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On the Solution of the Stationary Riccati Equation by Integration

Choice of Steplength

Lindahl, Sture

1974

Document Version:

Publisher's PDF, also known as Version of record

[Link to publication](#)

Citation for published version (APA):

Lindahl, S. (1974). *On the Solution of the Stationary Riccati Equation by Integration: Choice of Steplength.* (Research Reports TFRT-3115). Department of Automatic Control, Lund Institute of Technology (LTH).

Total number of authors:

1

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ON THE SOLUTION OF THE STATIONARY RICCATI
EQUATION BY INTEGRATION - CHOICE OF
STEPLength

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September 1974

Dokumentutgivare
Lund Institute of Technology
Handläggare Dept of Automatic Control
0610
Författare
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Dokumentnamn
RÉPORT LUTFD2/(TFRT-8115)/1-42/(1974)
Utgivningsdatum
Sept 1974
Ärendebeteckning
06T6

10T4

Dokumenttitel och undertitel

1810
On the solution of the stationary Riccati equation by integration-choice
of steplength

Referat (sammandrag)

3610
One way to solve the stationary Riccati equation

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is to integrate the associated differential equation

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until ds/dt is zero. In order to reduce the computation time it is desirable to increase the steplength as much as possible. The numerical stability of the integration method limits the steplength. In this report the results of some numerical experiments are given. A rule of thumb for the choice of steplength is also given.

Referat skrivet av
Author

Förslag till ytterligare nyckelord
/ / Tn

Klassifikationssystem och -klass(er)
5010

Indexterminer (ange källa)

5210
Numerical integration (Thesaurus of Engineering and Scientific Terms,
Engineers Joint Council, N.Y., USA)

DOCU MENT DATABA SE omfattar SIS:62 10-12

Omfång 421 pages	Övriga bibliografiska uppgifter 56T2
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Språk English	
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Sekretessuppgifter 60T0	
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Dokumentet kan erhållas från Department of Automatic Control Lund Institute of Technology Box 725, S-220 07 LUND 7, Sweden	Mottagarens uppgifter 62T4
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ON THE SOLUTION OF THE STATIONARY RICCATI EQUATION BY
INTEGRATION-CHOICE OF STEPLENGTH

STURE LINDAHL

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ON THE SOLUTION OF THE STATIONARY RICCATI EQUATION BY
INTEGRATION-CHOICE OF STEPLENGTH

ABSTRACT

One way to solve the stationary Riccati equation

$$0 = A^T X + XA - XBQ_2^{-1} B^T X + Q_1$$

is to integrate the associated differential equation

$$-\frac{dS}{dt} = A^T S + SA - SBQ_2^{-1} B^T S + Q_1$$

until dS/dt is zero. In order to reduce the computation time it is desirable to increase the steplength as much as possible. The numerical stability of the integration method limits the steplength. In this report the results of some numerical experiments are given. A rule of thumb for the choice of steplength is also given.

1. INTRODUCTION

Consider the linear, time-invariant stabilizable system

$$\frac{dx}{dt} = Ax + Bu \quad (1.1)$$

and the quadratic cost functional to be minimized

$$V = \int_0^{\infty} [x^T(s) Q_1 x(s) + u^T(s) Q_2 u(s)] ds \quad (1.2)$$

where x is the n -dimensional state vector, u the r -dimensional control vector, A a $n \times n$ -matrix and B a $n \times r$ -matrix. The symmetric $n \times n$ -matrix, Q_1 , is non-negative definite, and Q_2 is a positive definite symmetric $r \times r$ -matrix.

The optimal control is a linear, time-invariant feedback

$$u(t) = -L x(t) \quad (1.3)$$

where

$$L = Q_2^{-1} B^T X \quad (1.4)$$

and X is a symmetric non-negative, definite solution of the algebraic Riccati equation

$$A^T X + X A - X B Q_2^{-1} B^T X + Q_1 = 0 \quad (1.5)$$

There are at least four different methods of solving (1.5).

Method A.

Let

$$a_i = \begin{bmatrix} b_i \\ c_i \end{bmatrix} \quad i = 1, 2, \dots, n$$

be eigenvectors of

$$E = \begin{bmatrix} A & -BQ_2^{-1}B^T \\ -Q_1 & -A^T \end{bmatrix}$$

In [1] it is shown that each solution of (1.5) can be expressed as

$$x = [c_1, c_2, \dots, c_n][b_1, b_2, \dots, b_n]^{-1}$$

where the inverse is assumed to exist for certain combinations of eigenvectors. Conversely, if $[b_1, b_2, \dots, b_n]$ is non-singular, then

$$x = [c_1, c_2, \dots, c_n][b_1, b_2, \dots, b_n]^{-1}$$

satisfies (1.5)

Method B.

