271	0,0187831	0,0888497	<b>Time</b>	0,0342567	0,0040196	6,51E-07	0,0086212
<b>SF6*SF6</b>	-0,544357	0,0536964	1,53E-07	0,116004	<b>SF6*t</b>	-0,023428	0,004111	5,50E-05	0,0088172
<b>SF6*t</b>	-0,095188	0,0428308	0,044619	0,0925304					

N = 18	Q2 =	0,91	Cond. no. =	3,163	N = 18	Q2 =	0,723	Cond. no. =	1,358
DF = 13	R2 =	0,959	RSD =	0,1614	DF = 14	R2 =	0,908	RSD =	0,01583
Comp. = 2	R2 adj. =	0,946			Comp. = 2	R2 adj. =	0,888		
			Conf. lev. =	0,95				Conf. lev. =	0,95

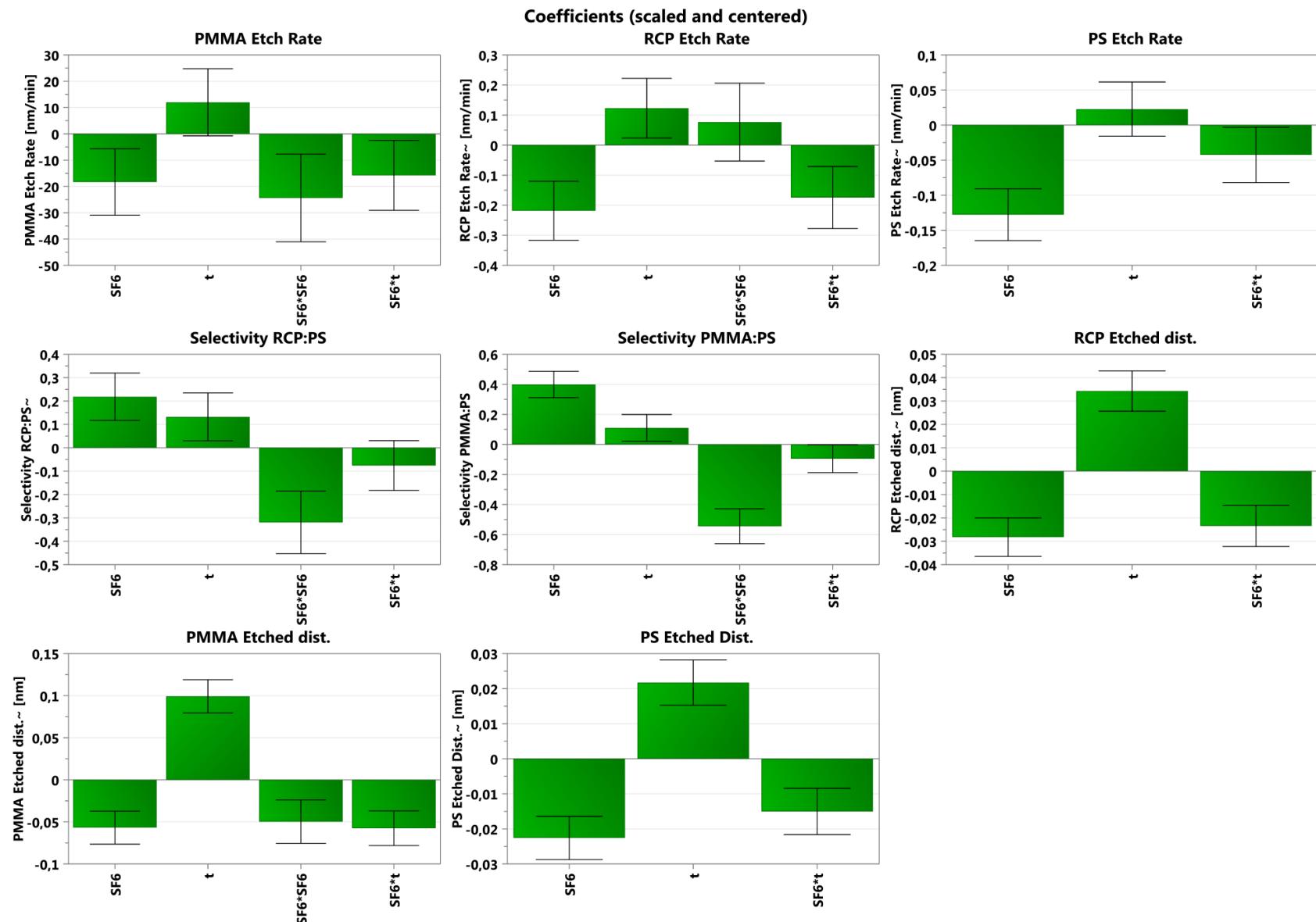
PMMA $\Delta h$	Coeff. SC	Std. Err.	P	Conf. int(±)	PS $\Delta h$	Coeff. SC	Std. Err.	P	Conf. int(±)
<b>Constant</b>	-1,73273	0,0141125	2,61E-21	0,0304883	<b>Constant</b>	-1,9389	0,0027904	3,61E-33	0,0059849
<b>SF6 Flow</b>	-0,056811	0,0090577	2,87E-05	0,0195679	<b>SF6 Flow</b>	-0,022582	0,0028716	1,67E-06	0,0061591
<b>Time</b>	0,0992172	0,0091474	6,95E-08	0,0197618	<b>Time</b>	0,0217116	0,0030056	4,40E-06	0,0064465
<b>SF6*SF6</b>	-0,049732	0,0119431	0,00111164	0,0258015	<b>SF6*t</b>	-0,015026	0,003074	0,00023951	0,006593
<b>SF6*t</b>	-0,057509	0,0095264	4,19E-05	0,0205805					

N = 18	Q2 =	0,659	Cond. no. =	3,163	N = 18	Q2 =	0,669	Cond. no. =	1,358
DF = 13	R2 =	0,935	RSD =	0,0359	DF = 14	R2 =	0,897	RSD =	0,01184
Comp. = 2	R2 adj. =	0,915			Comp. = 2	R2 adj. =	0,875		
			Conf. lev. =	0,95				Conf. lev. =	0,95

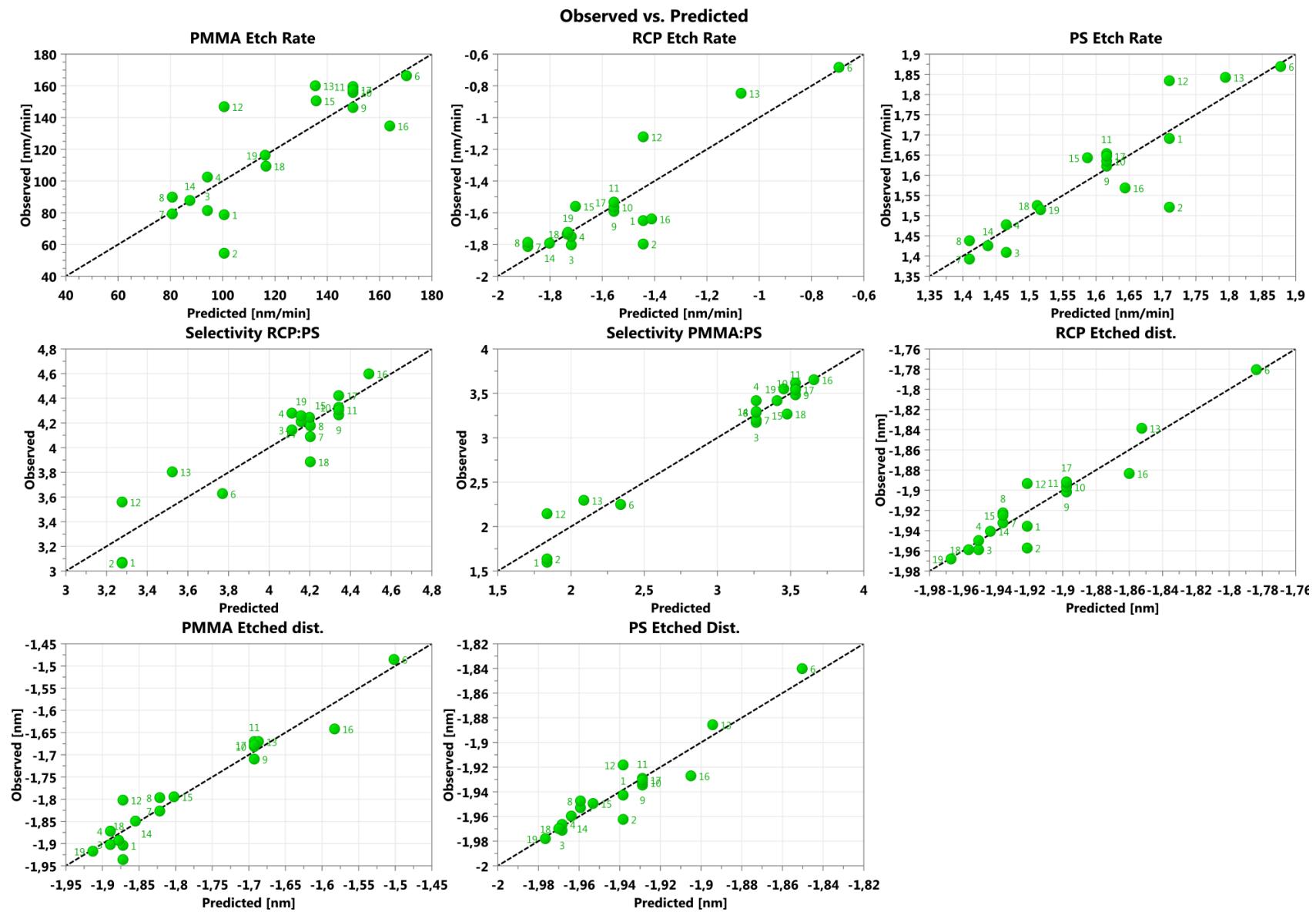
### A3.19 SF<sub>6</sub> / O<sub>2</sub> RIE MODDE DOE – Coefficients (Unscaled)

	PMMA Etch Rate	PS Etch Rate	RCP Etch Rate	RCP:PS Selectivity	PMMA:PS Selectivity	PMMA $\Delta h$	PS $\Delta h$	R10.5 $\Delta h$
<b>Constant</b>	-111,335	1,42859	-2,71987	1,17121	-1,1608	-2,71128	-2,09943	-2,17991
<b>SF6 Flow</b>	62,3314	0,015055	0,049264	0,797251	1,31542	0,159743	0,014742	0,0259
<b>Time</b>	9,72359	0,024217	0,105377	0,0623528	0,0666105	0,047053	0,011413	0,017879
<b>SF6*SF6</b>	-4,26835	-	0,013394	-0,0558881	-0,0952935	-0,00871	-	-
<b>SF6*t</b>	-1,38195	-0,00373	-0,01526	-0,006643	-0,0083335	-0,00503	-0,00132	-0,00205

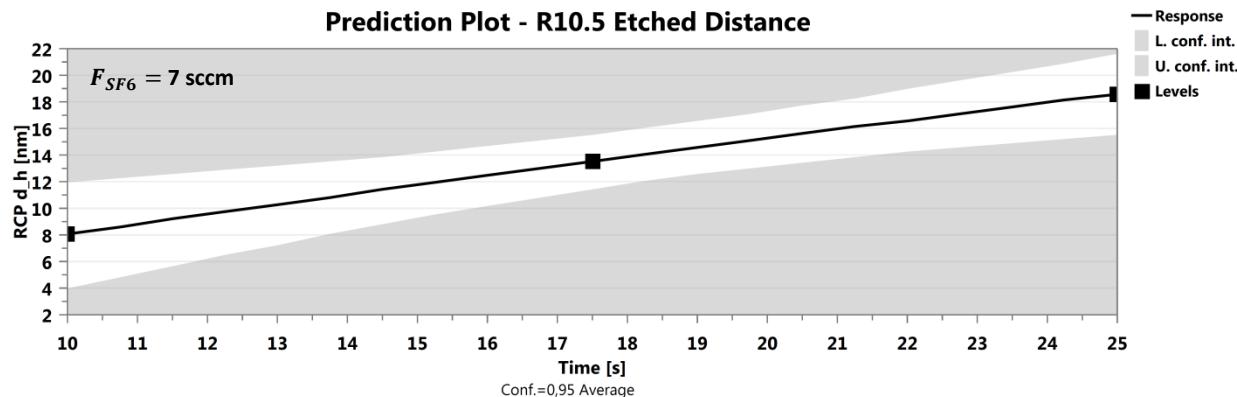
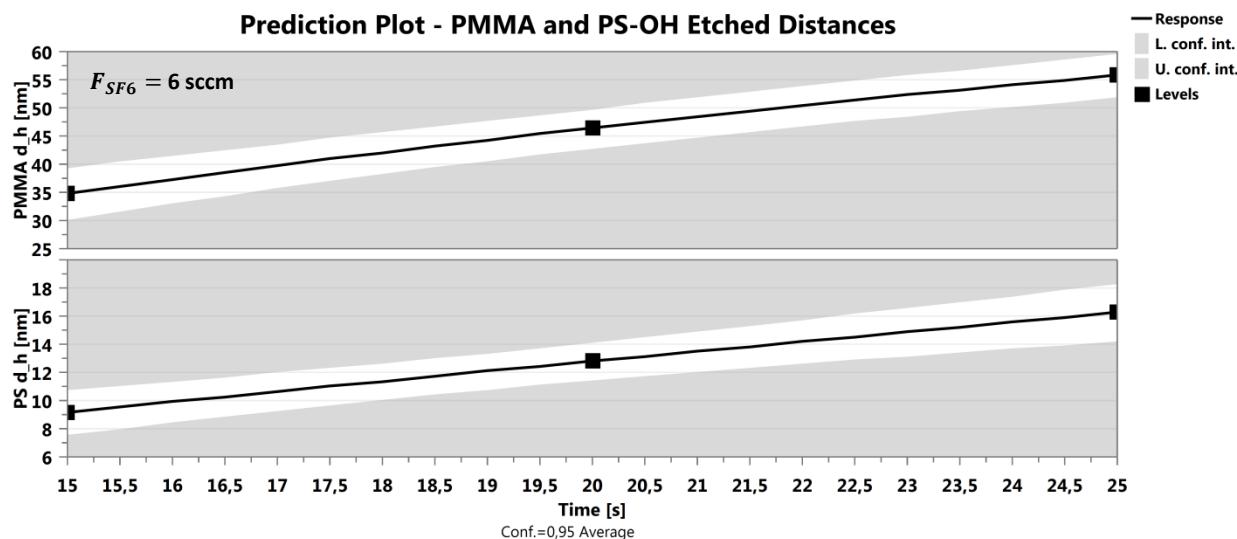
### A3.20 SF<sub>6</sub> / O<sub>2</sub> RIE MODDE DOE – Plotted Scaled and Centered Coefficients



### A3.21 SF<sub>6</sub> /O<sub>2</sub> RIE MODDE DOE – Observed vs. Predicted



### A3.22 SF<sub>6</sub> /O<sub>2</sub> RIE MODDE DOE –Predictions of etched distances



### A3.23 Effects of DUV and AA on grafted R10.5 blanket samples from Exp. I

Sample #	Treatment		R10.5 Ellipsometer Measurement				Diff. $\Delta h_{R10.5}$ /[nm]
	Step 1 $D_{DUV}$ /[J/cm <sup>2</sup> ]	Step 2 AA Bath /[min]	Before		After		
	MSE <sub>1</sub>	$h_{R10.5; 1}$ /[nm]	MSE <sub>2</sub>	$h_{R10.5; 2}$ /[nm]			
C9	<b>2,28</b>	8	3,37	7,2	3,742	3,178	4,022
C10	<b>2,28</b>	8	3,428	7	3,739	3,283	3,717
C11	<b>2,28</b>	8	3,365	6,1	3,476	3,013	3,087
C12	<b>2,28</b>	8	4,113	6,3	3,632	2,923	3,377
C1	<b>0</b>	8	3,986	5,2	2,777	3,291	1,909
C3	<b>0</b>	8	3,761	5,5	3,057	3,259	2,241
C4	<b>0</b>	8	3,805	5,7	3,321	3,58	2,120

**APPENDIX A4**  
**Deposition of SiN<sub>x</sub>/SiO<sub>2</sub>**  
**and Pattern Transfer**

#### A4.1 SiN<sub>x</sub> PECVD on samples WN1-5

"Deposition parameters:

200°C, gas flow 50 sccm Ar, 6 sccm SiH<sub>4</sub>, 8 sccm NH<sub>3</sub> (samples 1, 4, 5) or 9 sccm NH<sub>3</sub> (samples 2, 3), process pressure 0.015mbar, RF bias voltage is set to 300V (RF load power 70-85W), ICP load power is set to 1000W, process time 20 sec.