Consider

$$J = \frac{1}{2} x^T(t_1) Q_0 x(t_1) + \frac{1}{2} \int_{t_0}^{t_1} [x^T(s) Q_1 x(s) + u^T(s) Q_2 u(s)] ds \quad (1.6)$$

The optimal control is a linear feedback

$$u(t) = -Q_2^{-1} B^T S(t) x(t) \quad (1.7)$$

where $S(t)$ is a solution of the Riccati equation

$$-\frac{ds}{dt} = A^T S + S A - S B Q_2^{-1} B^T S + Q_1 \quad (1.8)$$

$$S(t_1) = Q_0 \quad (1.9)$$

Let $\pi(t; Q_0, t_1)$ be the solution of (1.8) with the initial condition

$$\pi(t_1; Q_0, t_1) = Q_0 \quad (1.10)$$

Using the fact that the system is stabilizable, it can be shown [1] that

$$\lim_{t \rightarrow -\infty} \pi(t; 0, t_1) = \bar{S} \quad (1.11)$$

exists. \bar{S} is a non-negative, definite solution of (1.5). Using the fundamental matrix approach

$$\pi(t; Q_0, t_1) = [\Sigma_{21}(t; t_1) + \Sigma_{22}(t; t_1)Q_0] \cdot$$

$$[\Sigma_{11}(t; t_1) + \Sigma_{12}(t; t_1)Q_0]^{-1} \quad (1.12)$$

where

$$\Sigma(t, t_1) = \begin{bmatrix} \Sigma_{11}(t; t_1) & \Sigma_{12}(t; t_1) \\ \Sigma_{21}(t; t_1) & \Sigma_{22}(t; t_1) \end{bmatrix} \quad (1.13)$$

and

$$\frac{d}{dt} \Sigma(t; t_1) = E \Sigma(t; t_1) \quad (1.14)$$

$\pi(t; 0, t_1)$ is computed for increasing value of $t_1 - t$ until a stationary solution is reached with desired accuracy.

Method C.

The optimal regulator problem can also be solved by straightforward integration of (1.8) until a stationary solution is reached with desired accuracy. In [2] a fourth-order Runge-

Kutta method was used.

Method D (Kleinman's method),

Kleinman [5] has proposed that Newton's method should be used in order to solve (1.5). In each iteration we have to solve the Lyapunov equation

$$A_K^T V_k + V_k A_k + Q_1 + L_k^T Q_2 L_k = 0$$

where

$$A_k = A - BL_k$$

and

$$L_k = Q_2^{-1} B^T V_{k-1}$$

The author has no experience with this method.

Choice of method.

Using method A we have to compute all eigenvalues and all eigenvectors of a $2n \times 2n$ -matrix, invert a $n \times n$ -matrix and compute a couple of $n \times n$ -matrix products. For high-order systems the eigenvalue problem can cause numerical difficulties, especially if there are multiple eigenvalues.

Using method B we have to compute the transition matrix for (1.14), and for high-order systems this may lead to computational difficulties.

Method C is computationally simpler than method A and method B since it can be shown [1] that the numerical integration is a stable procedure. The disadvantage of method

C is that it is time consuming. In order to reduce the computation time it is desirable to increase the step-length as much as possible. The numerical stability of the integration method used limits the steplength. The results of some numerical experiments with (1.8) is given and a rule of thumb for the steplength is also given.

2. CHOICE OF STEPLENGTH

Consider the matrix differential equation

$$-\frac{dS}{dt} = A^T S + SA - SBQ_2^{-1} B^T S + Q_1 \quad (2.1)$$

$$S(t_1) = Q_0 \quad (2.2)$$

Our problem is to determine the maximum possible steplength, h_{\max} .

Let S_1 denote the exact solution of (2.1) and S_2 an approximate solution of (2.1) obtained by numerical integration.

Introducing $\Delta S = S_1 - S_2$ we can derive the following differential equation for ΔS

$$-\frac{d}{dt} \Delta S = (A - BQ_2^{-1} B^T S_1)^T \Delta S + \Delta S (A - BQ_2^{-1} B^T S_1) + \Delta S B Q_2^{-1} B^T \Delta S \quad (2.3)$$

with the initial condition

$$\Delta S(t_1) = 0 \quad (2.4)$$

Equation (2.3) can also be written as

$$-\frac{d}{dt} \Delta S = F^T(t) \Delta S + \Delta S F(t) + \Delta S B Q_2^{-1} B^T \Delta S \quad (2.5)$$

where

$$F(t) = [A - BQ_2^{-1} B^T S_1(t)] \quad (2.6)$$

Introducing $z = (\Delta s_{11}, \Delta s_{21}, \dots, \Delta s_{nn})^T$ equation (2.5) can be written as

$$\frac{dz}{dt} = G(t)z + O(||z||^2) \quad (2.7)$$

The eigenvalues $\mu_k(t)$ of $G(t)$ are given by [3]

$$\mu_k(t) = \lambda_i(t) + \lambda_j(t) \quad i, j = 1, 2, \dots, n \quad (2.8)$$

where $\lambda_i(t)$ is an eigenvalue of $F(t)$. To obtain numerical stability for equation (2.1) it seems reasonable to use a steplength which makes

$$\frac{dz}{dt} = G(t)z \quad (2.9)$$

numerically stable for all t .

This means that we obtain the following rule of thumb

$$h_{\max} \leq \hat{h}$$

where

$$\mu_i(t)\hat{h} \in D_s$$

and D_s is the domain of stability for the integration method used.

If we use a fourth-order Runge-Kutta method to integrate

$$\frac{dy}{dt} = My \quad (2.10)$$

it is known [4] that this integration procedure is stable if

and only if

$$h \rho_i \in \Omega \quad \forall i \quad i = 1, 2, \dots, N$$

where ρ_i is an eigenvalue of M and

$$\Omega = \{\alpha \in \mathbb{C}; |1 + \alpha + \alpha^2/2 + \alpha^3/6 + \alpha^4/24| < 1\}$$

3. NUMERICAL EXPERIMENTS

In this section the results of some numerical experiments are given.