Process is based on quick start of the generators and getting flow of SiH<sub>4</sub> after plasma ignition." /Mariusz Graczyk

#### A4.2 Ellipsometer measurements of PECVD SiN<sub>x</sub> on WN1-5

**Model:** SiN<sub>x</sub>/Si(100) (Si3N4.mat/Si.jell)

Sample #	MSE	h <sub>SiN<sub>x</sub></sub> / [nm]	n <sub>633 nm</sub>	Fitted
WN1	17.39	11.672	NA	h
WN1	7.117	12.939	2.5076	h, n
WN2	5.023	11.257	NA	h
WN2	3.649	11.376	1.8502	h, n
WN3	5.324	11.401	NA	h
WN3	3.693	11.525	1.8458	h, n
WN4	4.282	10.544	NA	h
WN4	3.458	10.642	2.0664	h, n
WN5	4.281	10.514	NA	h
WN5	3.369	10.609	1.8664	h, n

#### A4.3 Ellipsometer measurements of PECVD SiN<sub>x</sub> before and after surface treatments

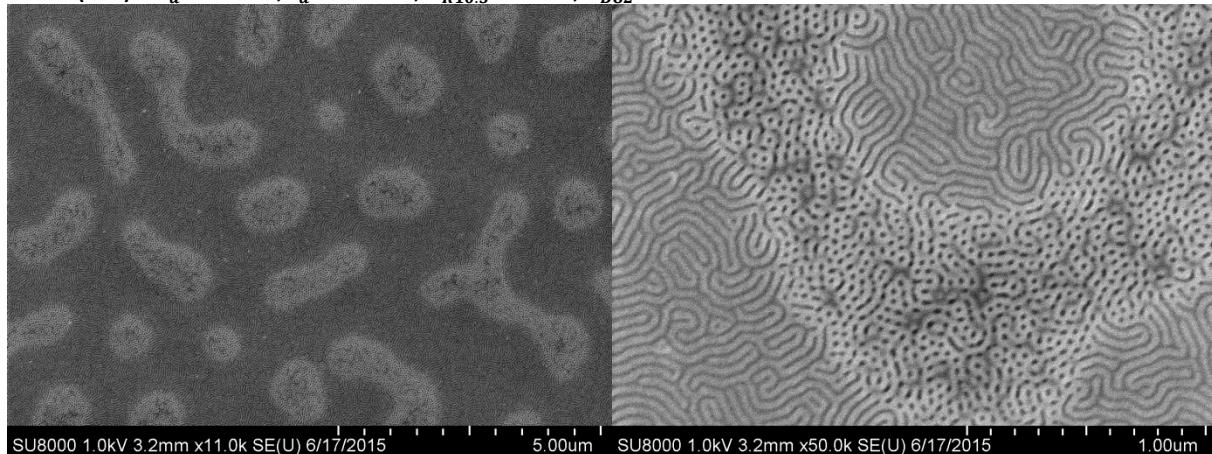
**λ / [nm]:** [370.44, 1239]

**Model:** SiN<sub>x</sub>/Native oxide (15 Å)/Si(100) (Si3N4.mat/ntve.jaw/Si.jaw)

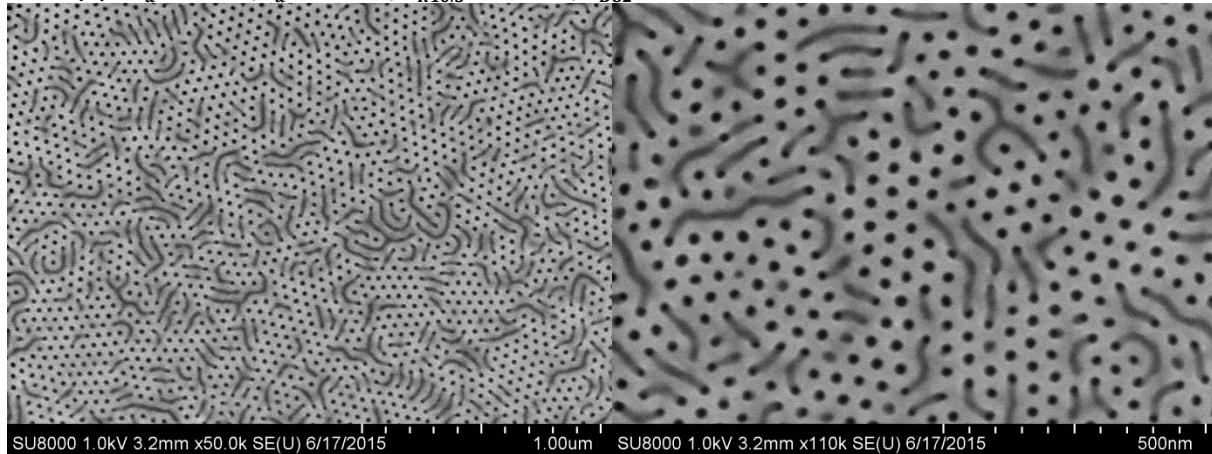
Sample #	$\alpha_i / [^\circ]$	Before Surface Activation			After Surface Activation			Fitted	Surface Activation
		Ellipsometer measurement 1			Ellipsometer measurement 2				
WN1D	65-75	24.49	103.86	2.0211	h	15.5	109.13	2.0211	h
WN1D	65-75	9.159	116.10	2.5399	h, n	6.917	115.30	2.388	h, n
WN2	50-75	4.804	100.58	2.0211	h	5.655	101.27	2.0211	h
WN2	50-75	3.637	101.72	1.8448	h, n	3.615	103.22	1.7953	h, n
WN3	50-75	4.021	102.09	2.0211	h	4.877	100.77	2.0211	h
WN3	50-75	2.963	103.27	2.0211	h, n	3.306	102.09	1.8467	h, n
WN4A	50-75	3.78	94.06	2.0211	h	5.891	97.42	2.0211	h
WN4A	50-75	3.036	95.26	2.1378	h, n	3.487	99.41	1.7975	h, n

**A4.4 R10.5 grafting and wetting behavior on PECVD SiN<sub>x</sub>**

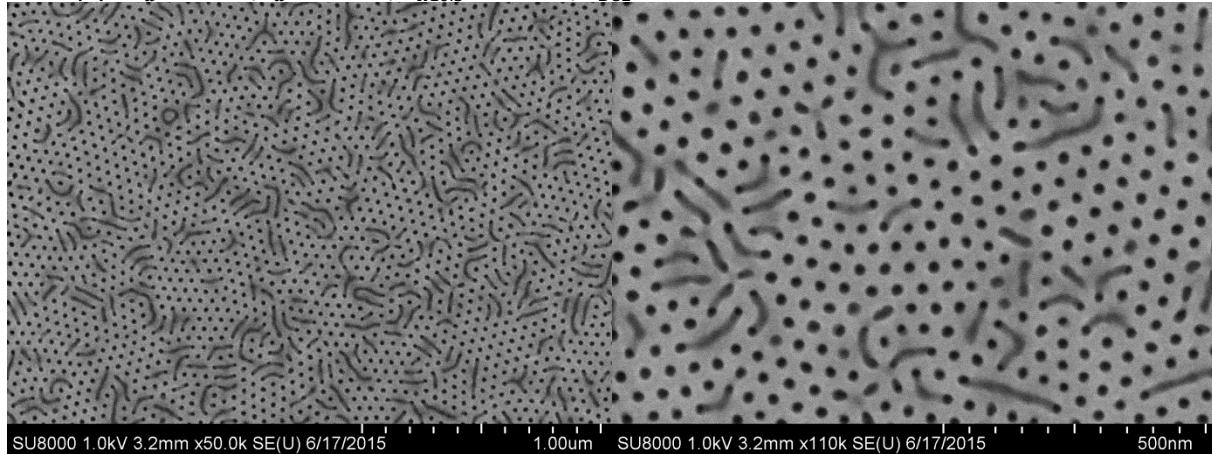
WN1A (N-U) –  $T_a = 250^\circ\text{C}$ ;  $t_a = 30 \text{ min}$ ;  $h_{R10.5} = 0 \text{ nm}$ ;  $h_{B82} = 44.6 \text{ nm}$  – No Surface Activation



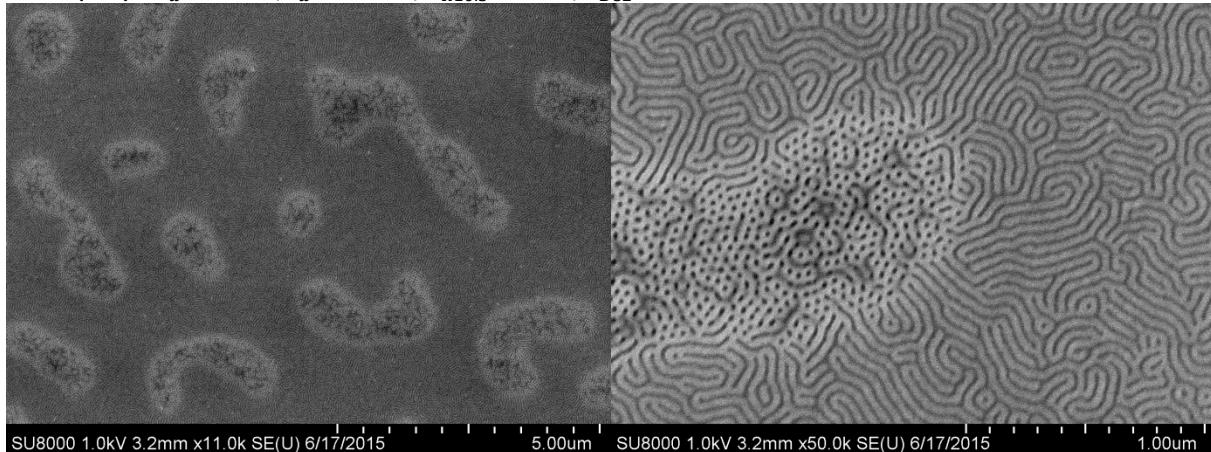
WN1B (U) –  $T_a = 250^\circ\text{C}$ ;  $t_a = 30 \text{ min}$ ;  $h_{R10.5} = 7.6 \text{ nm}$ ;  $h_{B82} = 41.9 \text{ nm}$  – No Surface Activation



WN1C (U) –  $T_a = 250^\circ\text{C}$ ;  $t_a = 30 \text{ min}$ ;  $h_{R10.5} = 5.9 \text{ nm}$ ;  $h_{B82} = 39.4 \text{ nm}$  – RIE Surface Activation

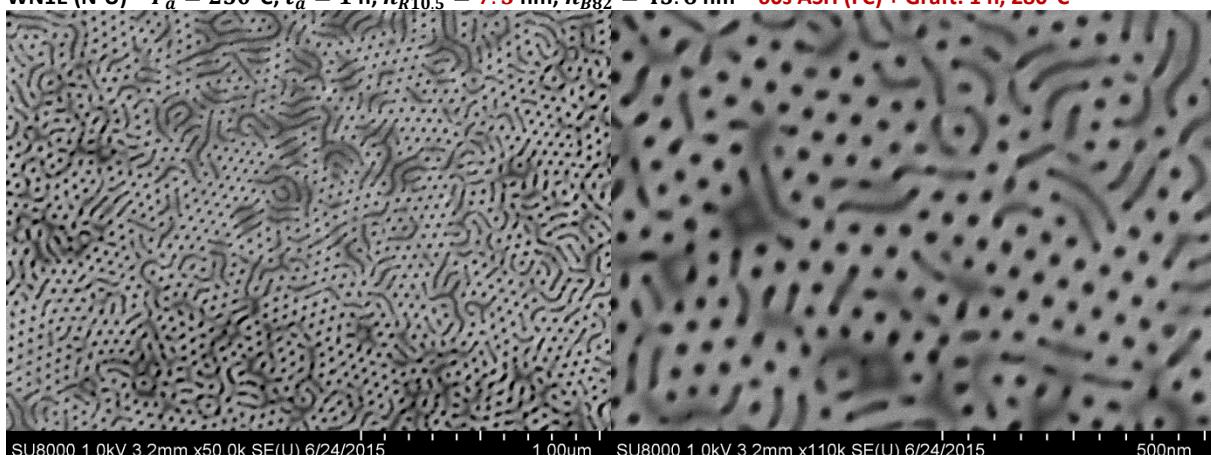


WN1D (N-U) –  $T_a = 250^\circ\text{C}$ ;  $t_a = 30 \text{ min}$ ;  $h_{R10.5} = 0 \text{ nm}$ ;  $h_{B82} = 44.4 \text{ nm}$  – No Surface Activation

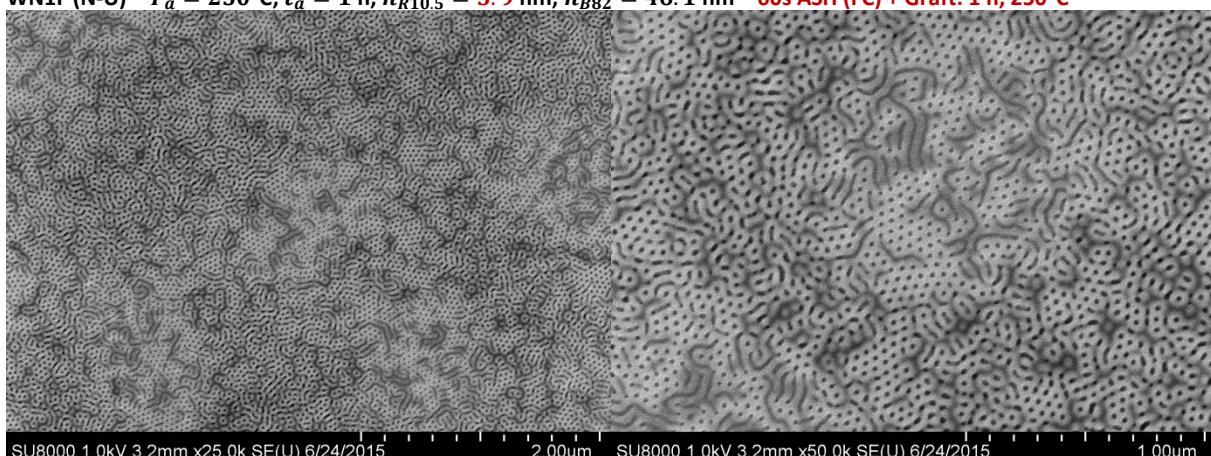


#### A4.5 Extended grafts on PECVD SiN<sub>x</sub>

WN1E (N-U) –  $T_a = 250^\circ\text{C}$ ;  $t_a = 1 \text{ h}$ ;  $h_{R10.5} = 7.3 \text{ nm}$ ;  $h_{B82} = 43.6 \text{ nm}$  – 60s ASH (FC) + Graft: 1 h, 280°C

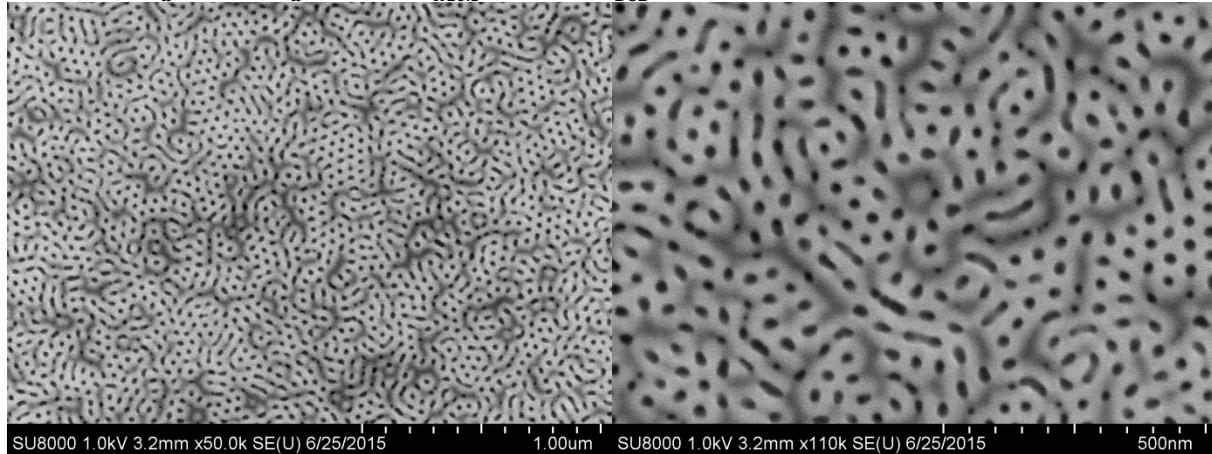


WN1F (N-U) –  $T_a = 250^\circ\text{C}$ ;  $t_a = 1 \text{ h}$ ;  $h_{R10.5} = 5.9 \text{ nm}$ ;  $h_{B82} = 46.1 \text{ nm}$  – 60s ASH (FC) + Graft: 1 h, 250°C

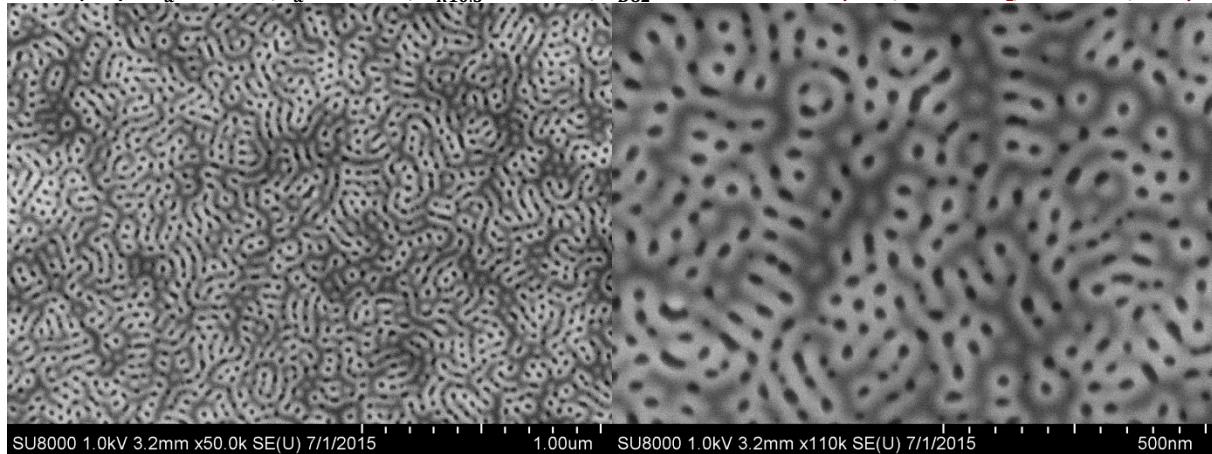


**A4.6 Efficacy of various surface activation treatments on PECVD SiN<sub>x</sub>**

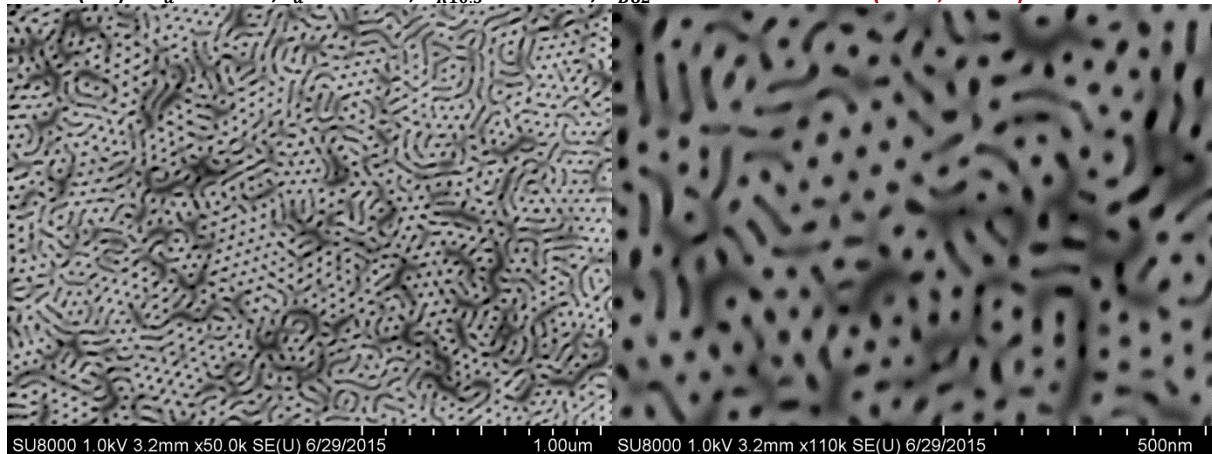
WN2E ( $\approx$ U) –  $T_a = 250^\circ\text{C}$ ;  $t_a = 30$  min;  $h_{R10.5} = 6.1$  nm;  $h_{B82} = 45.7$  nm – RIE: (30W, 20 sccm O<sub>2</sub>, 150 mTorr, 80s)