Example 1

The system is

$$\frac{dx}{dt} = u \quad (3.1)$$

and the cost functional is

$$V = \int_0^\infty [100x^2(s) + u^2(s)]ds \quad (3.2)$$

It is possible to calculate an expression for $S(t)$ and $L(t)$

$$S(t) = 10(1-e^{-20t})/(1+e^{-20t}) \quad (3.3)$$

$$L(t) = 10(1-e^{-20t})/(1+e^{-20t}) \quad (3.4)$$

It is also possible to calculate an expression for $\lambda(t)$

$$\lambda(t) = -10(1-e^{-20t})/(1+e^{-20t}) \quad (3.5)$$

The maximum possible steplength is $\hat{h} = 0.139$.

From table 3.1 we can see that if $h \leq 0.136$ the initial error is reduced to zero after 30 steps. If $h = 0.139$ (the predicted maximum steplength) then the initial error is not reduced. If $h > 0.140$ the initial error is increased.

From table 3.2 we can see the result if we start with $Q_0 = 0$. If $h \leq 0.136$ the solution approaches the correct solution. If $h \geq 0.140$ the difference equations defined by the fourth-order Runge-Kutta integration procedure seems to have another stationary solution than the stationary solution to the differential equation.

h	Number of steps (k)		
	0	10	20
0.100	10.000010	10.000000	10.000000
0.120	10.000010	10.000000	10.000000
0.124	10.000010	10.000000	10.000000
0.128	10.000010	10.000000	10.000000
0.132	10.000010	10.000000	10.000000
0.136	10.000010	10.000003	10.000000
0.138	10.000010	10.000006	10.000004
0.139	10.000010	10.000010	10.000010
0.140	10.000010	10.000010	10.000010
0.160	10.000010	10.004057	10.900070
0.180	10.000010	10.673110	11.235236
0.200	10.000010	-7.8973007	-6.1129192
			-6.3156540

Table 3.1. $S(k \cdot h)$ for different steplengths and Q_0 in the neighbourhood of the stationary solution, $X = 10$.

h	Number of steps (k)			
	0	10	20	30
0.100	0.0000000	9.9998834	9.9999999	9.9999999
0.120	0.0000000	9.9888766	9.9999672	10.000000
0.124	0.0000000	9.9656295	9.9996639	9.9999968
0.128	0.0000000	9.8871715	9.9962034	9.9998761
0.132	0.0000000	9.6105378	9.9494184	9.9942882
0.136	0.0000000	8.7672235	9.2072164	9.5158461
0.140	0.0000000	7.4291753	7.4157795	7.4152622
0.160	0.0000000	3.7616103	3.7614541	3.7614541
0.180	0.0000000	-1.4746107	-1.4666215	-1.4667521
0.200	0.0000000	-1.5139580•10 ⁻⁵	-2.4889708•10 ⁻³	-0.40397096

Table 3.2. S(k•h) in Example 1 for different steplengths and $Q_0 = 0$.

Example 2

The system is

$$\frac{dx_1}{dt} = -x_1 + u_1$$

$$\frac{dx_2}{dt} = x_2 + u_2$$

and the cost functional is

$$V = \int_0^{\infty} [0.002001x_1^2(s) + u_1^2(s) + u_2^2(s)]ds$$

The eigenvalues λ_1 and λ_2 corresponding to the stationary solution of the Riccati equation are

$$\begin{aligned}\lambda_1 &= -1.001 \text{ and } \lambda_2 = -1.0. \text{ The maximum steplength is} \\ h &= 1.39.\end{aligned}$$

From table 3.3 and 3.4 we can see that if $h \geq 1.40$ the numerical solution becomes indefinite, but if $h < 1.39$ the numerical solution remains positive definite. We can also see that the numerical solution approaches the exact solution very slowly if the steplength is chosen near the predicted maximum steplength.

h	Number of steps (k)			
	0	10	20	30
1.00	0.0000000	0.99998273	1.0000000	1.0000000
1.20	0.0000000	0.99694269	0.99999069	0.99999999
1.24	0.0000000	0.98989057	0.99989801	0.99999901
1.28	0.0000000	0.96597843	0.99884576	0.99996089
1.32	0.0000000	0.88463093	0.98674634	0.99847821
1.36	0.0000000	0.60857983	0.84758890	0.94077613
1.38	0.0000000	0.27983353	0.48308406	0.62986818
1.39	0.0000000	0.02348535	0.04673550	0.06973800
1.40	0.0000000	-0.03238645	-0.07622321	-0.13631858
1.60	0.0000000	-63.571238	-62.552227	-62.551731

Table 3.3. 1000 $s_{11}(k \cdot h)$ in Example 2 for different steplengths and

$$Q_0 = \text{diag}(0.0, 1.9999).$$

h	Number of steps (k)		
	0	10	20
1.00	1.9999000	2.0000000	2.0000000
1.20	1.9999000	1.9999997	2.0000000
1.24	1.9999000	1.9999991	2.0000000
1.28	1.9999000	1.9999968	2.0000000
1.32	1.9999000	1.9999891	1.9999989
1.36	1.9999000	1.9999629	1.9999863
1.38	1.9999000	1.9999318	1.9999536
1.39	1.9999000	1.9999078	1.9999149
1.40	1.9999000	1.9998753	1.9998443
1.60	1.9999000	1.9524459	1.3759230

Table 3.4. $s_{22}(k \cdot h)$ in Example 2 for different steplengths and $Q_O = \text{diag}(0.0, 1.9999)$.

From table 3.5 and 3.6 we can see the result if $Q_0 = I$. The closed loop eigenvalues are then $\lambda_1(t_1) = -2.0$ and $\lambda_2(t_1) = 0.0$. The maximum steplength is now predicted to be ≈ 0.7 for $t = t_1$ and to be 1.39 when we reach the stationary value of the Riccati equation. If $h \geq 1.2$ the numerical solution "explodes", but if $h = 1.0$ the numerical solution approaches the correct solution. From table 3.5 and table 3.6 it can be seen that the choice of initial value (Q_0) can reduce the maximum steplength.

$Q_0 = 0$ and
From table 3.7 and 3.8 we can see that if h is sufficiently small the numerical solution approaches a positive, semi-definite solution of the algebraic Riccati equation. The closed loop eigenvalues are $\lambda_1 = -1.001$ and $\lambda_2 = 1.0$, i.e. the closed loop system is unstable.

h	Number of steps (k)		
	0	10	20
1.00	1000•0000	0.88122385	0.99999795
1.20	1000•0000	1.72•10 ³⁸	1.85•10 ³⁸
1.24	1000•0000	3.83•10 ⁻²⁸	1.39•10 ³⁴
			5.08•10 ³⁹

Table 3.5. $1000s_{11}$ (kh) in Example 2 for different steplengths and $Q_O = I$.

h	Number of steps (k)			
	0	10	20	30
1.00	1.0000000	1.9999883	2.0000000	2.0000000
1.20	1.0000000	1.9988877	1.9999967	2.0000000
1.24	1.0000000	1.9965630	1.9999664	1.9999997

Table 3.6. $s_{22}(k \cdot h)$ in Example 2 for different steplengths and $Q_O = I$.

h	Number of steps (k)			
	0	10	20	30
1.00	0.0000000	0.99998273	1.0000000	1.0000000
1.20	0.0000000	0.99694269	0.99999069	0.99999999
1.40	0.0000000	-0.32386451	0.76223211	-1.3631858
1.60	0.0000000	-635.71238	-625.52227	-625.51731

Table 3.7. $1000s_1(k \cdot h)$ in Example 2 for different steplengths and $Q_0 = 0$.

h	Number of steps (k)		
	0	10	20
1.00	0.0000000	0.0000000	0.0000000
1.20	0.0000000	0.0000000	0.0000000
1.40	0.0000000	0.0000000	0.0000000

Table 3.8. $s_{22}(k \cdot h)$ in Example 2 for different steplengths and $Q_O = 0$.

From table 3.9 and 3.10 we can see that if $Q_0 = 10 \cdot I$ the steplength must be chosen to be ≈ 0.15 in order to obtain numerical stability.

From table 3.11 and 3.12 we can see that it is possible to start with $Q_0 = \text{diag}(0.0, 1.0)$ and use a steplength near the maximum possible and obtain numerical stability.

h	Number of steps (k)			
	0	100	200	300
0.10	100000.000	1.0000034	1.0000001	1.0000001
0.15	100000.000	1.0000001	1.0000001	1.0000001
0.20	100000.000	-3.44•10 ³⁵	-1.05•10 ²⁷	-2.93•10 ³⁶

Table 3.9. 1000 $s_{11}(k \cdot h)$ in Example 2 for different steplengths and $Q_O = 10 \cdot I$.

h	Number of steps (k)			
	0	100	200	300
0.10	10.000000	2.0000001	2.0000001	2.0000001
0.15	10.000000	2.0000001	2.0000001	2.0000001
0.20	10.000000	2.0000000	2.0000000	2.0000000

Table 3.10. $s_{22}(k \cdot h)$ in Example 2 for different steplengths and $Q_0 = 10 \cdot I$.

h	Number of steps (k)			
	0	10	20	30
1.00	0.0000000	0.99998273	1.0000000	1.0000000
1.20	0.0000000	0.99694269	0.99999069	0.99999999
1.24	0.0000000	0.98989057	0.99989801	0.99999901
1.28	0.0000000	0.96597843	0.99884576	0.99996089
1.32	0.0000000	0.88463093	0.98674634	0.99847821
1.36	0.0000000	0.60857983	0.84758890	0.94077613
1.38	0.0000000	0.27983353	0.48308406	0.62986818
1.39	0.0000000	0.02348535	0.04673550	0.06973800
1.40	0.0000000	-0.32386451	-0.76223211	-1.3631858
1.60	0.0000000	-635.71238	-625.52227	-625.51731

Table 3.11. $1000s_{11}(k \cdot h)$ in Example 2 for different steplengths and $Q_O = \text{diag}(0.0, 1.0)$.

h	Number of steps (k)		
	0	10	20
1.00	1.0000000	1.9999883	2.0000000
1.20	1.0000000	1.998877	1.9999967
1.24	1.0000000	1.9965630	1.9999664
1.28	1.0000000	1.9887173	1.9996204
1.32	1.0000000	1.9610539	1.9949420
1.36	1.0000000	1.8767226	1.9207219
1.38	1.0000000	1.8100455	1.8193716
1.39	1.0000000	1.7756506	1.7767811
1.40	1.0000000	1.7429177	1.7415780
1.60	1.0000000	1.3761611	1.3761454

Table 3.12. $s_{22}(k \cdot h)$ in Example 2 for different steplengths and $Q_O = \text{diag}(0.0, 1.0)$.