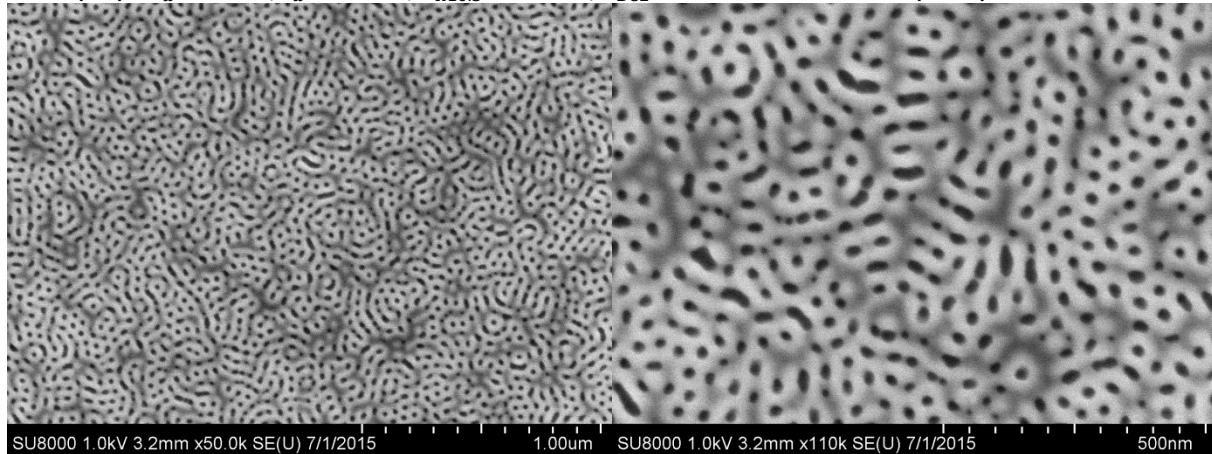
WN4A ( $\approx$ U) –  $T_a = 250^\circ\text{C}$ ;  $t_a = 60$  min;  $h_{R10.5} = 2.3$  nm;  $h_{B82} = 51.2$  nm – RIE: (50W, 40 sccm O<sub>2</sub>, 150 mTorr, 120s)



WN3A ( $\approx$ U) –  $T_a = 250^\circ\text{C}$ ;  $t_a = 30$  min;  $h_{R10.5} = 5.2$  nm;  $h_{B82} = 45.0$  nm – Ozone: (150°C, 10 min)



WN4B ( $\approx$ U) –  $T_a = 250^\circ\text{C}$ ;  $t_a = 60$  min;  $h_{R10.5} = \textcolor{red}{5.8}$  nm;  $h_{B82} = 54.1$  nm – PP Ash: 60s (No FC)



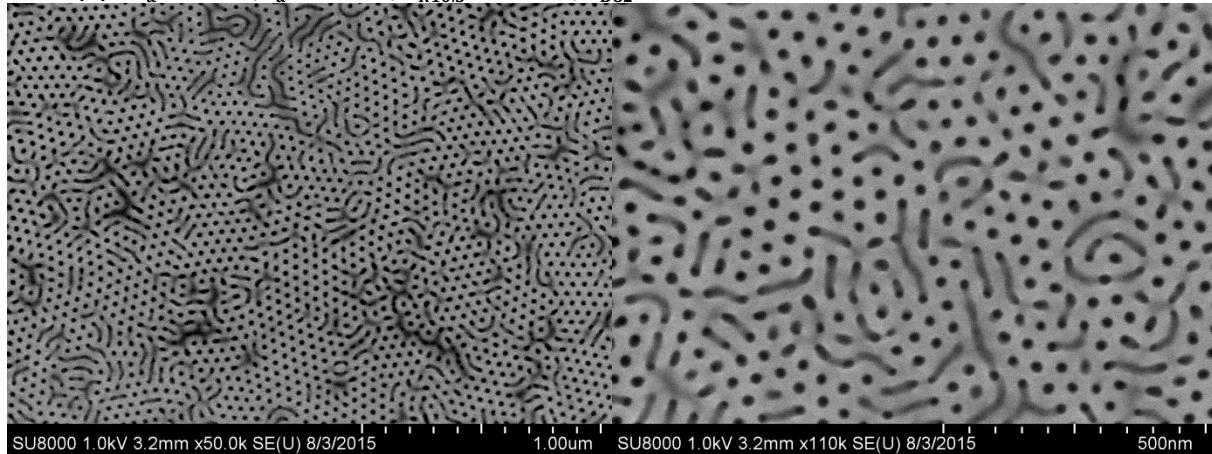
#### A4.7 SiO<sub>2</sub> and SiN<sub>x</sub> ellipsometer data for WN5 and WHD1

$\lambda$  / [nm]: [370.44, 1239]

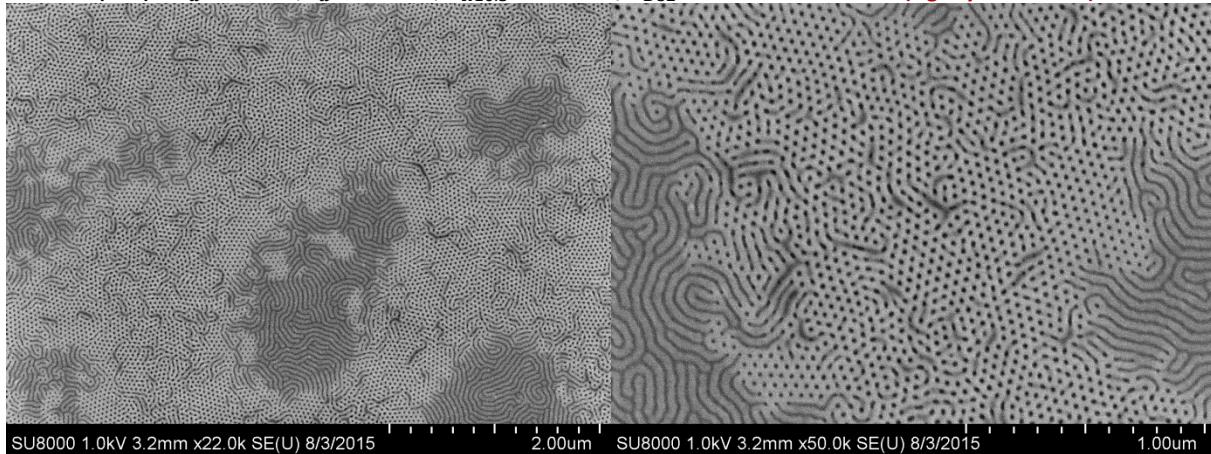
Sample #	MSE	$h_{\text{SiO}_2}$ / [Å]	$h_{\text{SiN}_x}$ / [Å]	$n_{\text{SiN}_x;633}$	$h_{\text{SiO}_x}$ / [Å]	Fitted	$\alpha_i$ / [°]	Comments
WHD1	9.385	0	138.48	2.0211	0	$h_{\text{SiN}_x}$	[65,75]	After PECVD
WHD1	5.145	0	145.67	1.6803	0	$h_{\text{SiN}_x}, n_{\text{SiN}_x}$	[65,75]	After PECVD
WHD1	5.933	14.31	145.67	1.6803	0	$h_{\text{SiO}_2}$	[50,75]	After ALD
WN5	3.411	18.50	91.59	2.0683	15	$h_{\text{SiO}_2}$	[50,75]	After ALD
WHD1	5.669	14.17	145.67	1.6803	0	$h_{\text{SiO}_2}$	[50,75]	Before 2 <sup>nd</sup> Piranha
WN5	3.204	18.45	91.59	2.0683	15	$h_{\text{SiO}_2}$	[50,75]	Before 2 <sup>nd</sup> Piranha

#### A4.8 B82 polymer pattern on R10.5 grafted to a SiO<sub>2</sub>/SiN<sub>x</sub> stack

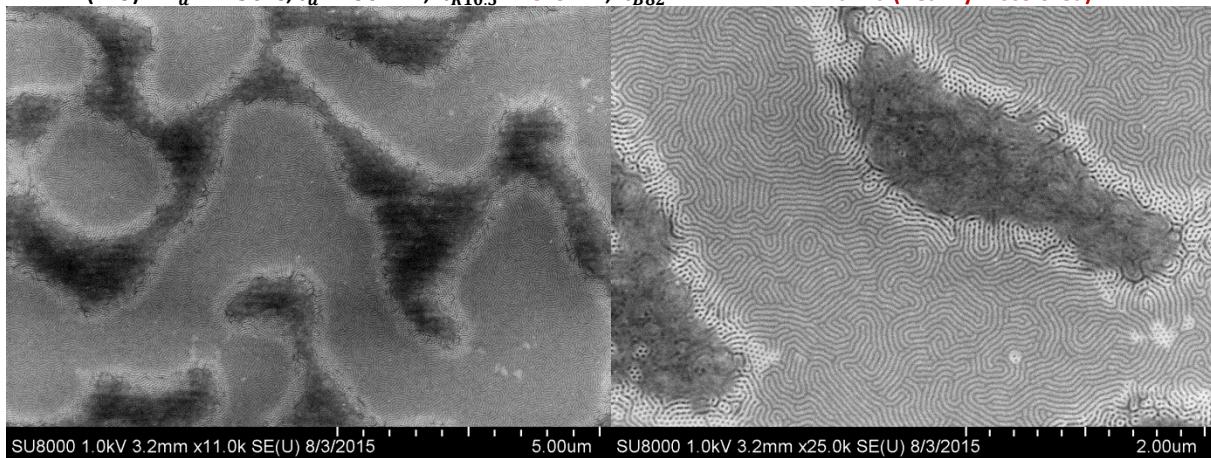
WN5A (U) –  $T_a = 250^\circ\text{C}$ ;  $t_a = 60$  min;  $h_{R10.5} = \textcolor{red}{8.1}$  nm;  $h_{B82} = 45.9$  nm – Piranha



WHD1M (N-U) –  $T_a = 250^\circ\text{C}$ ;  $t_a = 60 \text{ min}$ ;  $h_{R10.5} = 6.8 \text{ nm}$ ;  $h_{B82} = 44.7 \text{ nm}$  – Piranha (Lightly Discolored)

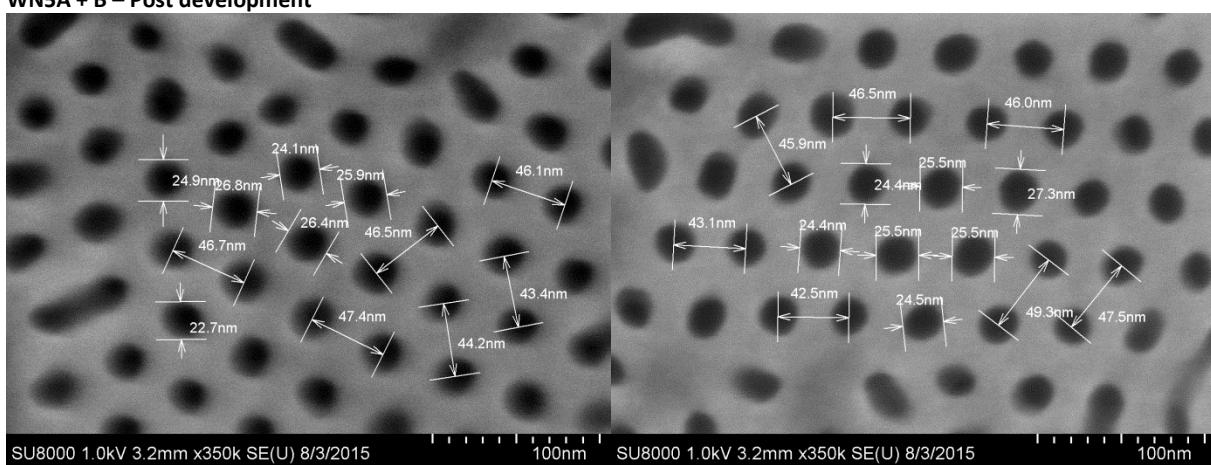


WHD1L (N-U) –  $T_a = 250^\circ\text{C}$ ;  $t_a = 60 \text{ min}$ ;  $h_{R10.5} = 6.8 \text{ nm}$ ;  $h_{B82} = 44.7 \text{ nm}$  – Piranha (Heavily Discolored)



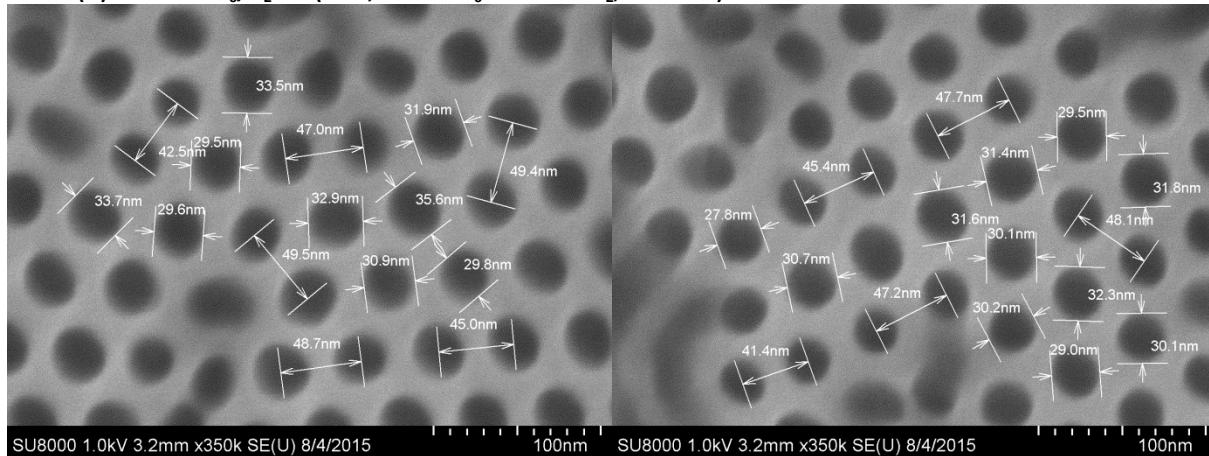
#### A4.9 Pattern Transfer Calibration – After Step 0: Post-Development

WN5A + B – Post development

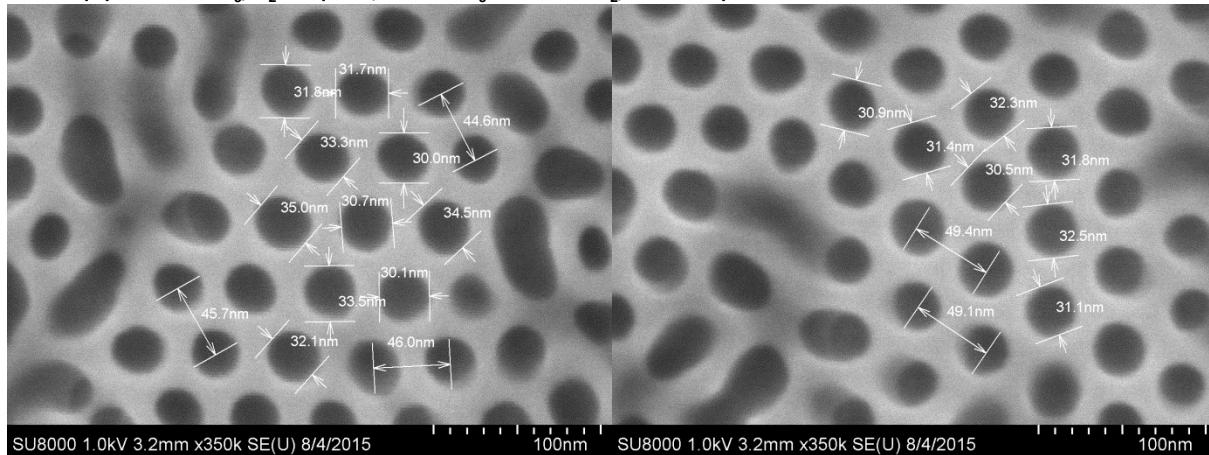


#### A4.10 Pattern Transfer Calibration – After Step 1: SF<sub>6</sub>/O<sub>2</sub> RIE

WN5A (U) – Post 6s SF<sub>6</sub>/O<sub>2</sub> RIE (30W, 7 sccm SF<sub>6</sub> + 13 sccm O<sub>2</sub>, 75 mTorr)

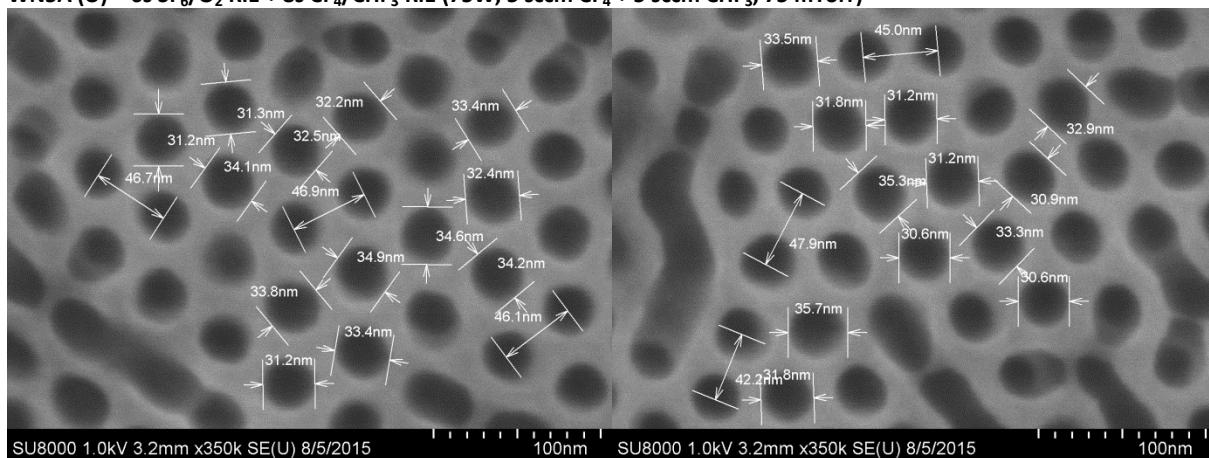


WN5B (U) – Post 9s SF<sub>6</sub>/O<sub>2</sub> RIE (30W, 7 sccm SF<sub>6</sub> + 13 sccm O<sub>2</sub>, 75 mTorr)