Example 3.

The A-matrix is given in table 3.13 and the B-matrix is given in table 3.14. The matrices in the cost functional are defined in table 3.15, 3.16 and 3.17.

The absolute largest eigenvalue to $(A - BQ_2^{-1} B^T X)$ is $\lambda_{\max} = -0.86907$, and we predict the maximum possible steplength $\hat{h} = 1.60$. From table 3.18 and 3.19 we can see that if $h \leq 1.64$ the method is numerically stable. If the step-length is increased to 1.66 and larger, the numerical solution becomes indefinite as can be seen from table 3.20 and 3.21.

A-MATRIX

COLUMN	NR	1	2	3	4	5
ROW	NR 1	• 00000000	• 00000000	1• 00000000	• 00000000	• 00000000
ROW	NR 2	• 00000000	• 00000000	• 00000000	1• 00000000	• 00000000
ROW	NR 3	-• 13170980-04	-• 96791798-06	-• 20002711-03	• 54515979-07	-• 46031430-04
ROW	NR 4	-• 24601647-03	-• 18255061-03	.15007541-05	• 25000602-01	-• 18774520-03
ROW	NR 5	.78567932-01	.58067810-01	-.62180548-03	-.34535808-03	-.31832823
ROW	NR 6	• 28879373	-.49754370-01	• 63869415-03	-.12290437-02	• 19315409
ROW	NR 7	• 00000000	• 00000000	• 00000000	• 00000000	• 00000000
ROW	NR 8	• 00000000	• 00000000	• 00000000	• 00000000	• 00000000
ROW	NR 9	• 00000000	• 00000000	• 00000000	• 00000000	• 00000000
ROW	NR 10	• 00000000	• 00000000	• 00000000	• 00000000	• 00000000
COLUMN	NR	6	7	8	9	10
ROW	NR 1	• 00000000	• 00000000	• 00000000	• 00000000	• 00000000
ROW	NR 2	• 00000000	• 00000000	• 00000000	• 00000000	• 00000000
ROW	NR 3	.14145960-04	• 00000000	• 00000000	• 49862601-04	• 00000000
ROW	NR 4	.12249854-02	• 00000000	• 00000000	• 00000000	• 23873246-02
ROW	NR 5	-.67394390-01	.31415920	• 00000000	• 00000000	• 00000000
ROW	NR 6	-.47811935	• 00000000	• 26179933	• 00000000	• 00000000
ROW	NR 7	• 00000000	-.25000000	• 00000000	• 00000000	• 00000000
ROW	NR 8	• 00000000	• 00000000	-.33333333	• 00000000	• 00000000
ROW	NR 9	• 00000000	• 00000000	• 00000000	-.52958364-02	• 00000000
ROW	NR 10	• 00000000	• 00000000	• 00000000	-.828862453	

Table 3.13. The A-matrix in Example 3.

B-MATRIX		COLUMN	NR	1				
ROW	NR			2	3	4	5	
ROW	NR 1	•00000000	•00000000	•00000000	•00000000	•00000000	•00000000	
ROW	NR 2	•00000000	•00000000	•00000000	•00000000	•00000000	•00000000	
ROW	NR 3	•00000000	•00000000	•00000000	•00000000	•00000000	•00000000	
ROW	NR 4	•00000000	•00000000	•00000000	•00000000	•00000000	•00000000	
ROW	NR 5	•00000000	•00000000	•00000000	•00000000	•00000000	•00000000	
ROW	NR 6	•00000000	•00000000	•00000000	•00000000	•00000000	•00000000	
ROW	NR 7	•25000000	•00000000	•00000000	•00000000	•00000000	•00000000	
ROW	NR 8	•00000000	•33333333	•00000000	•00000000	•00000000	•00000000	
ROW	NR 9	•00000000	•00000000	•65320781-02	•00000000	•00000000	•50344827-02	
ROW	NR 10	•00000000	•00000000	•00000000	•00000000	•82862454	•00000000	

Table 3.14. The B-matrix in Example 3.

MATRIX QO

COLUMN	NR	1	2	3	4	5
ROW NR	1	379.82376	-43.451472	34608.372	727.89941	5.8865554
ROW NR	2	-43.451471	110.31614	3774.3282	1525.7137	1.2761667
ROW NR	3	34608.371	3774.3284	9166720.6	-103378.96	1154.8761
ROW NR	4	727.89954	1525.7137	-103378.98	301072.06	171.96108
ROW NR	5	5.8865546	1.2761670	1154.8761	171.96107	1.8481911
ROW NR	6	2.7113116	2.9714576	-153.81176	678.83426	*50985337
ROW NR	7	4.7754853	96221570	920.80695	124.32339	*89868520
ROW NR	8	1.6680177	1.2289739	-87.778200	341.46571	*29917379
ROW NR	9	48.529049	35.200892	40288.950	-57.274871	5.2857703
ROW NR	10	2.1447715	3.8590539	-296.69852	824.96145	*47013877
COLUMN	NR	6	7	8	9	10
ROW NR	1	2.7113146	4.7754852	1.6680177	48.529049	2.1447713
ROW NR	2	2.9714602	*96221569	1.2289739	35.200894	*3.8590539
ROW NR	3	-153.81192	920.80695	-87.778200	40288.951	-296.69848
ROW NR	4	678.83495	124.32339	341.46571	-57.275035	824.96145
ROW NR	5	*50985406	*89868520	*29917379	5.2857701	*47013875
ROW NR	6	2.5550682	27412874	1.04244168	*14953485	1.8614350
ROW NR	7	*27412875	2.4004240	*17594776	4.1992211	*33977994
ROW NR	8	1.0424168	*17594776	1.7797400	*14854220-01	*93719392
ROW NR	9	*14953410	4.1992211	-.14854216-01	*338.62543	*26860848
ROW NR	10	1.8614363	*33977994	*93719392	*26860881	*2.8505125