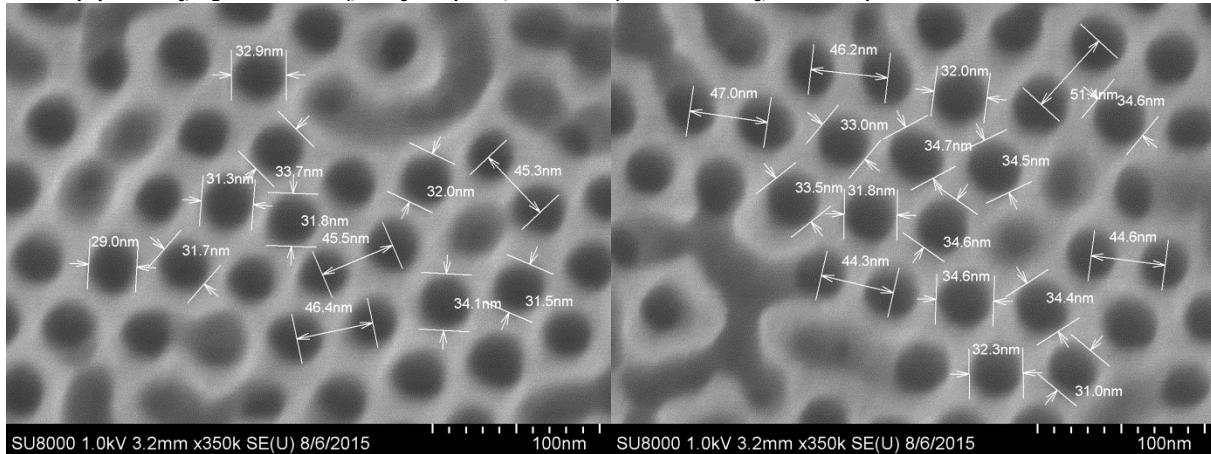


#### A4.11 Pattern Transfer Calibration – After Step 2: CF<sub>4</sub>/CHF<sub>3</sub> RIE

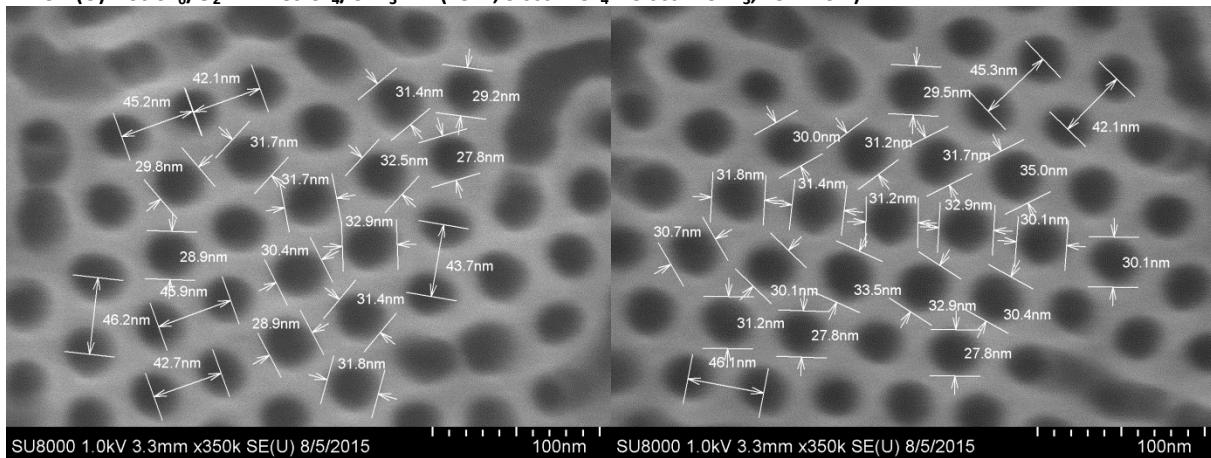
WN5A (U) – 6s SF<sub>6</sub>/O<sub>2</sub> RIE + 8s CF<sub>4</sub>/CHF<sub>3</sub> RIE (75W, 5 sccm CF<sub>4</sub> + 5 sccm CHF<sub>3</sub>, 75 mTorr)



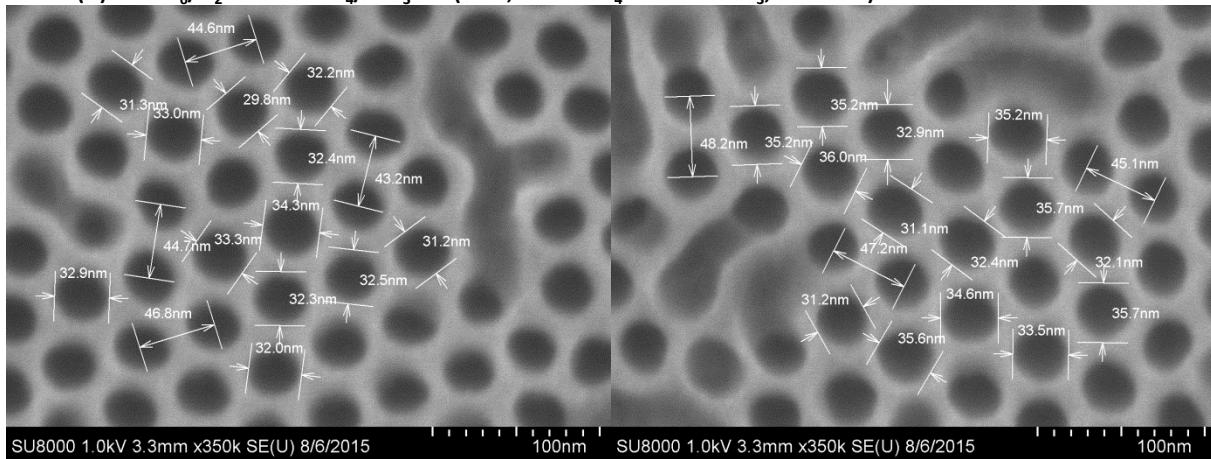
**WN5C (U) – 6s SF<sub>6</sub>/O<sub>2</sub> RIE + 11s CF<sub>4</sub>/CHF<sub>3</sub> RIE (75W, 5 sccm CF<sub>4</sub> + 5 sccm CHF<sub>3</sub>, 75 mTorr)**



**WN5B (U) – 9s SF<sub>6</sub>/O<sub>2</sub> RIE + 8s CF<sub>4</sub>/CHF<sub>3</sub> RIE (75W, 5 sccm CF<sub>4</sub> + 5 sccm CHF<sub>3</sub>, 75 mTorr)**

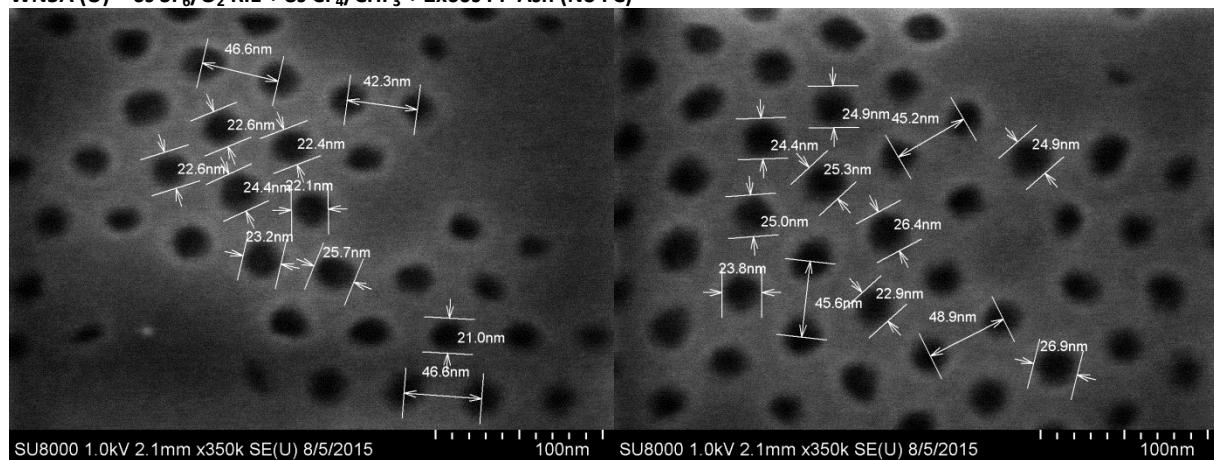


**WN5D (U) – 9s SF<sub>6</sub>/O<sub>2</sub> RIE + 11s CF<sub>4</sub>/CHF<sub>3</sub> RIE (75W, 5 sccm CF<sub>4</sub> + 5 sccm CHF<sub>3</sub>, 75 mTorr)**

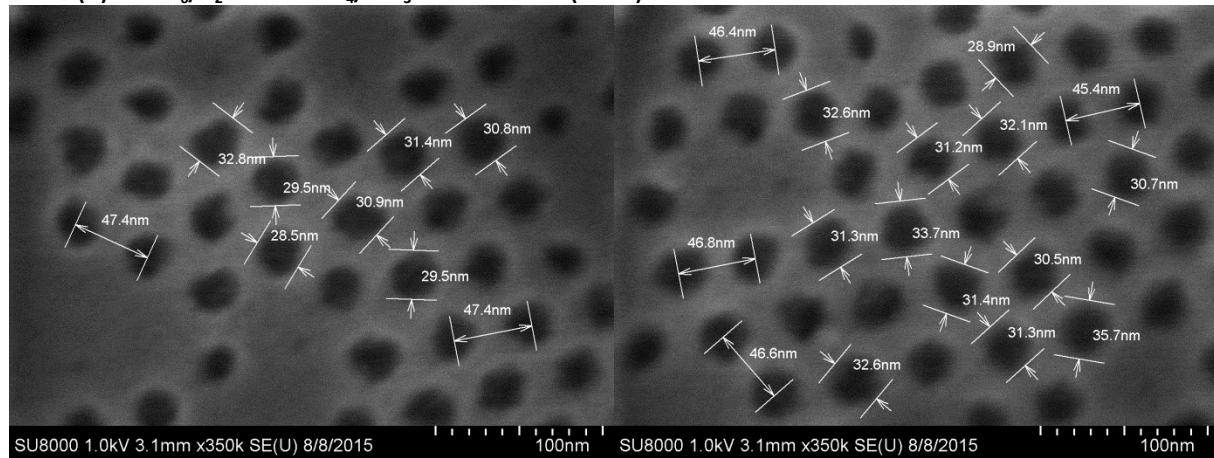


#### A4.12 Pattern Transfer Calibration – After Step 3: PS Removal

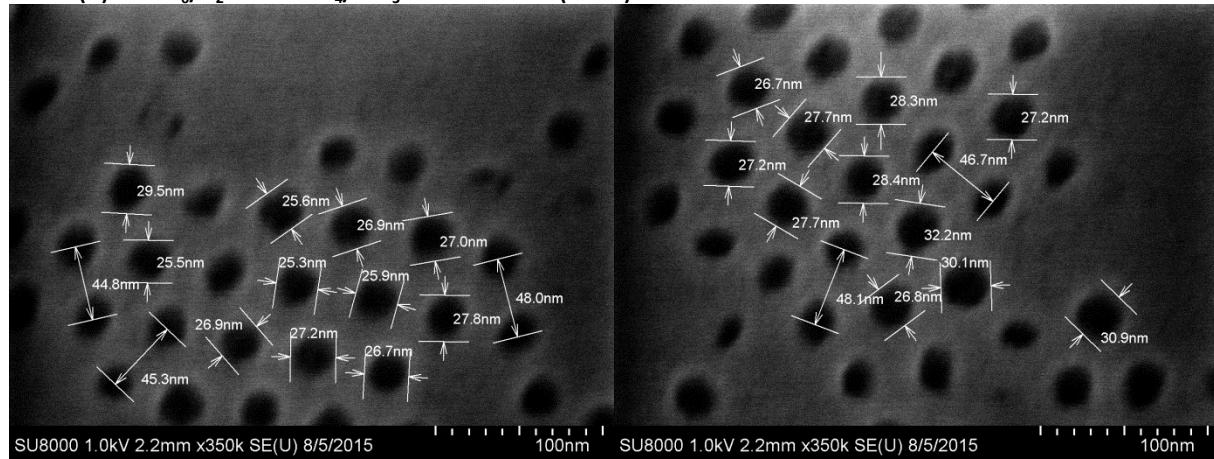
WN5A (U) – 6s SF<sub>6</sub>/O<sub>2</sub> RIE + 8s CF<sub>4</sub>/CHF<sub>3</sub> + 2x60s PP Ash (No FC)



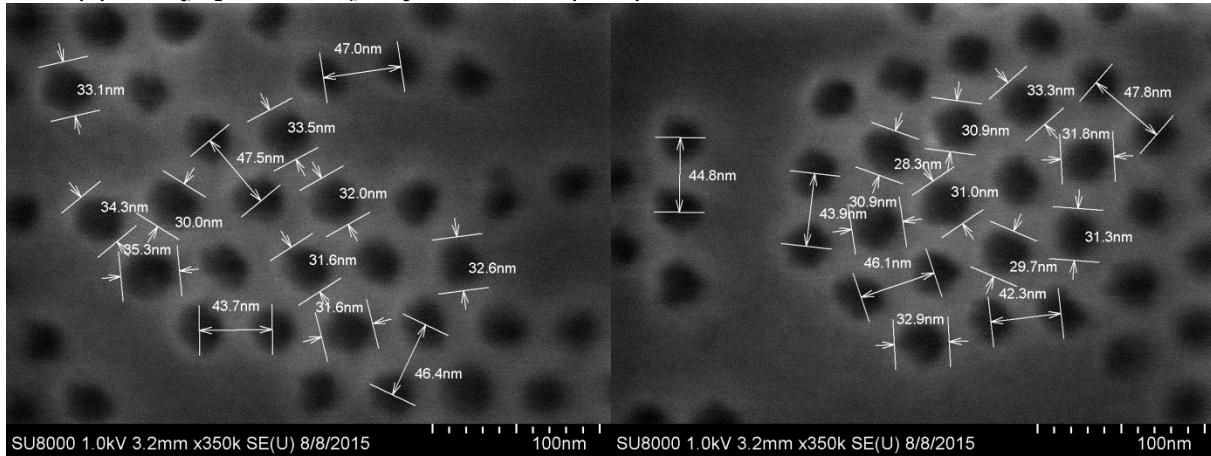
WN5C (U) – 6s SF<sub>6</sub>/O<sub>2</sub> RIE + 11s CF<sub>4</sub>/CHF<sub>3</sub> + 2x60s PP Ash (No FC)



WN5B (U) – 9s SF<sub>6</sub>/O<sub>2</sub> RIE + 8s CF<sub>4</sub>/CHF<sub>3</sub> + 2x60s PP Ash (No FC)

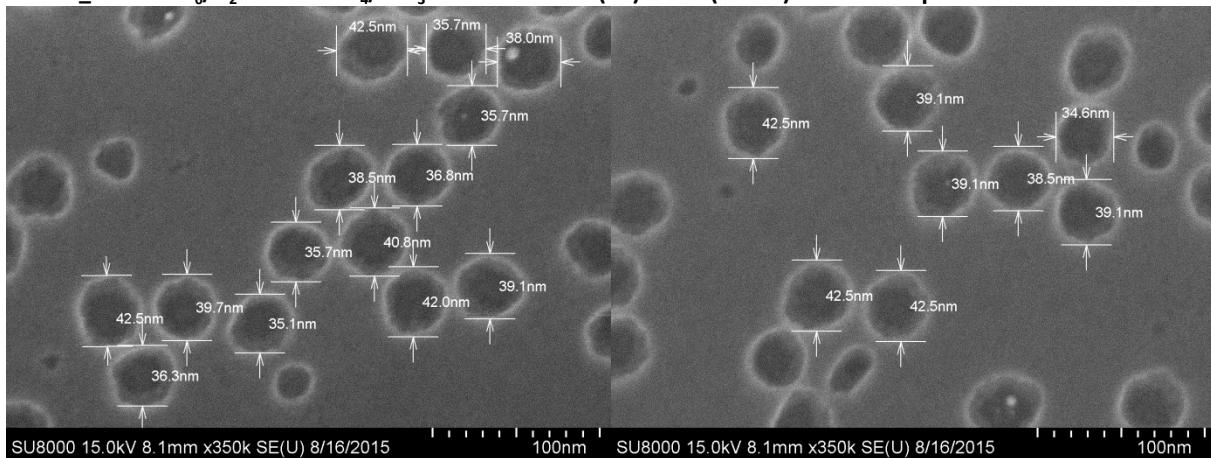


**WN5D (U) – 9s SF<sub>6</sub>/O<sub>2</sub> RIE + 11s CF<sub>4</sub>/CHF<sub>3</sub> + 2x60s PP Ash (No FC)**

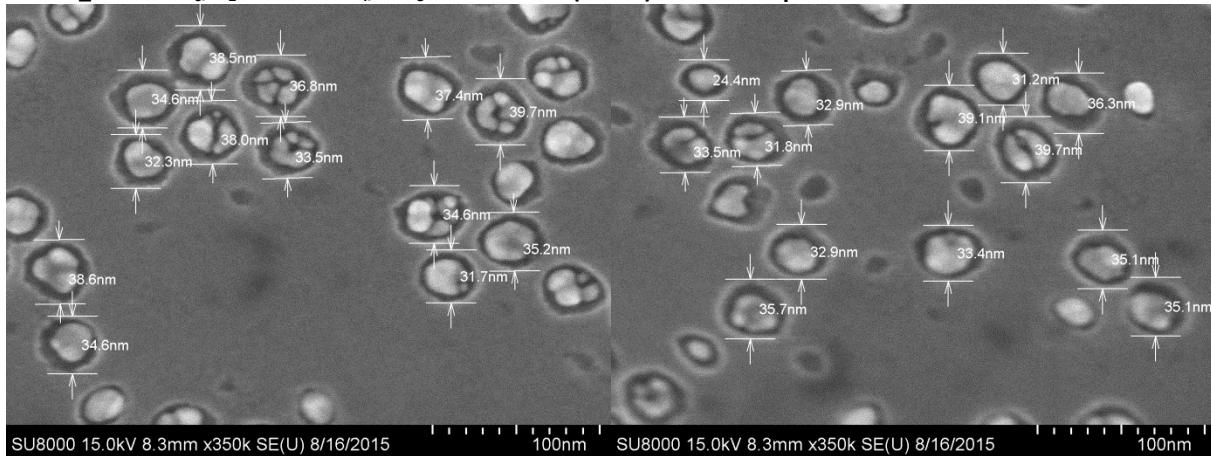


**A4.13 Higher quality SEM images and measurements taken post-electrodeposition**

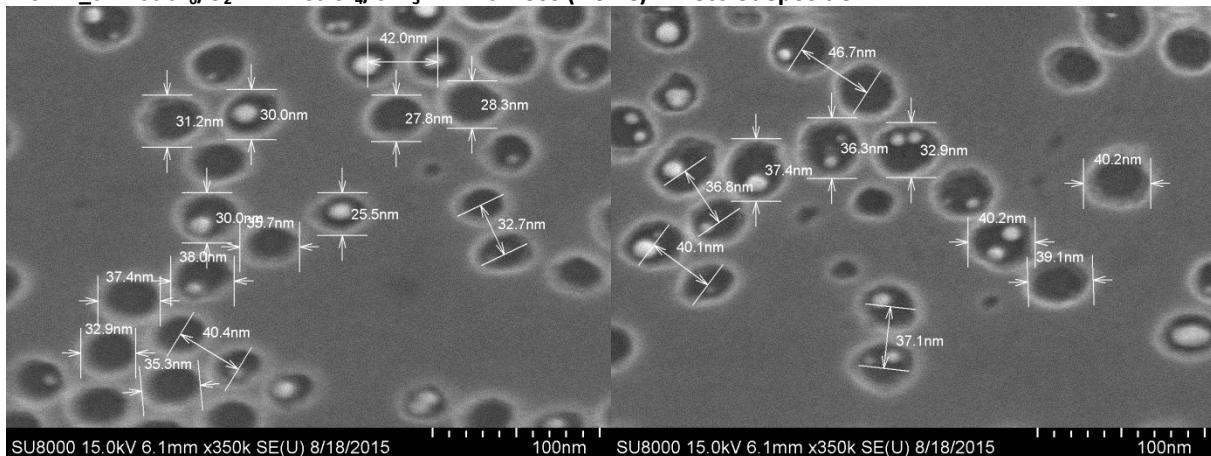
**BL9777\_01E - 9s SF<sub>6</sub>/O<sub>2</sub> RIE + 13s CF<sub>4</sub>/CHF<sub>3</sub> + PP Ash: 2x60s (FC) + 60s (No FC) + Electrodeposition**



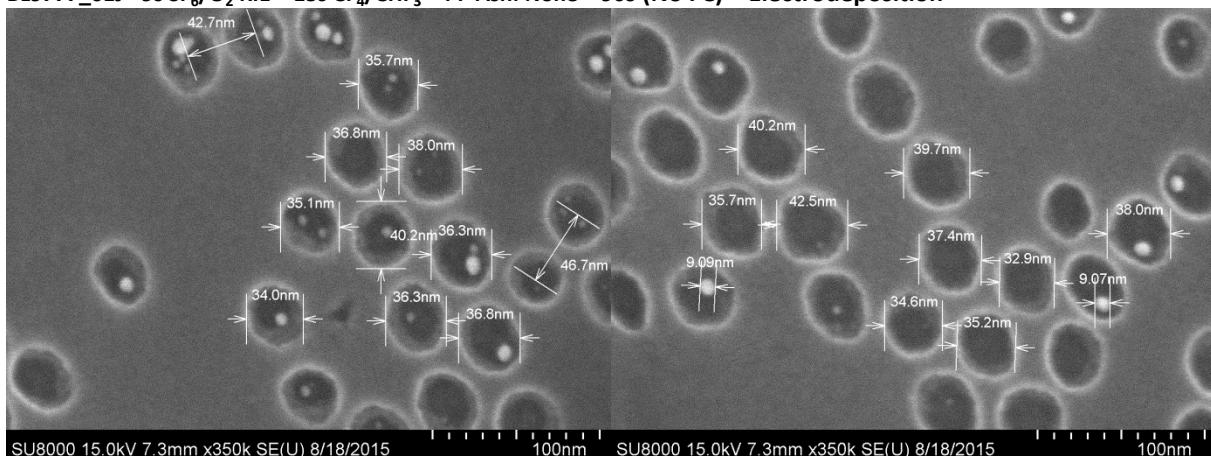
**BL9777\_01F - 9s SF<sub>6</sub>/O<sub>2</sub> RIE + 15s CF<sub>4</sub>/CHF<sub>3</sub> + PP Ash: 20s (No FC) + Electrodeposition**



**BL9777\_01I - 9s SF<sub>6</sub>/O<sub>2</sub> RIE + 15s CF<sub>4</sub>/CHF<sub>3</sub> + PP Ash: 60s (No FC) + Electrodeposition**



**BL9777\_01J - 9s SF<sub>6</sub>/O<sub>2</sub> RIE + 15s CF<sub>4</sub>/CHF<sub>3</sub> + PP Ash: None + 90s (No FC) + Electrodeposition**



#### A4.14 SiO<sub>2</sub>, SiN<sub>x</sub> and InAs ellipsometer data of BL9777\_01, \_02, \_04

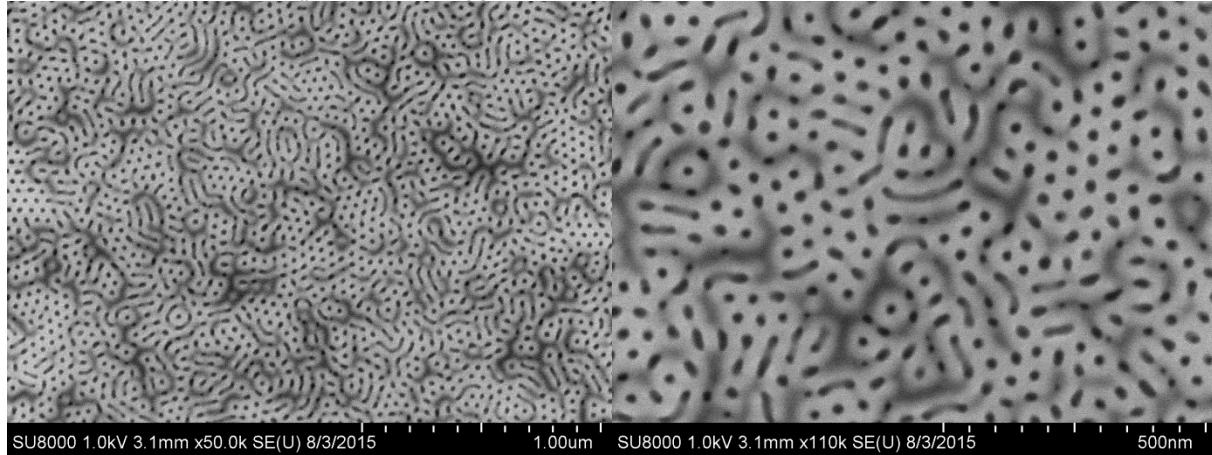
$\lambda$  / [nm]: [370.44, 1694.6]

$\alpha_i$  / [ $^{\circ}$ ]: 50-75

Sample #	MSE	$h_{\text{SiO}_2}$ / [ $\text{\AA}$ ]	$h_{\text{SiN}_x}$ / [ $\text{\AA}$ ]	$n_{\text{SiN}_x, 633}$	$h_{\text{InAs-OX}}$ / [ $\text{\AA}$ ]	$h_{\text{InAs}}$ / [nm]	$n_{\text{InAs}, 633}$	Fitted	Comments
BL9777_01	20.58	-	-	-	22.42	263.929	NA	$h_{\text{InAs-OX}}, h_{\text{InAs}}$	InAs/Si(111)
BL9777_02	17.77	-	-	-	17.11	275.304	NA	$h_{\text{InAs-OX}}, h_{\text{InAs}}$	InAs/Si(111)
BL9777_04	22.81	-	-	-	22.58	287.958	3.938	$h_{\text{InAs-OX}}, h_{\text{InAs}}$	InAs/Si(111)
BL9777_04	14.65	-	-	-	23.64	282.836	3.9141	$h_{\text{InAs-OX}}, h_{\text{InAs}}$ $n_{\text{InAs}}$	InAs/Si(111)
BL9777_01	20.47	-	85.12	2.0211	22.41	263.941	NA	$h_{\text{SiN}_x}$	After SiN <sub>x</sub> PECVD
BL9777_01	10.05	-	102.74	1.5644	22.41	263.941	NA	$h_{\text{SiN}_x}, n_{\text{SiN}_x}$	After SiN <sub>x</sub> PECVD
BL9777_02	29.97	-	86.81	2.0211	17.11	275.290	NA	$h_{\text{SiN}_x}$	After SiN <sub>x</sub> PECVD
BL9777_02	13.83	-	106.84	1.5506	17.11	275.290	NA	$h_{\text{SiN}_x}, n_{\text{SiN}_x}$	After SiN <sub>x</sub> PECVD
BL9777_01	24.36	15.33	85.12	2.0211	22.41	263.941	NA	$h_{\text{SiO}_2}$	After SiO <sub>2</sub> ALD
BL9777_02	25.6	17.95	86.81	2.0211	17.11	275.290	NA	$h_{\text{SiO}_2}$	After SiO <sub>2</sub> ALD
BL9777_04	21.11	86.04	0	NA	22.58	287.958	NA	$h_{\text{SiO}_2}$	After SiO <sub>2</sub> ALD
BL9777_01	20.34	17.56	85.12	2.0211	22.41	263.941	NA	$h_{\text{SiO}_2}$	After failed Piranha

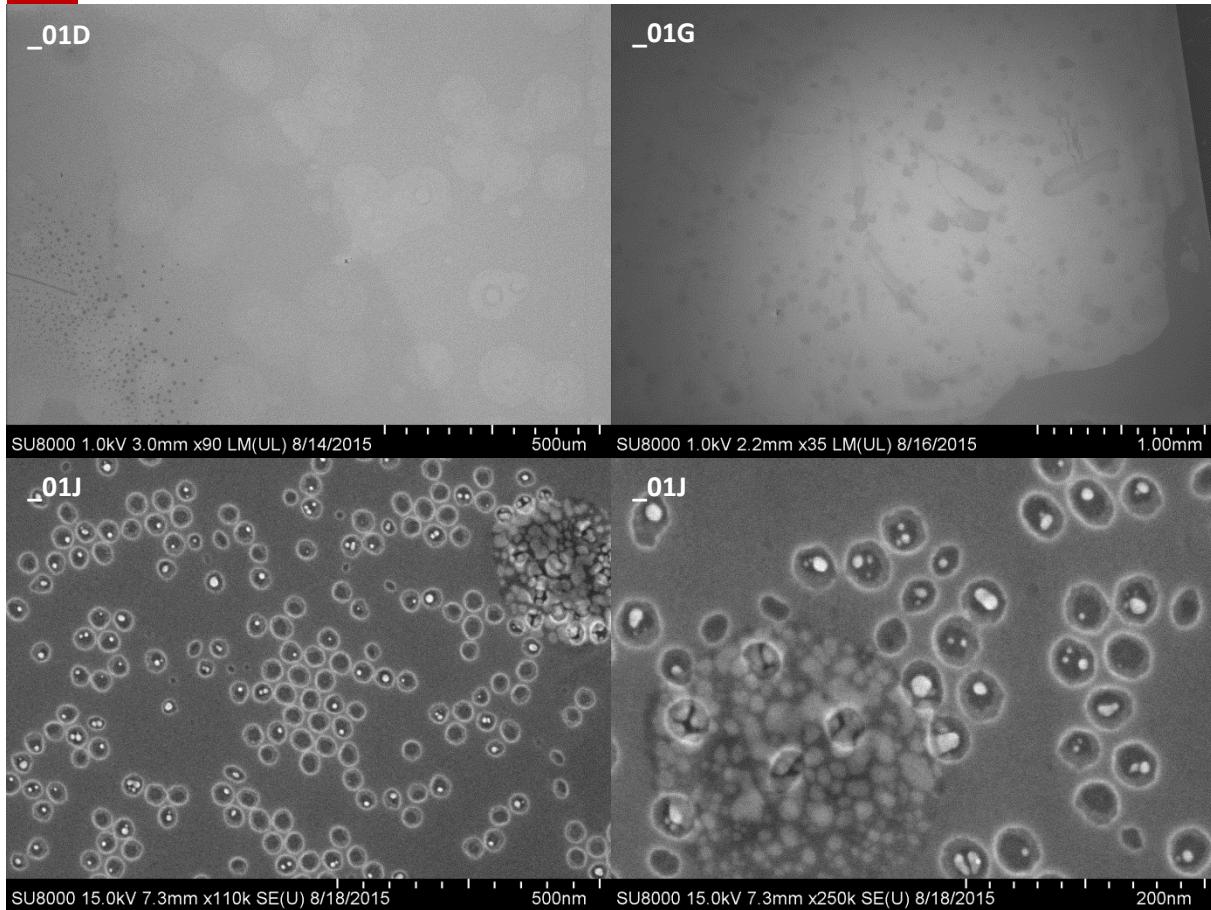
#### A4.15 Developed B82 pattern of BL9777\_01

BL9777\_01D –  $T_a = 250^{\circ}\text{C}$ ;  $t_a = 60$  min;  $h_{R10.5} = 6.8$  nm;  $h_{B82} = 44.6$  nm – PP Ash: 3x60s (FC)



**APPENDIX A5**  
**Electrodeposition**

**A5.1 Selected sample overviews illustrating defects after electrodeposition**



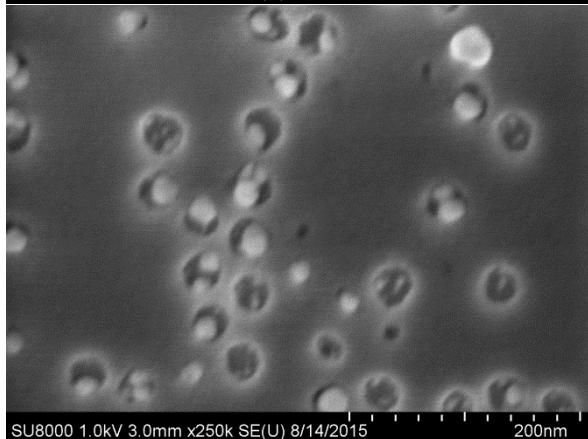
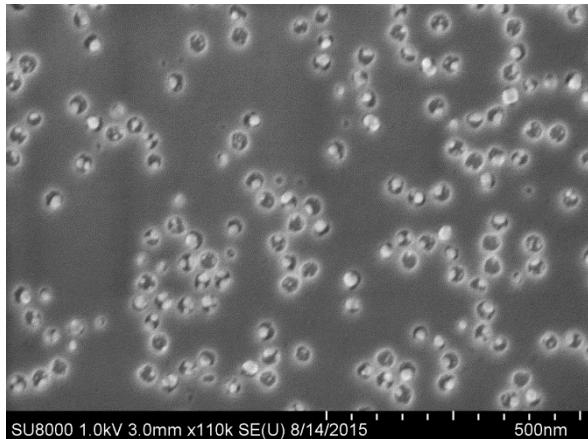
**A5.2 Etch, ash and electrodeposition data**

**#BL9777\_01D**

R10.5 RIE: **9 s**  
SiN<sub>x</sub> RIE: **11 s**  
ASH, Front (FC): **2 x 60 s (No)**  
ASH, Backside (FC): **None**

**Electrodeposition**

Current: **350 mA**  
Time: **10 s**

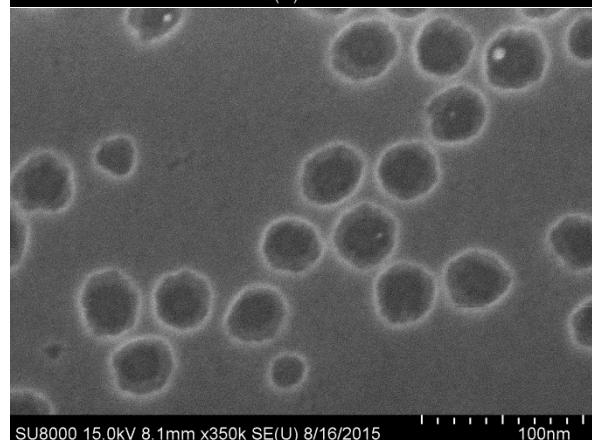
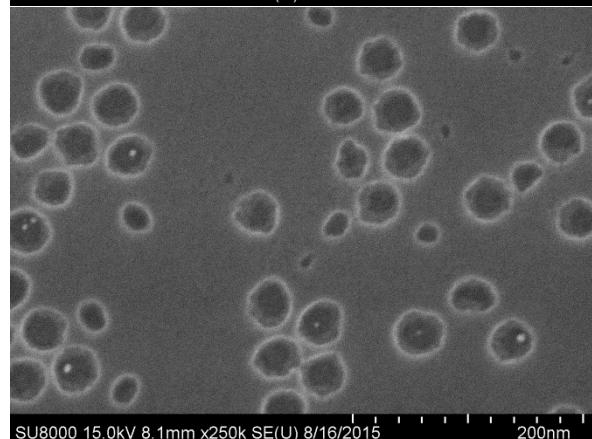
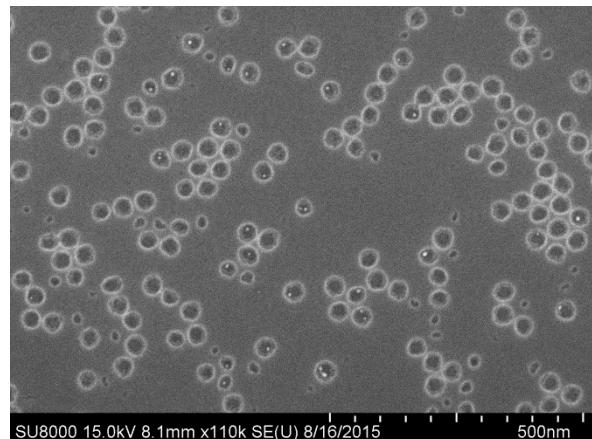


**#BL9777\_01E**

R10.5 RIE: **9 s**  
SiNx RIE: **13 s**  
ASH, Front (FC): **2x60 s (Yes) + 60 s (No)**  
ASH, Backside (FC): **15 s (No)**

**Electrodeposition**

Current: **350 mA**  
Time: **10 s**



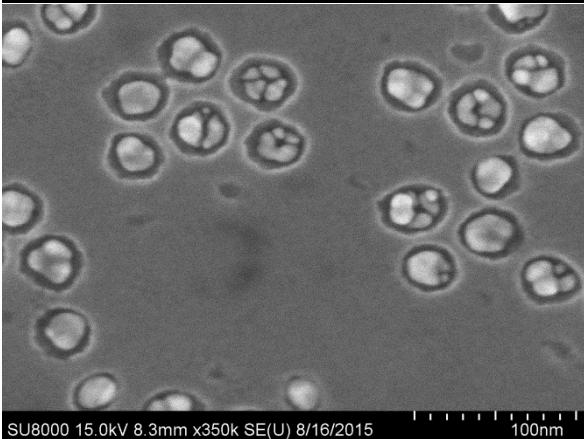
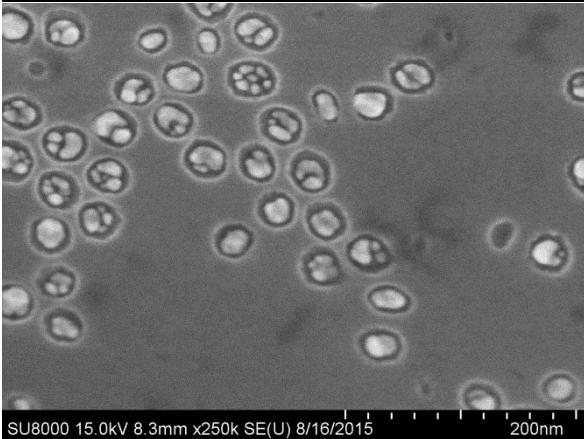
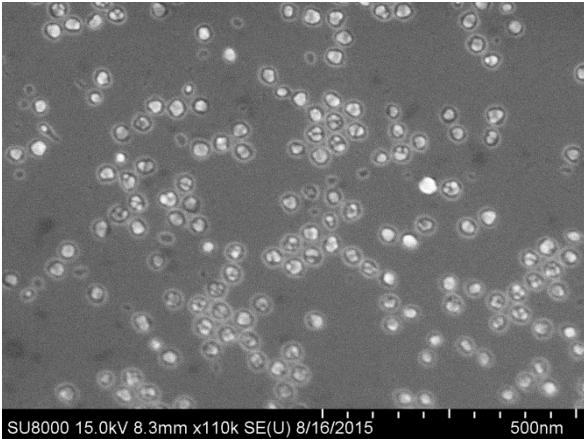
## #BL977\_01F

R10.5 RIE                   **9 s**  
SiNx RIE:                   **15 s**  
ASH, Front (FC):           **20 s (No)**  
ASH, Backside (FC):       **15 s (No)**

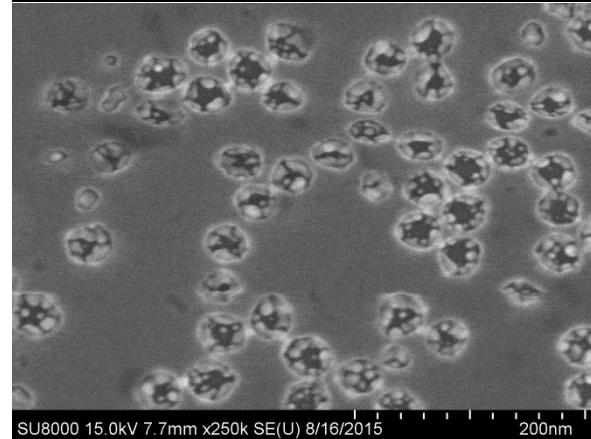
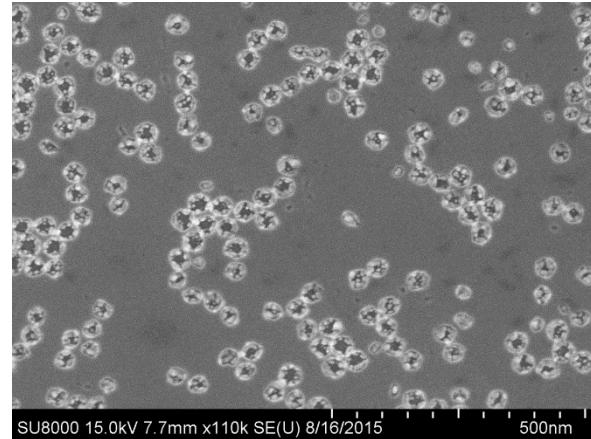
### Electrodeposition