Table 3.15. The Q_O -matrix in Example 3.

MATRIX Q1

COLUMN	NR	1	2	3	4	5
ROW	NR	1.0000000	0.0000000	0.0000000	0.0000000	0.0000000
ROW	NR 2	0.0000000	1.0000000	0.0000000	0.0000000	0.0000000
ROW	NR 3	0.0000000	0.0000000	1.0000000	0.0000000	0.0000000
ROW	NR 4	0.0000000	0.0000000	0.0000000	1.0000000	0.0000000
ROW	NR 5	0.0000000	0.0000000	0.0000000	0.0000000	1.0000000
ROW	NR 6	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000
ROW	NR 7	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000
ROW	NR 8	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000
ROW	NR 9	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000
ROW	NR 10	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000
COLUMN	NR	6	7	8	9	10
ROW	NR	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000
ROW	NR 2	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000
ROW	NR 3	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000
ROW	NR 4	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000
ROW	NR 5	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000
ROW	NR 6	1.0000000	0.0000000	0.0000000	0.0000000	0.0000000
ROW	NR 7	0.0000000	1.0000000	0.0000000	0.0000000	0.0000000
ROW	NR 8	0.0000000	0.0000000	1.0000000	0.0000000	0.0000000
ROW	NR 9	0.0000000	0.0000000	0.0000000	1.0000000	0.0000000
ROW	NR 10	0.0000000	0.0000000	0.0000000	0.0000000	1.0000000

Table 3.16. The Q₁-matrix in Example 3.

MATRIX 92

MATRIX Q2						
COLUMN	NR	1	2	3	4	5
ROW	NR 1	1.0000000	• 00000000	• 00000000	• 00000000	• 00000000
ROW	NR 2	• 00000000	1.0000000	• 00000000	• 00000000	• 00000000
ROW	NR 3	• 00000000	• 00000000	• 00000000	• 00000000	• 00000000
ROW	NR 4	• 00000000	• 00000000	• 00000000	• 00000000	10.00000
ROW	NR 5	• 00000000	• 00000000	• 00000000	• 00000000	10.00000

Table 3.17. The Q_2 -matrix in Example 3.

RESULT AFTER 571 RUNGE-KUTTA STEP

COMPUTED S-MATRIX

COLUMN	NR	ROW	NR	1	2	3	4	5	6	7	8	9	10
ROW	NR	1	380.	00371	-43.455655	34614.816	727.53316	5.8874521					
ROW	NR	2	-43.455655	110.31786	3775.5042	1525.7415	1.2763391						
ROW	NR	3	34614.815	3775.5044	9168047.6	-103376.58	1155.0512						
ROW	NR	4	727.53265	1525.7405	1.2763401	301073.06	171.96207						
ROW	NR	5	5.8871520	1155.0512	171.96212								
ROW	NR	6	2.7105601	2.9715248	-153.79704	678.83614							
ROW	NR	7	4.7759351	96235238	920.94452	124.32421							
ROW	NR	8	1.6676458	1.2290048	-87.773803	341.46676							
ROW	NR	9	48.479482	35.205842	40290.324	-57.130109							
ROW	NR	10	2.1437742	3.8591233	-296.69558	824.96413							
COLUMN	NR	ROW	NR	1	2	3	4	5	6	7	8	9	10
ROW	NR	1	2.7105675	4.7759351	1.6676459	48.479484	1.4985874	1.8614401					
ROW	NR	2	2.9715292	96235236	1.2290048	35.205845	4.1994457	4.33978178					
ROW	NR	3	-153.79722	920.94451	-87.773802	40290.324	-14701636-01	93719672					
ROW	NR	4	678.83715	124.32421	341.46676	-57.130075	338.64982	-26822516					
ROW	NR	5	.50985763	.89870375	.29917508	5.2860467	-.26822509	2.8505197					
ROW	NR	6	2.5550723	.27413143	.27413143	1.0424189	1.4985874						
ROW	NR	7	*27413144	2.4004387	2.4004387	*1.7594880	4.1994457						
ROW	NR	8	1.0424189	*17594880	*17594880	1.7797410	-14701636-01						
ROW	NR	9	*14985750	4.1994456	-14701627-01	*.93719672							
ROW	NR	10	1.8614420	*33978178	*.93719672								

Table 3.18. The result after 571 steps with $h = 1.62$.