Nom. Current:              **350 mA**  
Nom. Time:                  **10 s**

(Column I: Center of sample)



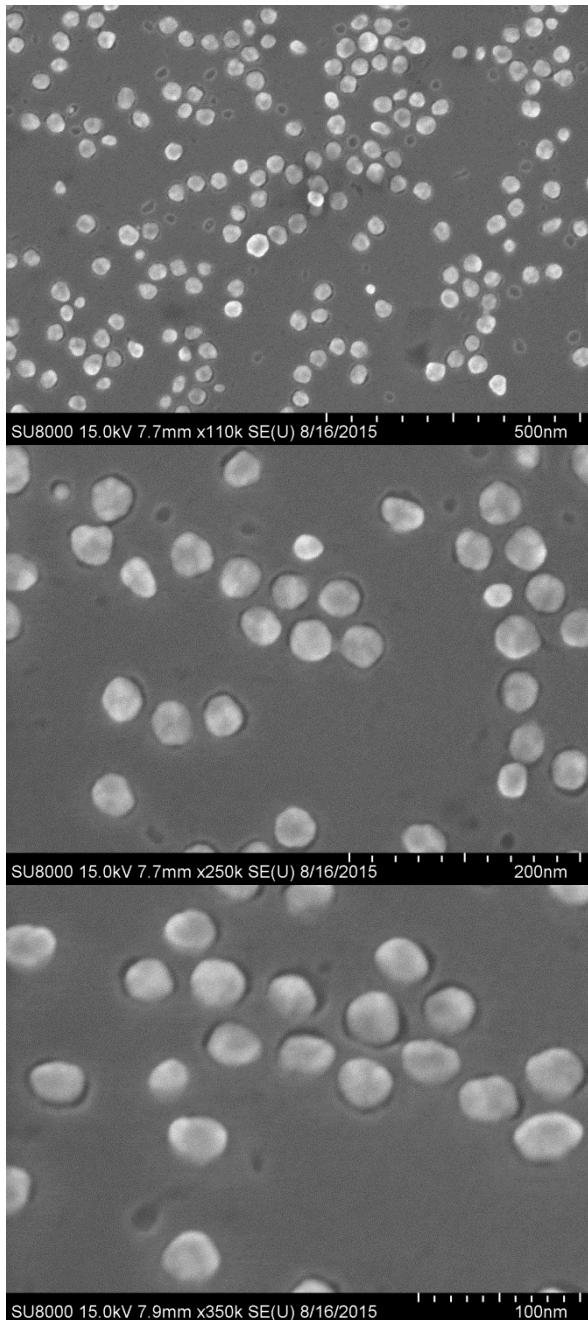
(Column II: Closer to sample edge)



## #BL9777\_01G

R10.5 RIE                    **9 s**  
SiNx RIE:                    **17 s**  
ASH, Front (FC):            **20 s (No)**  
ASH, Backside (FC):        **15 s (No)**

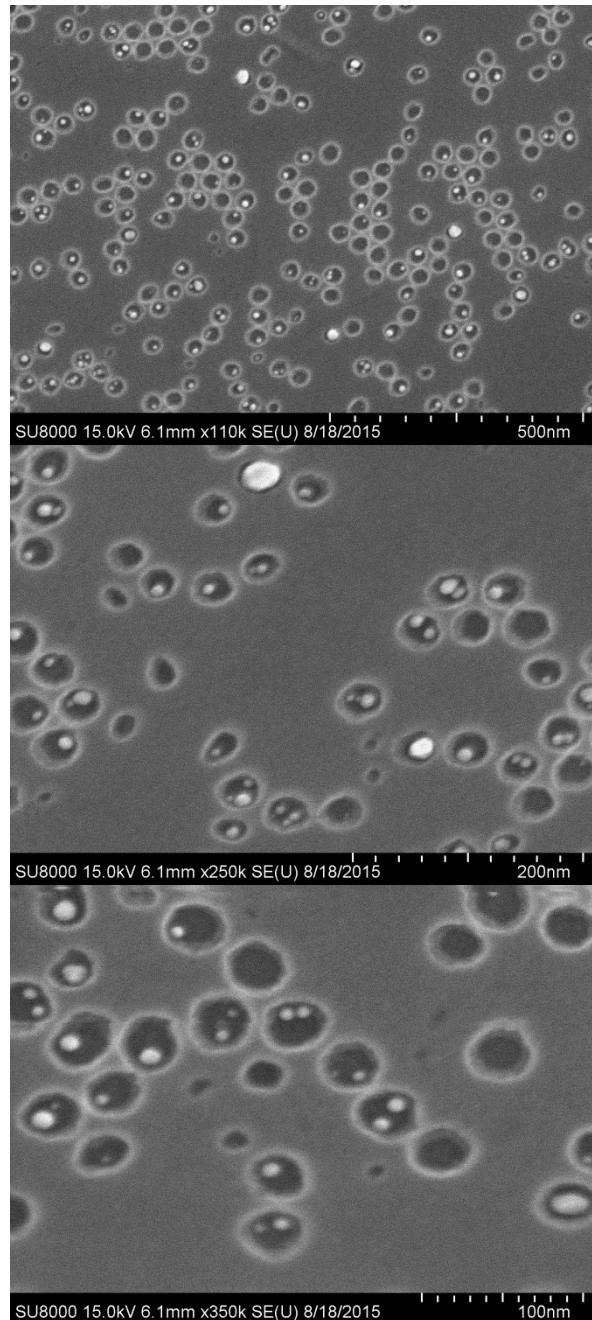
**Electrodeposition** (Performed twice)  
Nom. Current:                **450 mA**  
Nom. Time:                    **10 s + 10 s**  
NB: Current fluctuations first time!



## #BL9777\_01I

R10.5 RIE                    **9 s**  
SiNx RIE:                    **15 s**  
ASH, Front (FC):            **60 s (No)**  
ASH, Backside (FC):        **15 s (No)**

**Electrodeposition** (Performed twice)  
Nom. Current:                **1st: 450 mA + 2nd: 240 mA**  
Nom. Time:                    **~10 s + 10 s**  
NB: Timer died first time!

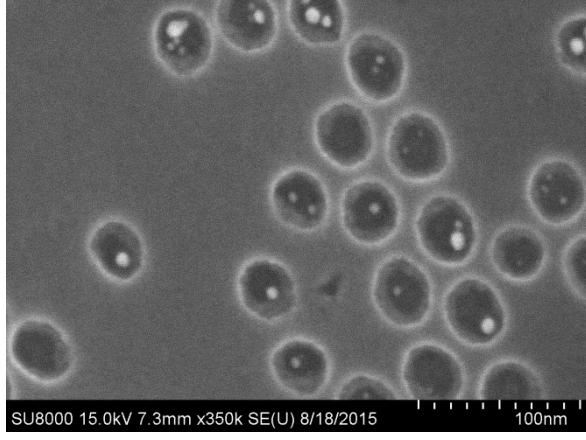
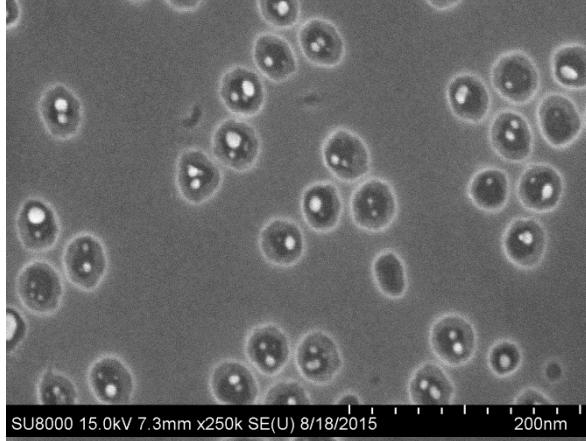
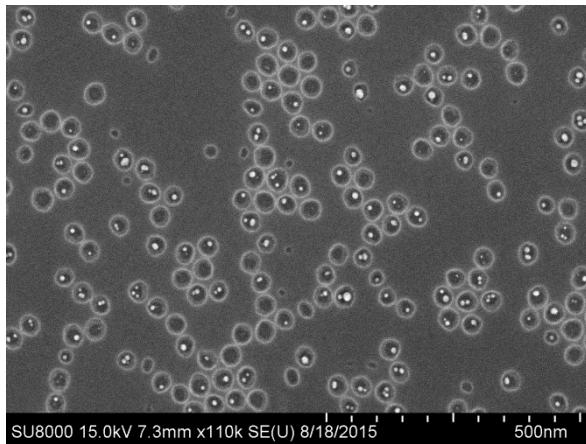


## #BL9777\_01J

R10.5 RIE                    9 s  
SiNx RIE:                15 s  
ASH, Front (FC):        None + 90 s (No)  
ASH, Backside (FC):     15 s

### Electrodeposition (Performed twice)

Nom. Current:            450 mA  
Nom. Time:                10 s + 10 s  
NB: No ash first time (i.e. polymer still on)

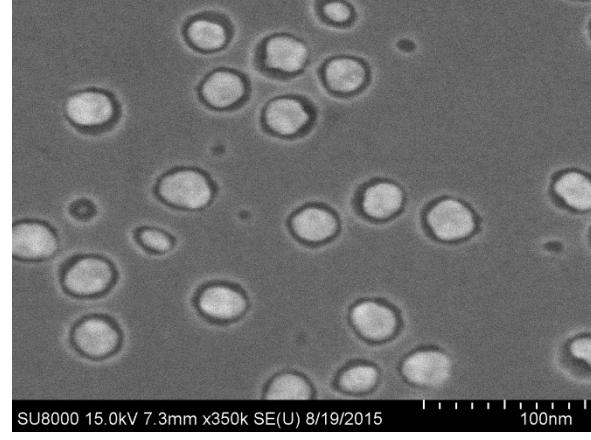
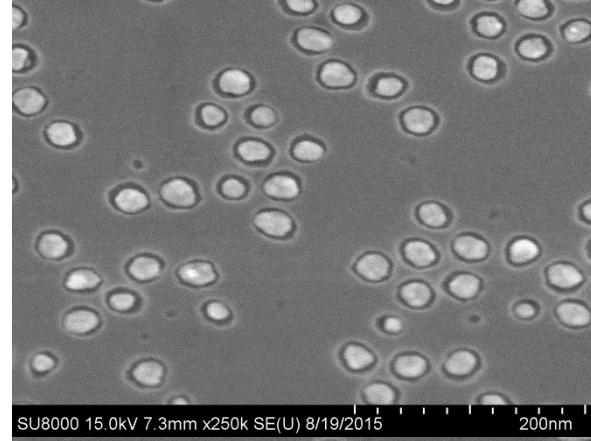
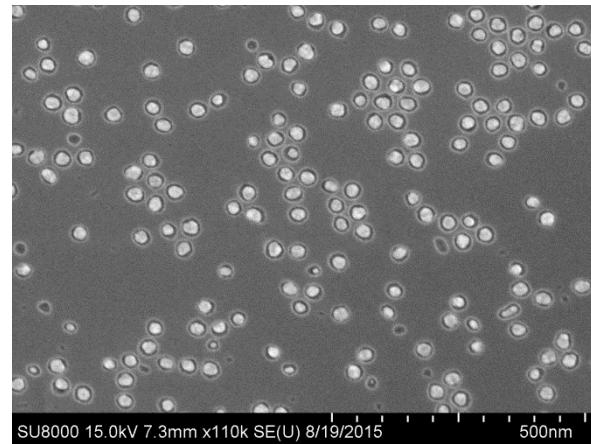


## #BL9777\_01K

R10.5 RIE                    9 s  
SiNx RIE:                15 s  
ASH, Front (FC):        2 x 60 s (No)  
ASH, Backside (FC):     15 s

### Electrodeposition

Nom. Current:            450 mA  
Nom. Time:                10 s



## #BL977\_01L

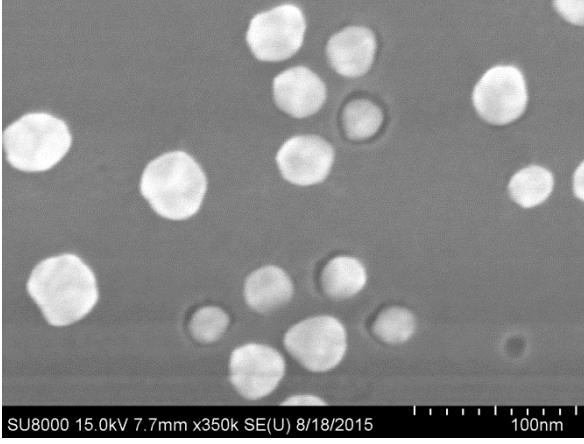
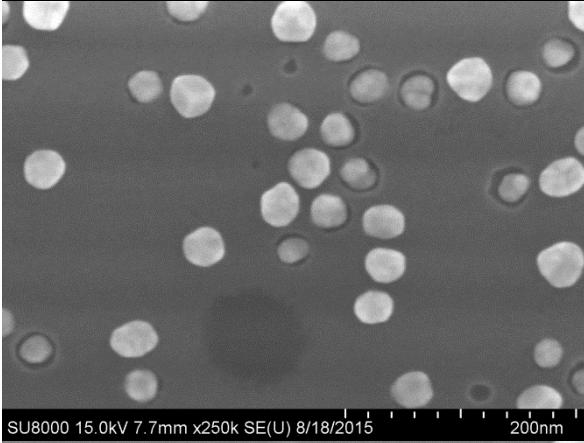
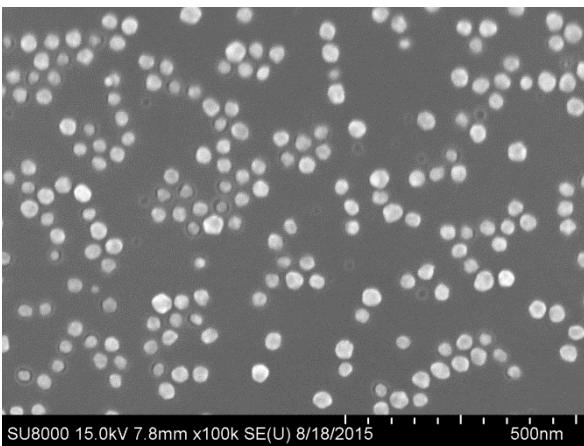
R10.5 RIE                   **9 s**  
SiNx RIE:                   **15 s**  
ASH, Front (FC):           **2 x 60 s (No)**  
ASH, Backside (FC):       **15 s**

### Electrodeposition (Performed twice)

Nom. Current:              **< 450 mA**

Nom. Time:                  **10 s + 5 s**

NB: Low current first time!

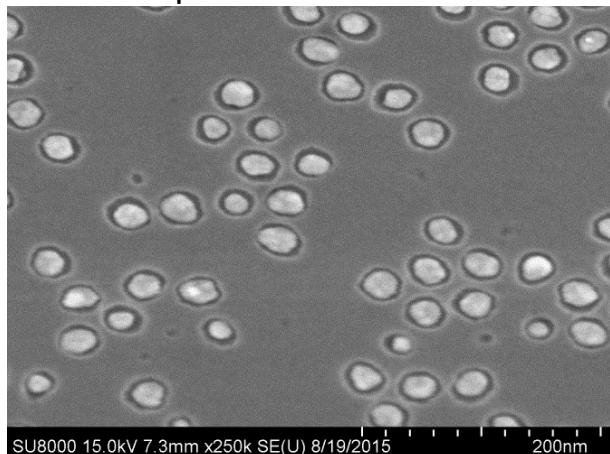


APPENDIX A6

**Metal-Organic Vapour-Phase Epitaxy (MOVPE)**

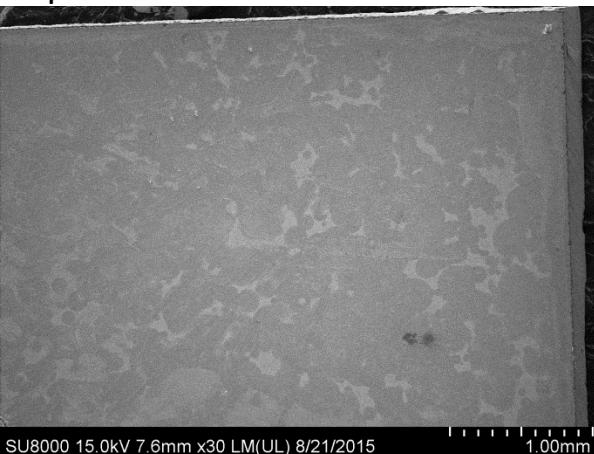
**MOVPE RUN #10551 - Sample #BL9777\_01K**

After electrodeposition



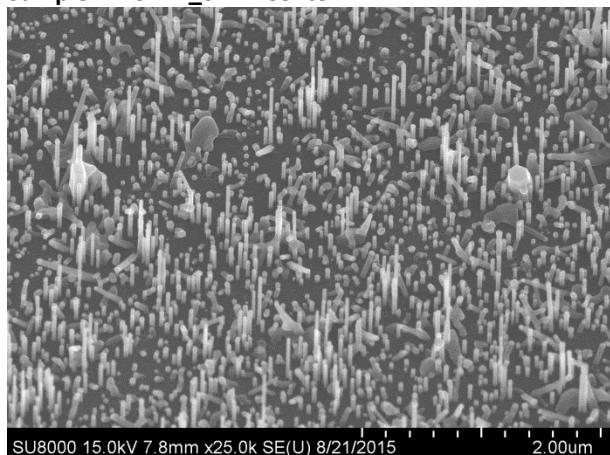
SU8000 15.0kV 7.3mm x250k SE(U) 8/19/2015

Sample overview after MOVPE

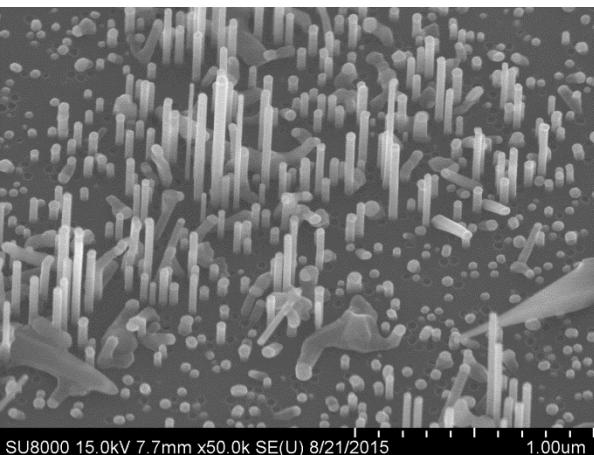


SU8000 15.0kV 7.6mm x30 LM(UL) 8/21/2015

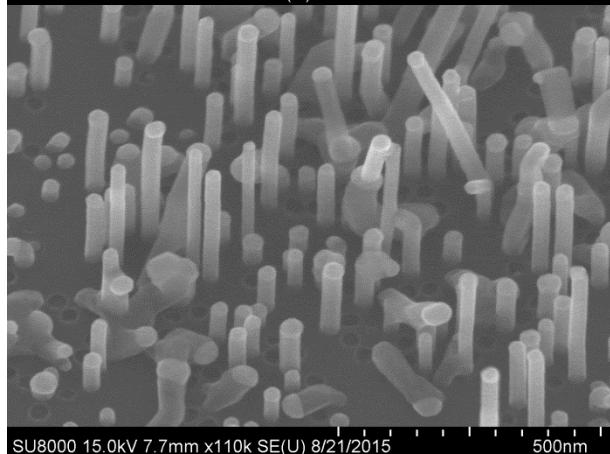
**Sample #BL9777\_01K - Center**



SU8000 15.0kV 7.8mm x25.0k SE(U) 8/21/2015



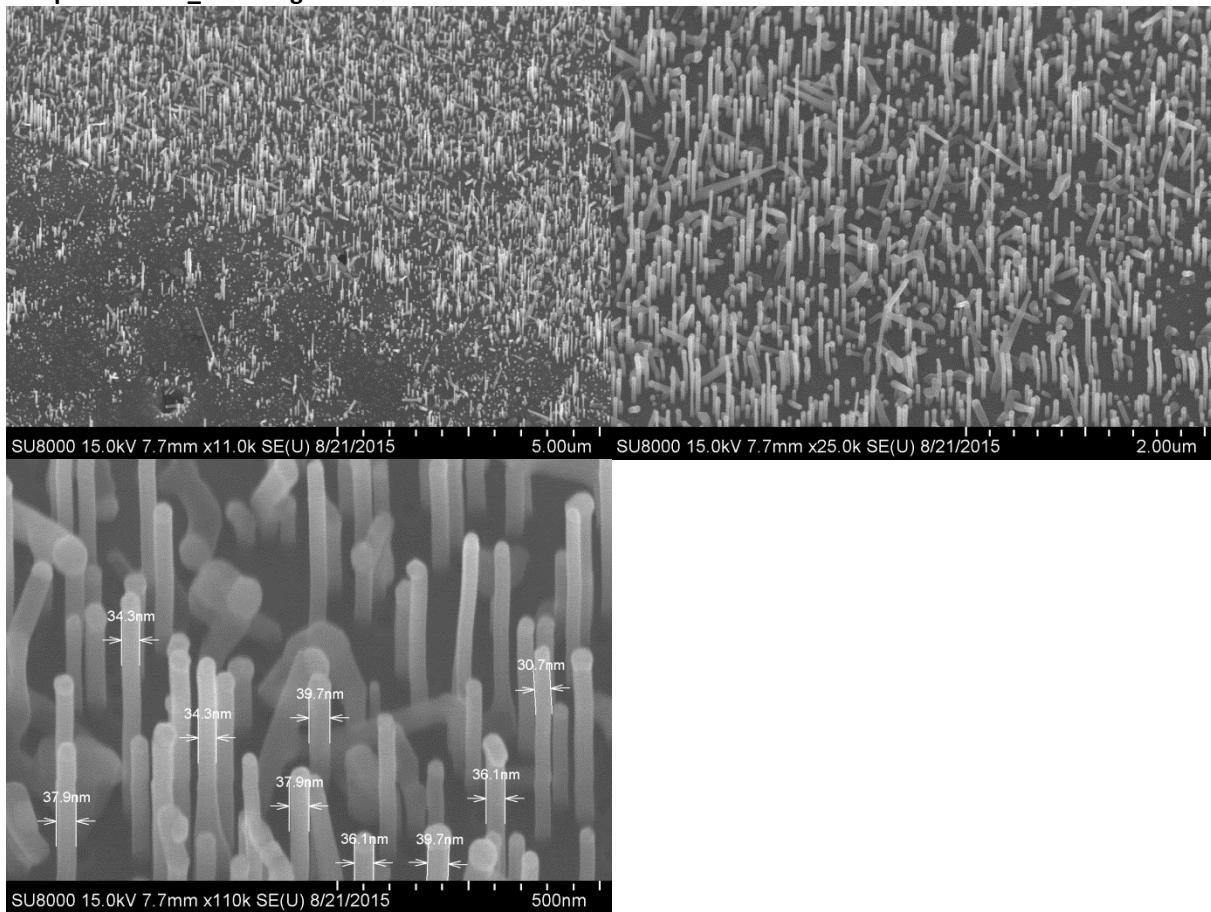
SU8000 15.0kV 7.7mm x50.0k SE(U) 8/21/2015



SU8000 15.0kV 7.7mm x110k SE(U) 8/21/2015

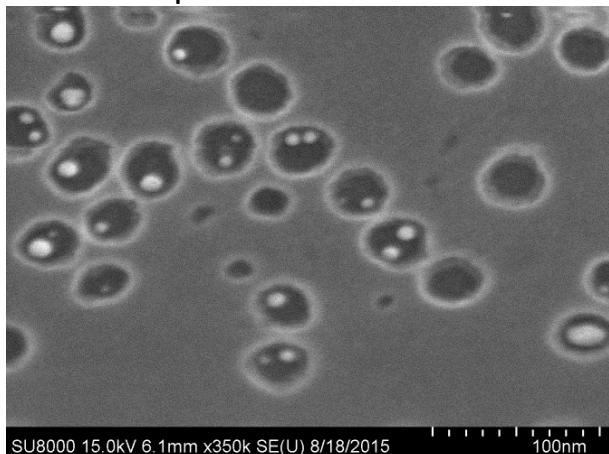
95

Sample #BL9777\_01K - Edge



**MOVPE RUN #10551 - Sample #BL9777\_01I**

After electrodeposition



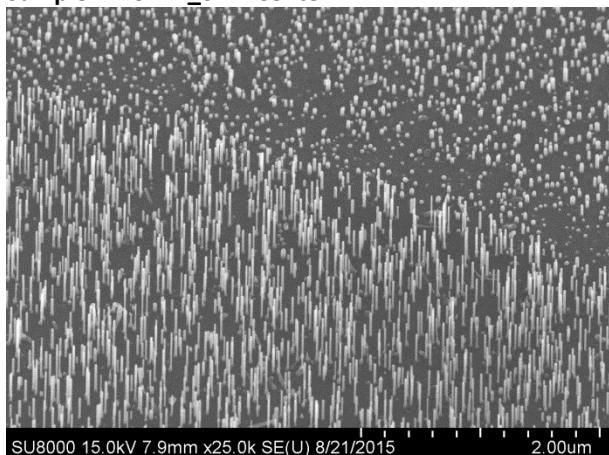
SU8000 15.0kV 6.1mm x350k SE(U) 8/18/2015

Sample overview after MOVPE

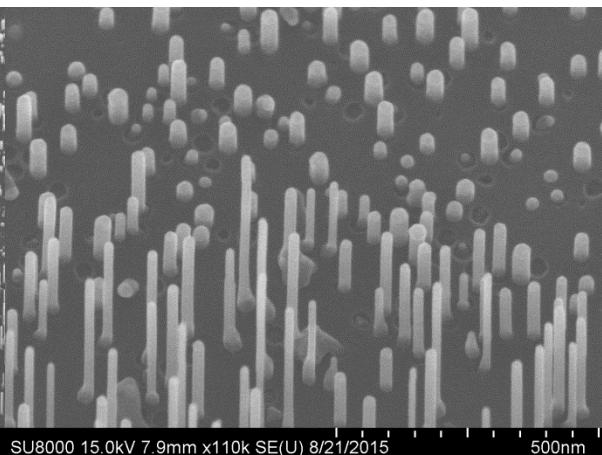


SU8000 15.0kV 7.7mm x30 LM(UL) 8/21/2015

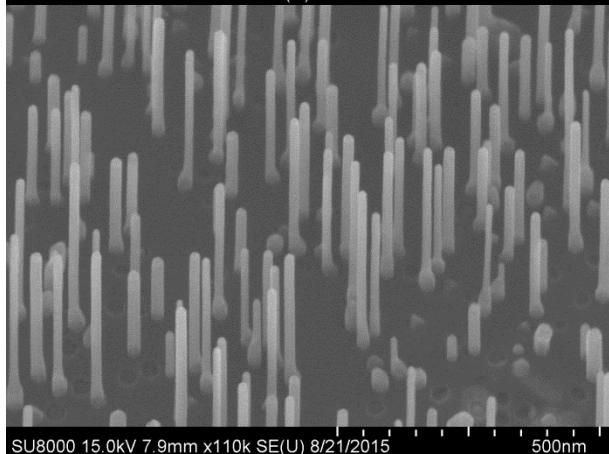
**Sample #BL9777\_01I - Center**



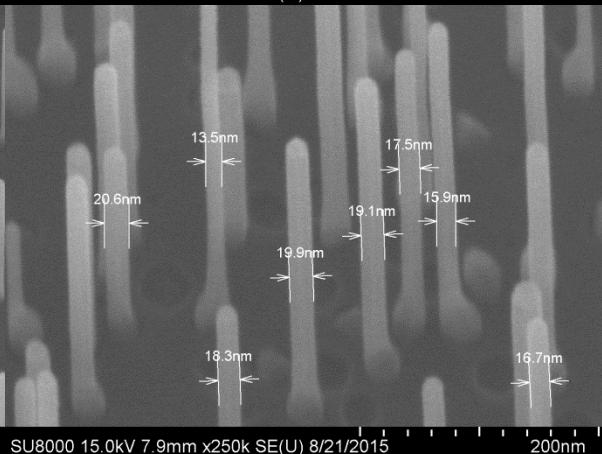
SU8000 15.0kV 7.9mm x25.0k SE(U) 8/21/2015



SU8000 15.0kV 7.9mm x110k SE(U) 8/21/2015



SU8000 15.0kV 7.9mm x110k SE(U) 8/21/2015



SU8000 15.0kV 7.9mm x250k SE(U) 8/21/2015

16.7 nm

15.9 nm

17.5 nm

19.1 nm

19.9 nm

18.3 nm

20.6 nm

13.5 nm

16.7 nm

15.9 nm

17.5 nm

19.1 nm

19.9 nm

18.3 nm

20.6 nm

13.5 nm

16.7 nm

15.9 nm

17.5 nm

19.1 nm

19.9 nm

18.3 nm

20.6 nm

13.5 nm

16.7 nm

15.9 nm

17.5 nm

19.1 nm

19.9 nm

18.3 nm

20.6 nm

13.5 nm

16.7 nm

15.9 nm

17.5 nm

19.1 nm

19.9 nm

18.3 nm

20.6 nm

13.5 nm

16.7 nm

15.9 nm

17.5 nm

19.1 nm

19.9 nm

18.3 nm

20.6 nm

13.5 nm

16.7 nm

15.9 nm

17.5 nm

19.1 nm

19.9 nm

18.3 nm

20.6 nm

13.5 nm

16.7 nm

15.9 nm

17.5 nm

19.1 nm

19.9 nm

18.3 nm

20.6 nm

13.5 nm

16.7 nm

15.9 nm

17.5 nm

19.1 nm

19.9 nm

18.3 nm

20.6 nm

13.5 nm

16.7 nm

15.9 nm

17.5 nm

19.1 nm

19.9 nm

18.3 nm

20.6 nm

13.5 nm

16.7 nm

15.9 nm

17.5 nm

19.1 nm

19.9 nm

18.3 nm

20.6 nm

13.5 nm

16.7 nm

15.9 nm

17.5 nm

19.1 nm

19.9 nm

18.3 nm

20.6 nm

13.5 nm

16.7 nm

15.9 nm

17.5 nm

19.1 nm

19.9 nm

18.3 nm

20.6 nm

13.5 nm

16.7 nm

15.9 nm

17.5 nm

19.1 nm

19.9 nm

18.3 nm

20.6 nm

13.5 nm

16.7 nm

15.9 nm

17.5 nm

19.1 nm

19.9 nm

18.3 nm

20.6 nm

13.5 nm

16.7 nm

15.9 nm

17.5 nm

19.1 nm

19.9 nm

18.3 nm

20.6 nm

13.5 nm

16.7 nm

15.9 nm

17.5 nm

19.1 nm

19.9 nm

18.3 nm

20.6 nm

13.5 nm

16.7 nm

15.9 nm

17.5 nm

19.1 nm

19.9 nm

18.3 nm

20.6 nm

13.5 nm

16.7 nm

15.9 nm

17.5 nm

19.1 nm

19.9 nm

18.3 nm

20.6 nm

13.5 nm

16.7 nm

15.9 nm

17.5 nm

19.1 nm

19.9 nm

18.3 nm

20.6 nm

13.5 nm

16.7 nm

15.9 nm

17.5 nm

19.1 nm

19.9 nm

18.3 nm

20.6 nm

13.5 nm

16.7 nm

15.9 nm

17.5 nm

19.1 nm

19.9 nm

18.3 nm

20.6 nm

13.5 nm

16.7 nm

15.9 nm

17.5 nm

19.1 nm

19.9 nm

18.3 nm

20.6 nm

13.5 nm

16.7 nm

15.9 nm

17.5 nm

19.1 nm

19.9 nm

18.3 nm

20.6 nm

13.5 nm

16.7 nm

15.9 nm

17.5 nm

19.1 nm

19.9 nm

18.3 nm

20.6 nm

13.5 nm

16.7 nm

15.9 nm

17.5 nm

19.1 nm

19.9 nm

18.3 nm

20.6 nm

13.5 nm

16.7 nm

15.9 nm

17.5 nm

19.1 nm

19.9 nm

18.3 nm

20.6 nm

13.5 nm

16.7 nm

15.9 nm

17.5 nm

19.1 nm

19.9 nm

18.3 nm

20.6 nm

13.5 nm

16.7 nm

15.9 nm

17.5 nm

19.1 nm

19.9 nm

18.3 nm

20.6 nm

13.5 nm

16.7 nm

15.9 nm

17.5 nm

19.1 nm

19.9 nm

18.3 nm

20.6 nm

13.5 nm

16.7 nm

15.9 nm

17.5 nm

19.1 nm

19.9 nm

18.3 nm

20.6 nm

13.5 nm

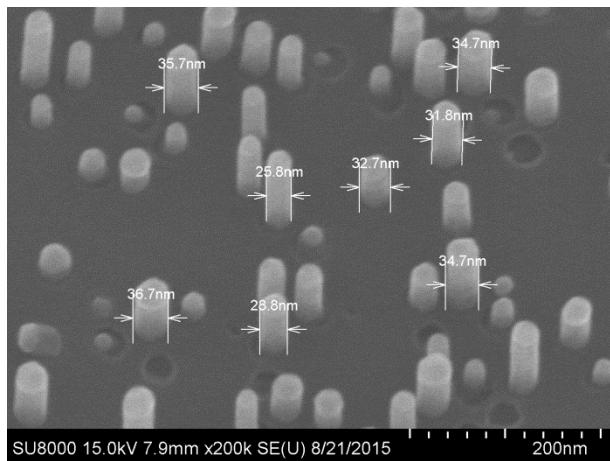
16.7 nm

15.9 nm

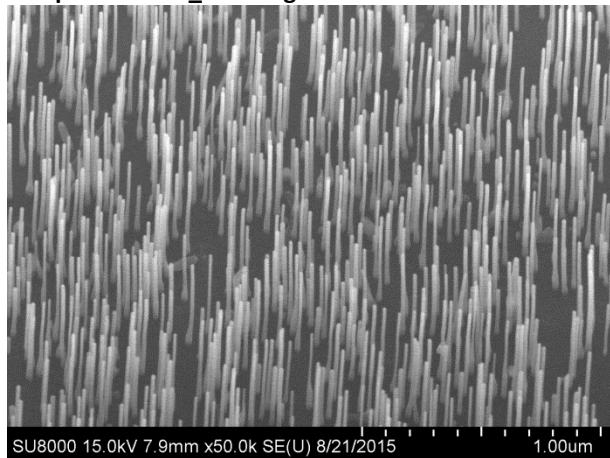
17.5 nm

19.1 nm

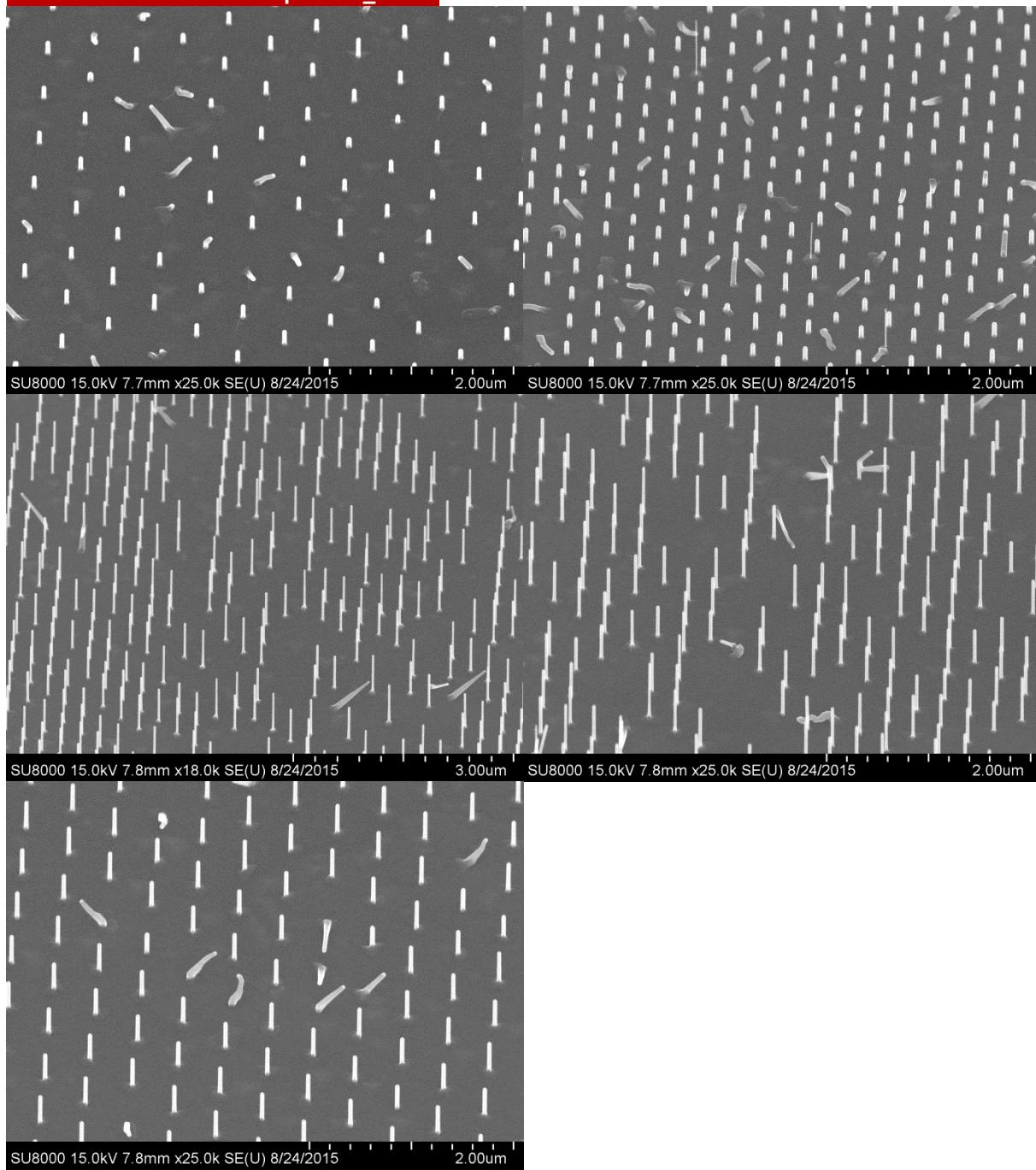
&lt;