RESULT AFTER 583 KUUCU-KUTTA STEP

COMPUTED S-MATRIX

COLUMN	NR	1	2	3	4	5
ROW	NR 1	380.00378	-43.455654	34614.824	727.53297	5.8871530
ROW	NR 2	-43.455654	110.31785	3775.5042	1525.7417	1.2763390
ROW	NR 3	34614.823	3775.5044	9168047.7	-103376.56	1155.0512
ROW	NR 4	727.53294	1525.7407	-103376.55	301073.07	171.96206
ROW	NR 5	5.8871534	1.2763395	1155.0511	171.96212	1.8482148
ROW	NR 6	2.9715264	-153.79712	-153.79712	678.83656	*50985672
ROW	NR 7	4.775357	920.94453	920.94453	124.32420	*89870376
ROW	NR 8	1.6676459	1.2290047	-87.773776	341.46677	*29917514
ROW	NR 9	48.479460	35.205842	40290.324	-57.130030	5.2860472
ROW	NR 10	2.1437747	3.8591238	-296.69556	824.96415	*47014100
COLUMN	NR	6	7	8	9	10
ROW	NR 1	2.7105674	4.7759356	1.6676459	48.479467	2.1437747
ROW	NR 2	2.9715292	*96235226	1.2290047	35.205844	3.8591256
ROW	NR 3	-153.79717	920.94453	-87.773777	40290.324	-296.69557
ROW	NR 4	678.03717	124.32420	341.46677	-57.129989	824.96414
ROW	NR 5	*50985766	*89870378	*29917514	5.2860464	*47014112
ROW	NR 6	< 5556733	*27413147	1.0424192	14985863	1.8614411
ROW	NR 7	.27413147	2.4004387	*17594882	4.1994457	*33978176
ROW	NR 8	1.0424192	*17594883	1.7797412	*14701564-01	*93719677
ROW	NR 9	*14985761	4.1994457	-14701557-01	338.64982	-26822494
ROW	NR 10	1.861442	*33978176	*93719676	-26822487	2.8505196

Table 3.19. The result after 583 steps with $h = 1.64$.

$h = 1.66$

RESULT AFTER 561 RUNGE-KUTTA STEP

COMPUTED S-MATRIX

COLUMN	NR	1	2	3	4	5	6	7	8	9	10
ROW	NR	1	379.98904	-43.477512	34616.792	722.32851	50748926	1.6437156	1.8720216		
ROW	NR	2	-43.477511	110.28535	3778.4478	1517.9916	89827353	3.4544656	3.4544656		
ROW	NR	3	34616.792	3778.4475	9167781.5	-102675.48	-299226.97	-29798213	-260.08807		
ROW	NR	4	722.32714	1517.9914	-102675.43	1155.4492	5.2865621	5.2865621	728.56961		
ROW	NR	5	5.8841959	1.2719399	1155.4492	170.91408	41541511	41541531	41541531		
ROW	NR	6	2.6988028	2.9540215	-152.21338	674.66656	1.2201830	48.482034	48.482034	1.6437156	
ROW	NR	7	4.7737986	•95917080	921.23232	123.56635	-86.975751	35.209655	35.209655	•30021058	
ROW	NR	8	1.6617216	1.2201830	-86.975751	339.36538	40289.980	-56.223239	-13669204-01	•82747251	
ROW	NR	9	48.482037	35.209652	40289.980	-260.08796	-260.08796	338.64938	-22087148	-2.1826091	
ROW	NR	10	1.8720191	3.4544652	728.56958			-.22087176			
COLUMN	NR	1	2	3	4	5	6	7	8	9	10
ROW	NR	1	2.6988120	4.7737986	1.6617216	48.482034	1.6437156	1.6437156	1.6437156	1.6437156	
ROW	NR	2	2.9540243	•95917079	1.2201830	35.209655	35.209655	35.209655	35.209655	35.209655	
ROW	NR	3	-152.21306	921.23232	-86.975750	40289.980	-86.975750	40289.980	40289.980	40289.980	
ROW	NR	4	674.66740	123.56635	339.36538	-56.223239	339.36538	-56.223239	-56.223239	-56.223239	
ROW	NR	5	•50749050	•89827354	•29798213	5.2865616	•29798213	5.2865616	5.2865616	5.2865616	
ROW	NR	6	2.5456546	•27241967	1.0376727	•15190771	1.0376727	1.0376727	1.0376727	1.0376727	
ROW	NR	7	•27241968	2.4001276	•17508617	4.1998180	•17508617	•17508617	•17508617	•17508617	
ROW	NR	8	1.0376727	•17508617	1.7775491	-13669204-01	1.7775491	1.7775491	1.7775491	1.7775491	
ROW	NR	9	•15190618	4.1998180	-.13669199-01	338.64938	-.13669199-01	338.64938	338.64938	338.64938	
ROW	NR	10	1.6437172	•30021058	•82747250	-.22087176	•82747250	•82747250	•82747250	•82747250	

Table 3.20. The result after 561 steps with $h = 1.66$.