Sample #BL9777\_01I - Edge

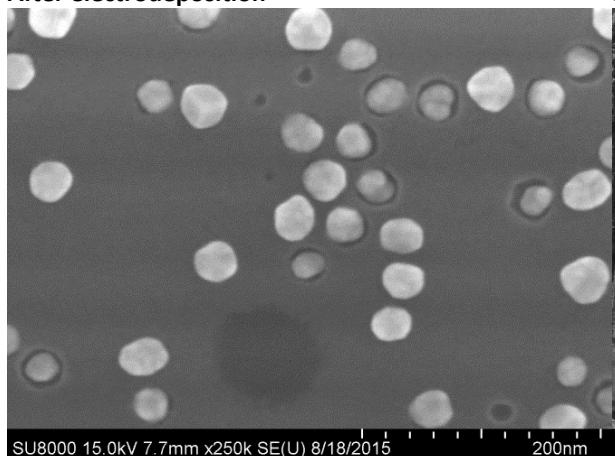


**MOVPE RUN #10551 - Sample #GT\_10551**



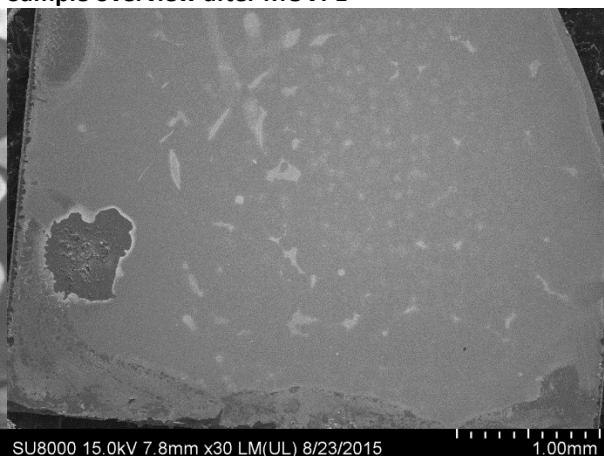
**MOVPE RUN #10552 - Sample #BL9777\_01L**

After electrodeposition



SU8000 15.0kV 7.7mm x250k SE(U) 8/18/2015

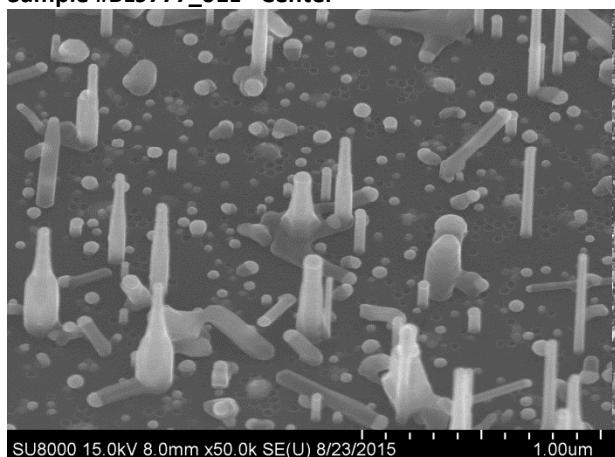
Sample overview after MOVPE



SU8000 15.0kV 7.8mm x30 LM(UL) 8/23/2015

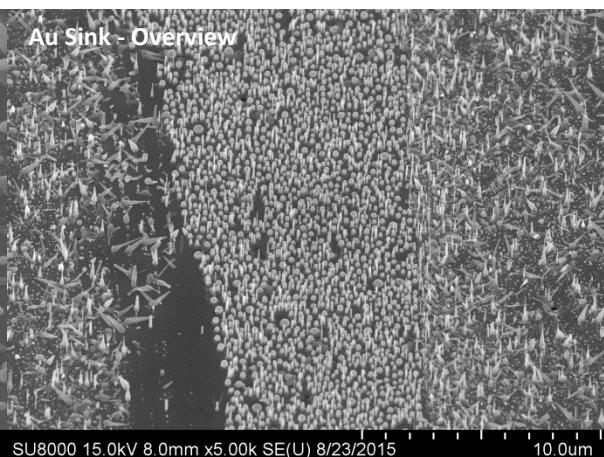
1.00mm

**Sample #BL9777\_01L - Center**



SU8000 15.0kV 8.0mm x50.0k SE(U) 8/23/2015

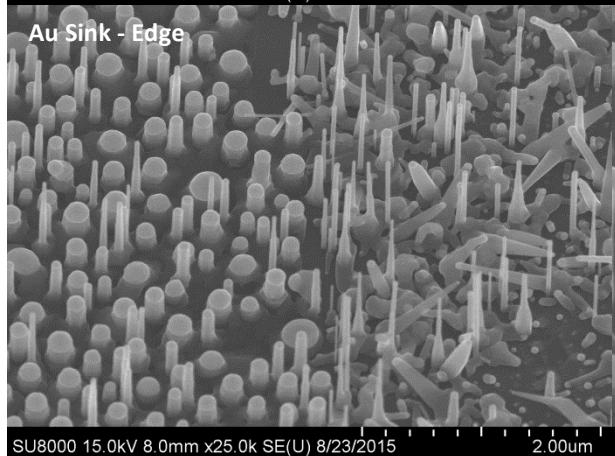
Au Sink - Overview



SU8000 15.0kV 8.0mm x5.00k SE(U) 8/23/2015

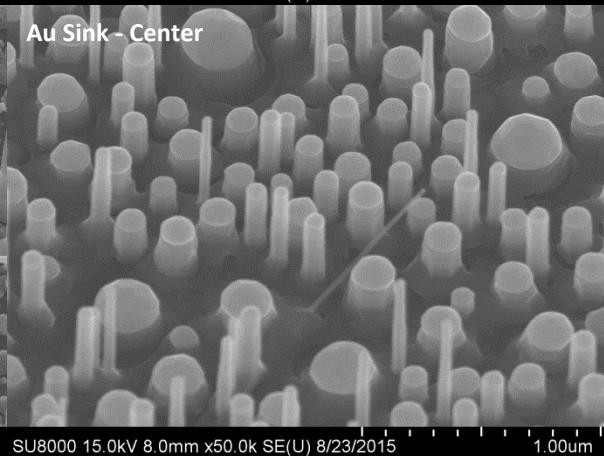
10.0um

**Au Sink - Edge**



SU8000 15.0kV 8.0mm x25.0k SE(U) 8/23/2015

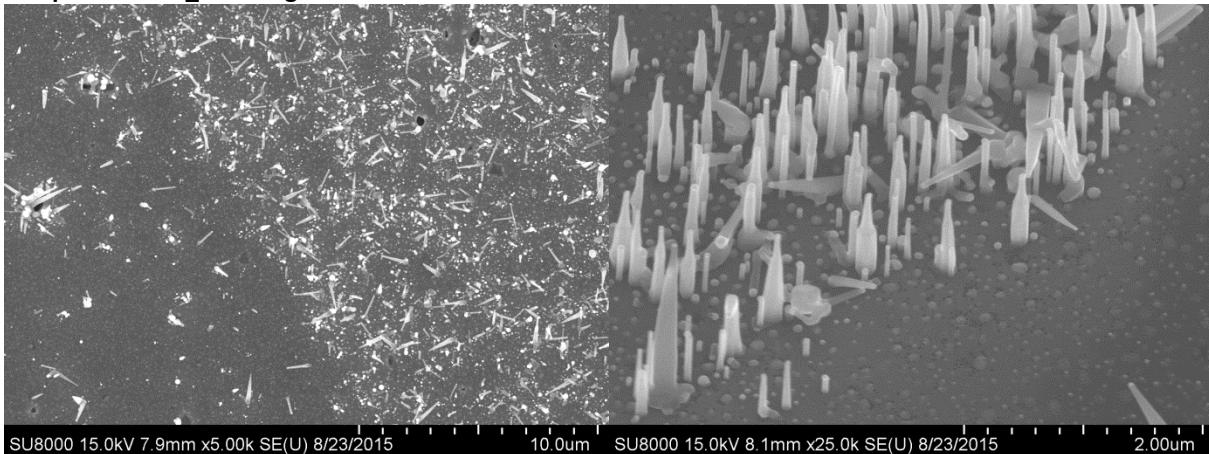
**Au Sink - Center**



SU8000 15.0kV 8.0mm x50.0k SE(U) 8/23/2015

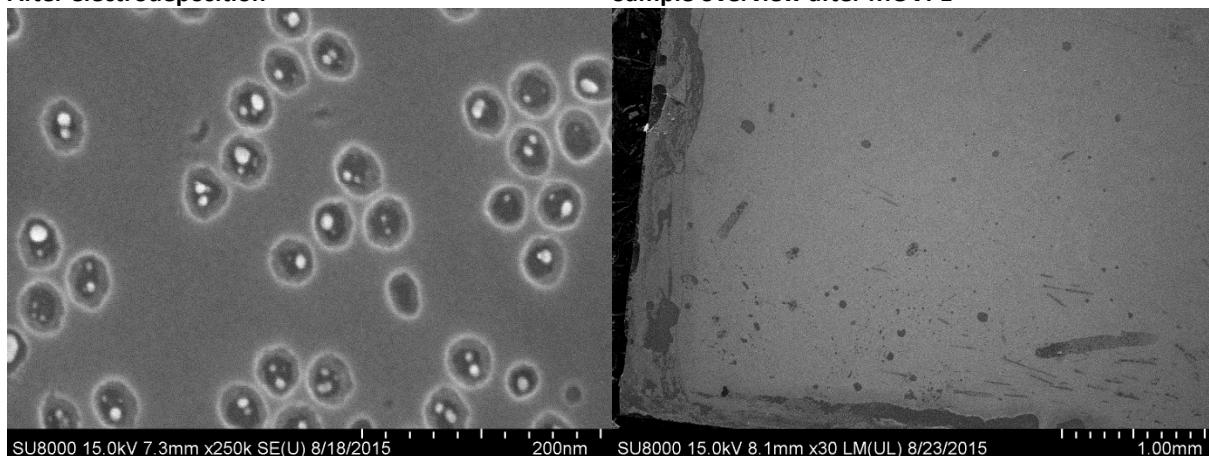
1.00um

Sample #BL9777\_01L - Edge



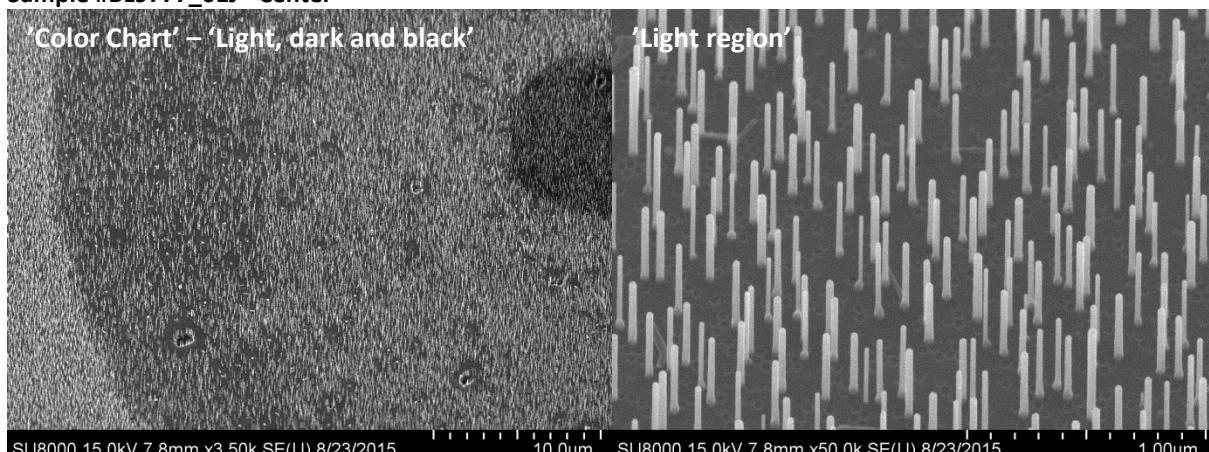
**MOVPE RUN #10552 - Sample #BL9777\_01J**

After electrodeposition

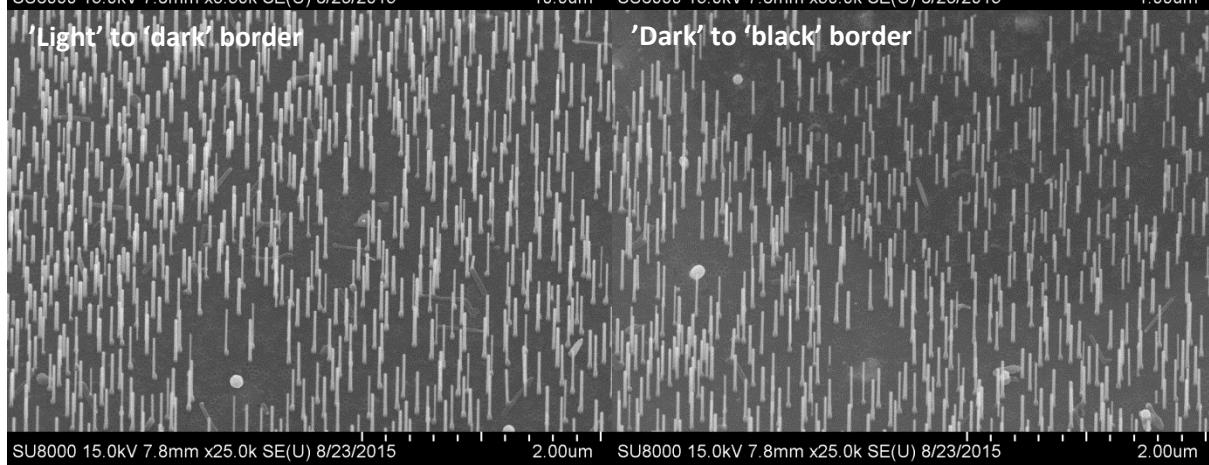


Sample overview after MOVPE

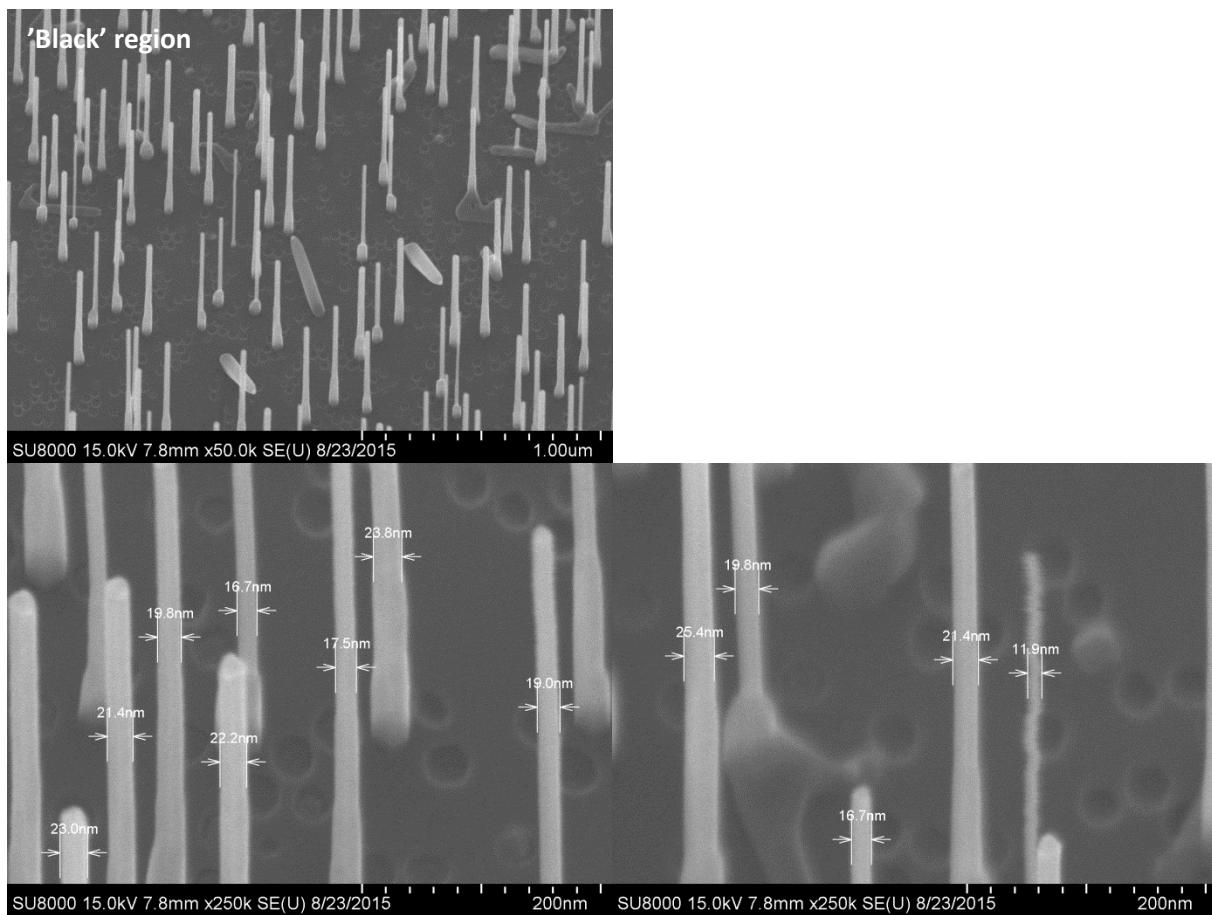
Sample #BL9777\_01J - Center



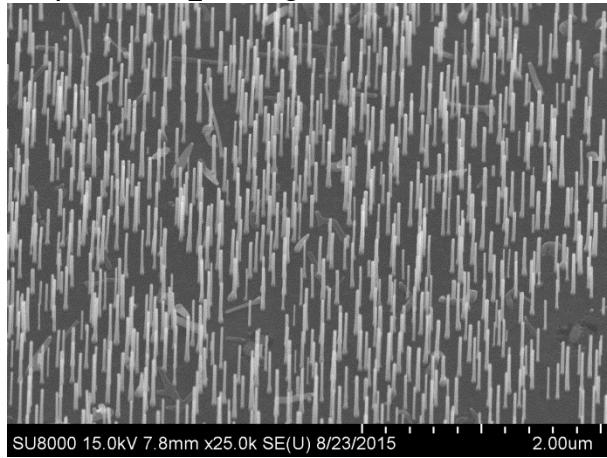
'Light region'



'Dark' to 'black' border



Sample #BL9777\_01J - Edge



**MOVPE RUN #10552 - Sample #GT\_10552**