$h = 1.80$

RESULT AFTER 576 RUNGE-KUTTA STEP

COMPUTED S-MATRIX

COLUMN	NR	1	2	3	4	5	6	7	8	9	10
ROW	NR 1	379.98091	-43.489766	34617.913	719.40854	5.8825412					
ROW	NR 2	-43.489765	110.26708	3780.0997	1513.6442	1.2694711					
ROW	NR 3	34617.914	3780.0994	9167633.1	-102282.21	1155.6726					
ROW	NR 4	719.40681	1513.6438	-102282.17	298191.31	170.32601					
ROW	NR 5	5.8825406	1.2694720	1155.6725	170.32608	1.8472860					
ROW	NR 6	2.6922080	2.9442018	-151.32523	672.32744	*50616114					
ROW	NR 7	4.7726009	*95738623	921.39388	123.14120	*89803217					
ROW	NR 8	1.6583979	1.2152344	-86.528098	338.18651	*29731289					
ROW	NR 9	48.483422	35.211788	40289.789	-55.714382	5.2868513					
ROW	NR 10	1.7195753	3.2274677	-239.55274	674.49618	*38471612					
COLUMN	NR	1	2	3	4	5	6	7	8	9	10
ROW	NR 1	379.98091	-43.489766	34617.913	719.40854	5.8825412					
ROW	NR 2	-43.489765	110.26708	3780.0997	1513.6442	1.2694711					
ROW	NR 3	34617.914	3780.0994	9167633.1	-102282.21	1155.6726					
ROW	NR 4	719.40681	1513.6438	-102282.17	298191.31	170.32601					
ROW	NR 5	5.8825406	1.2694720	1155.6725	170.32608	1.8472860					
ROW	NR 6	2.6922080	2.9442018	-151.32523	672.32744	*50616114					
ROW	NR 7	4.7726009	*95738623	921.39388	123.14120	338.18651					
ROW	NR 8	1.6583979	1.2152344	-86.528098	40289.789	-55.714382					
ROW	NR 9	48.483422	35.211788	40289.789	-55.714382	5.2868516					
ROW	NR 10	1.7195753	3.2274677	-239.55274	674.49618	*38471612					
COLUMN	NR	1	2	3	4	5	6	7	8	9	10
ROW	NR 1	379.98091	-43.489766	34617.913	719.40854	5.8825412					
ROW	NR 2	-43.489765	110.26708	3780.0997	1513.6442	1.2694711					
ROW	NR 3	34617.914	3780.0994	9167633.1	-102282.21	1155.6726					
ROW	NR 4	719.40681	1513.6438	-102282.17	298191.31	170.32601					
ROW	NR 5	5.8825406	1.2694720	1155.6725	170.32608	1.8472860					
ROW	NR 6	2.6922080	2.9442018	-151.32523	672.32744	*50616114					
ROW	NR 7	4.7726009	*95738623	921.39388	123.14120	338.18651					
ROW	NR 8	1.6583979	1.2152344	-86.528098	40289.789	-55.714382					
ROW	NR 9	48.483422	35.211788	40289.789	-55.714382	5.2868516					
ROW	NR 10	1.7195753	3.2274677	-239.55274	674.49618	*38471612					

Table 3.21. The result after 576 steps with $h = 1.80$.

It has been argued that numerical instability could be detected by inspecting the quantity

$$\delta(k) = \max_{ij} \{ |s_{ij}(k) - s_{ji}(k)| / |s_{ij}(k)| \}$$

and in table 3.22 we show this quantity for different steplengths. In table 3.22 we also show another quantity

$$\rho(k) = \max_{i,j} \{ | \frac{ds_{ij}(k)}{dt} | / |s_{ij}(k)| \}$$

In this example this quantity is more sensitive to numerical instability than δ .

Steplength	$\max_{ij} \{ s_{ij} - s_{ji} / s_{ij} \}$	$\max_{ij} \{ \left \frac{ds_{ij}}{dt} \right / s_{ij} \}$
1.62	$0.829 \cdot 10^{-5}$	$0.497 \cdot 10^{-7}$
1.64	$0.645 \cdot 10^{-5}$	$3.19 \cdot 10^{-7}$
1.66	$1.00 \cdot 10^{-5}$	9.57
1.80	$1.05 \cdot 10^{-5}$	5.56

Table 3.22. Two test quantities used to detect numerical instability.

4. CONCLUSIONS

The numerical integration of the Riccati equation is known to be a stable procedure. The numerical stability of the integration method used determines the upper limit of the steplength. The following rule of thumb can be given for the choice of steplength, h_{\max} .

Let $\lambda_i(t)$ be the eigenvalues of

$$(A - BQ_2^{-1} B^T S(t))$$

and

$$\mu_k(t) = \lambda_i(t) + \lambda_j(t) \quad i, j = 1, 2, \dots, n$$

The maximum steplength is then given by

$$h_{\max} \leq \hat{h}$$

where \hat{h} is given by

$$\hat{h} = \min_{\hat{h}} \{ h \mid h \mu_k(t) \in D_s, \forall k, t \}$$

and D_s is the domain of numerical stability of the integration method used.

A necessary condition to satisfy this rule is that

$$\hat{h} \tilde{\mu}_k \in D_s$$

where

$$\tilde{\mu}_k = \tilde{\lambda}_i + \tilde{\lambda}_j \quad i, j = 1, 2, \dots, n$$

and $\tilde{\lambda}_i$ is an eigenvalue of

For some

$$(A - BQ_2^{-1} B^T X)$$

For some choices of Q_o may be a sufficient condition too. It has also been proven that an improper choice of Q_o may lead to a considerable reduction of the steplength. It has been proven as well that the choice $Q_o = 0$ may lead to a limiting value of $S(t)$ such that the closed loop system is unstable.

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